

# Optimisation of Neural Network for Charpy Toughness of Steel Welds

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# Introduction



## **Neural network**

Empirical equation  $\rightarrow$  unphysical values

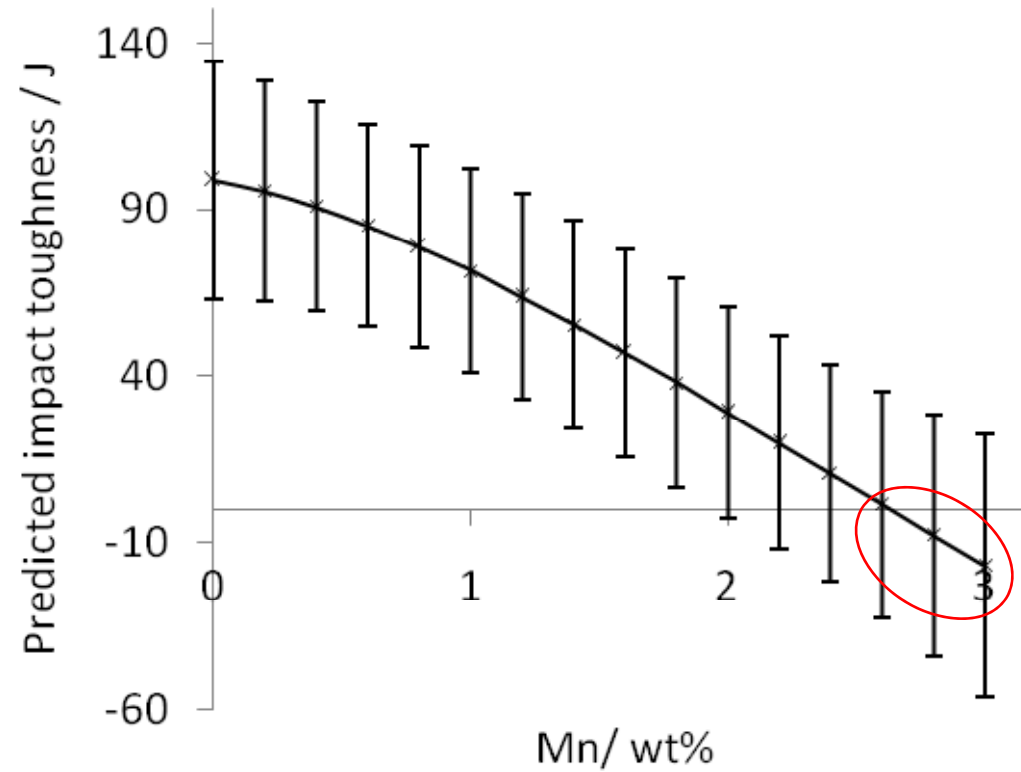
**Possible**

## **Charpy toughness (Impact toughness)**

Measured energy absorbed by a standard sample during fracture

**Never be negative !**

# Example of non-physical prediction



# Modelling of output (Yescas *et al.* 2001)

## Volume fraction from Avrami theory

$$\xi = 1 - \exp(-kt^n)$$

$\xi$ : volume fraction       $k, n$ : constants       $t$ : time

$$\ln[-\ln(1 - \xi)] \propto n \ln t$$

$$0 \leq \xi \leq 1$$

## Double logarithmic function for output

# Modelling of output (this work)

## New output form

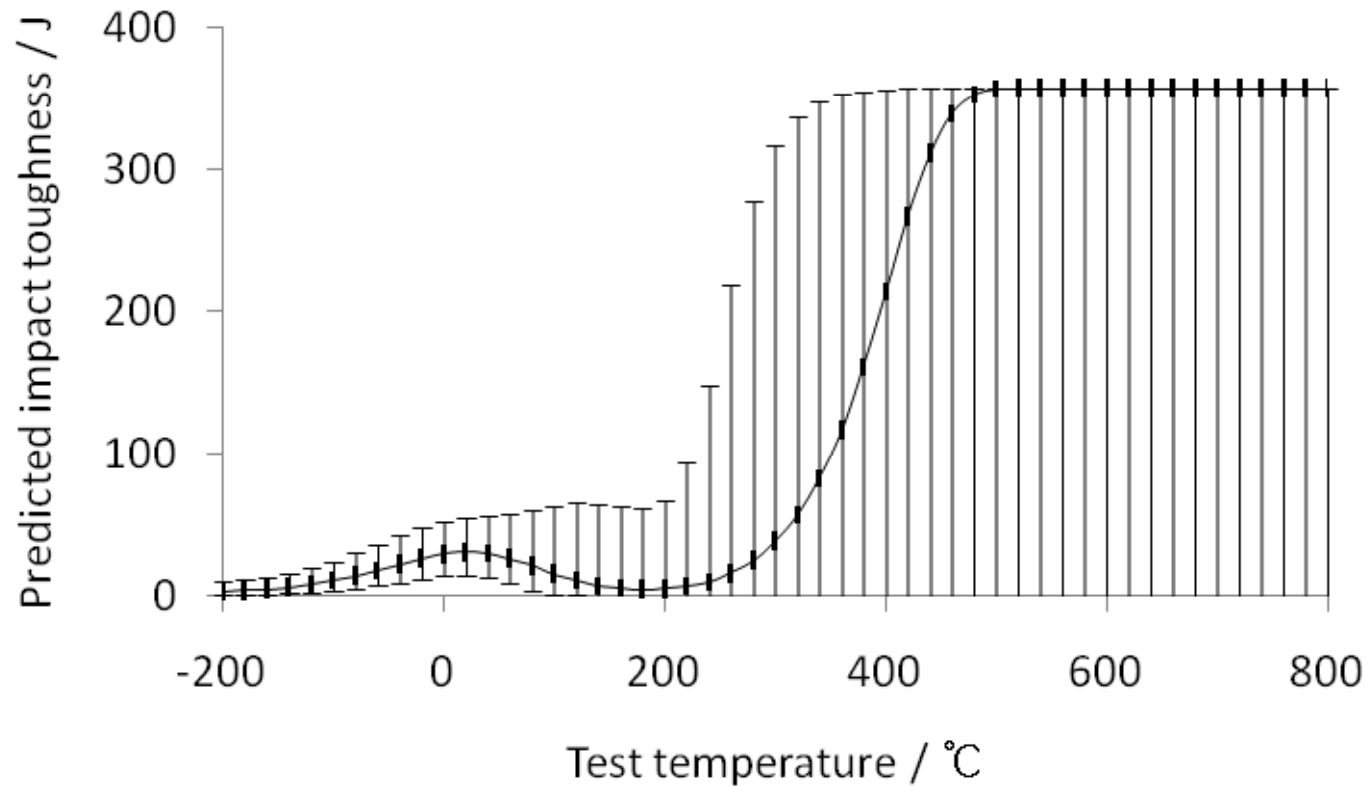
$$y' = -\ln \left\{ -\ln \left( \frac{y - y_{\min}}{y_{\max} - y_{\min}} \right) \right\}$$

$y_{\min} = 0 \text{ J}$       the least physical value of Charpy toughness

$y_{\max} = ?$       larger than the maximum value in database

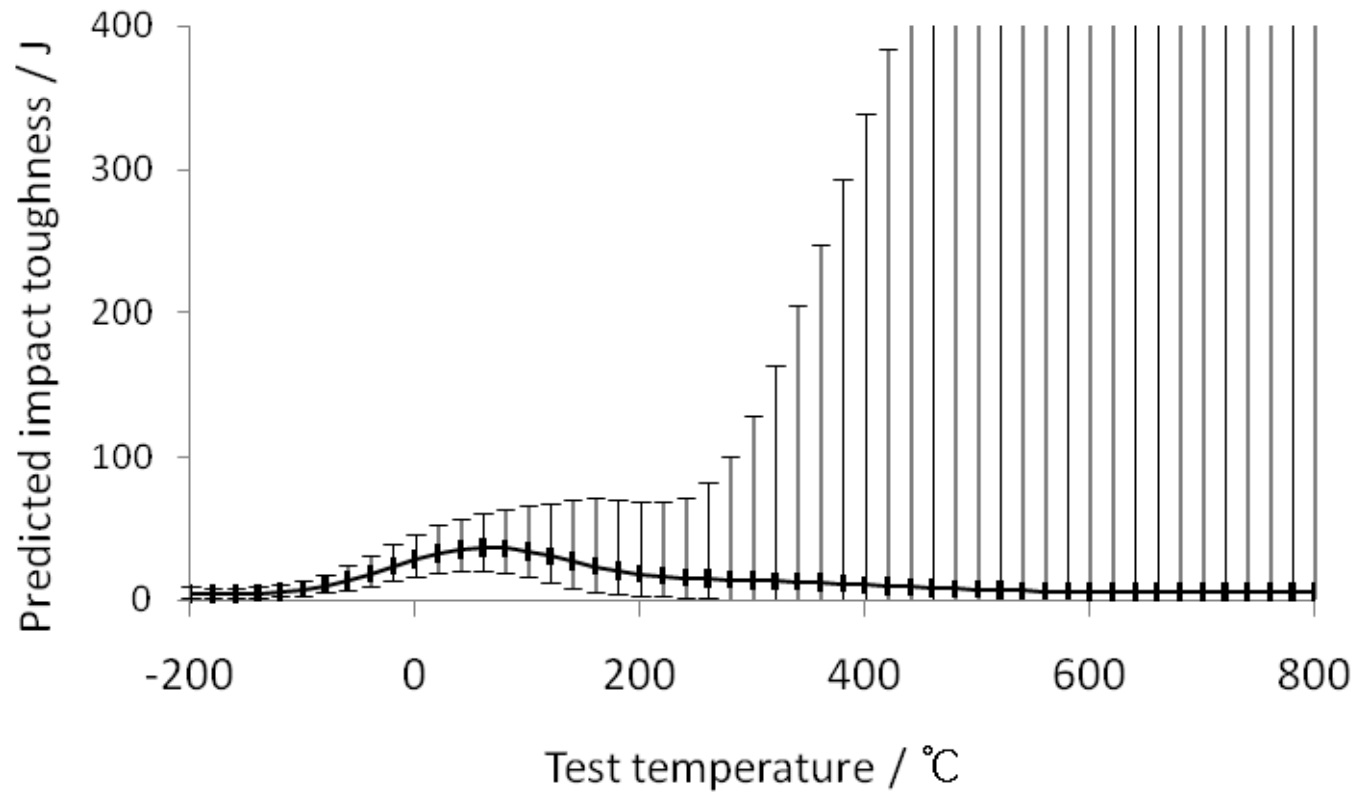
**$y_{\max} = 357 \text{ J}$  or  $3570 \text{ J}$**

# Bias in Models



$$y_{\min} = 0 \text{ J} \quad y_{\max} = 357 \text{ J}$$

# Bias in Models



$$y_{\min} = 0 \text{ J} \quad y_{\max} = 3570 \text{ J}$$



# Bias in Models

The selection of  $y_{\max} \rightarrow$  Bias

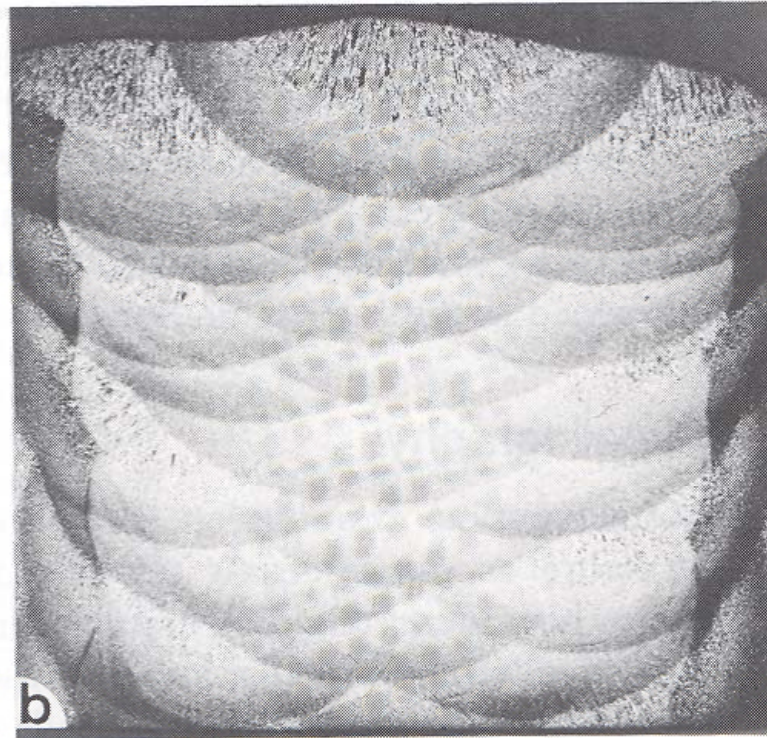
**Unjustified !**

Alternative way  $y' = \ln y$

$\rightarrow$  Infinite value of  $y_{\max}$

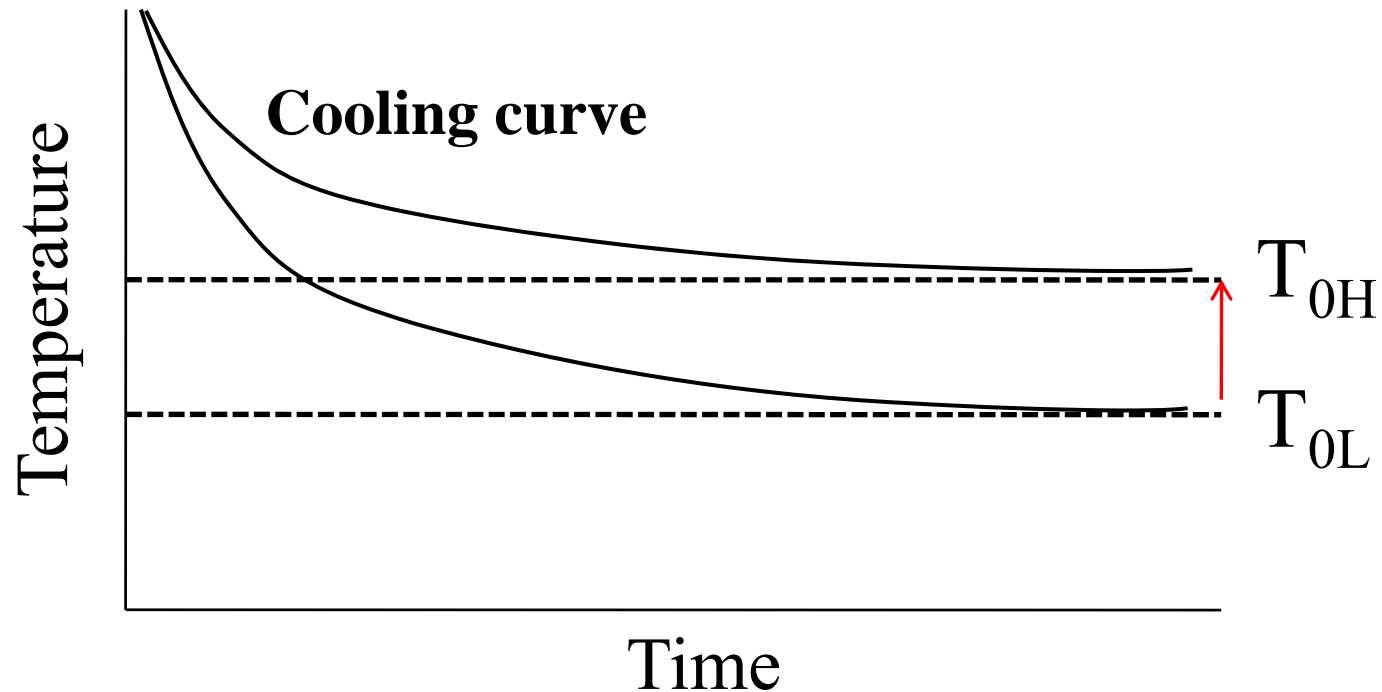
**Just use raw toughness value !**

# Interpass temperature



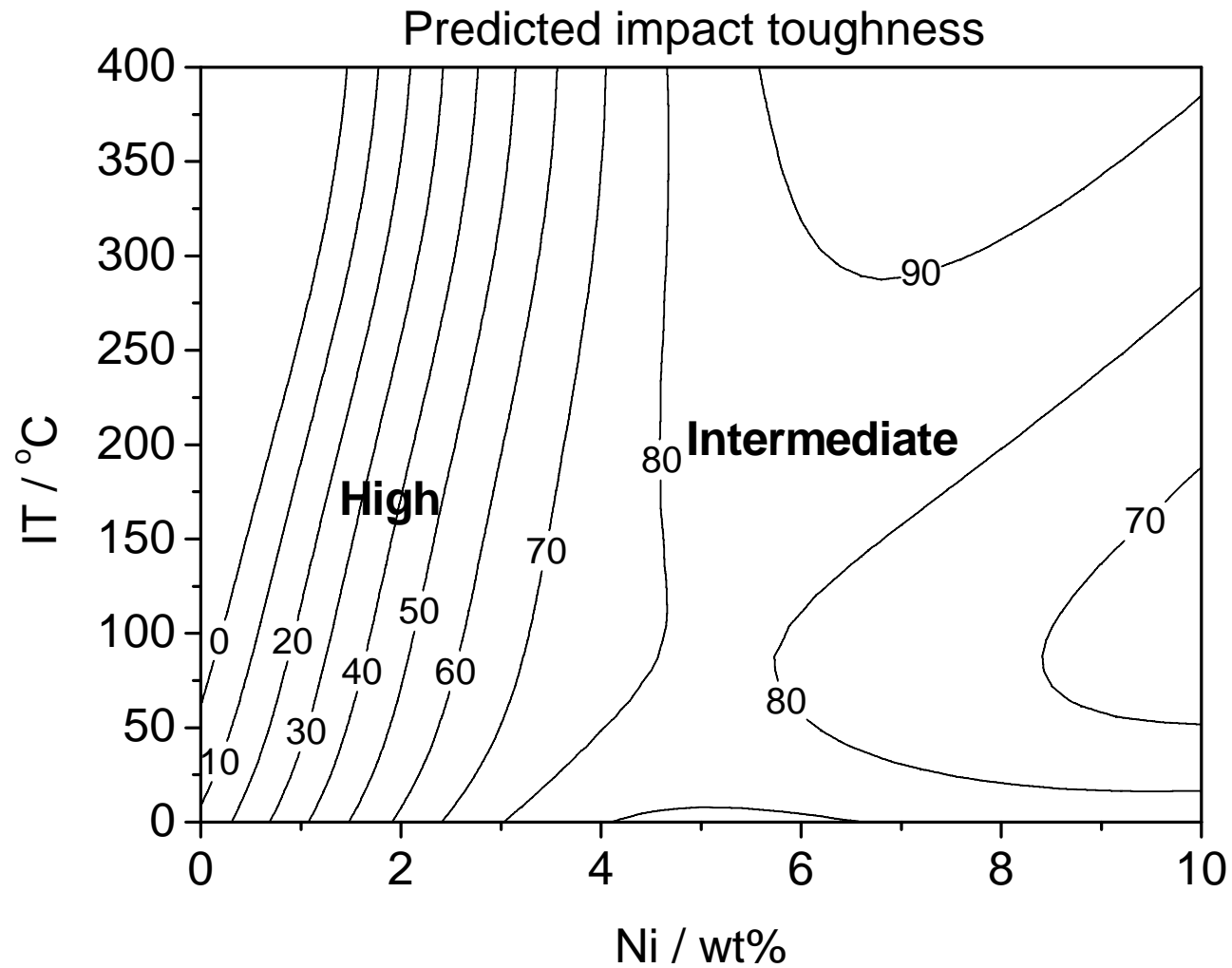
In multi-run welding, the temperature maintained immediately before depositing more metal

# Interpass temperature

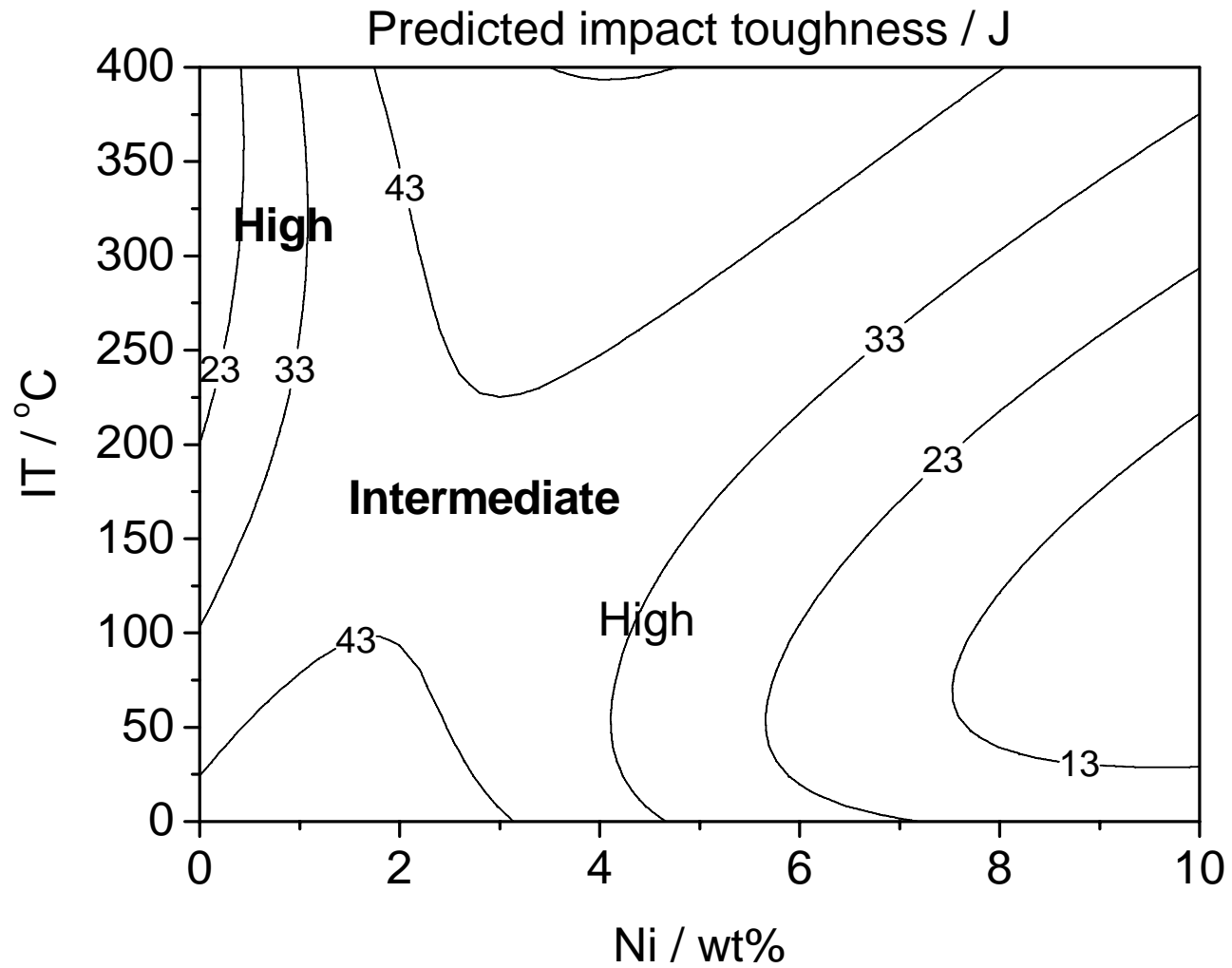


**Higher interpass temperature  
→ lower cooling rate**

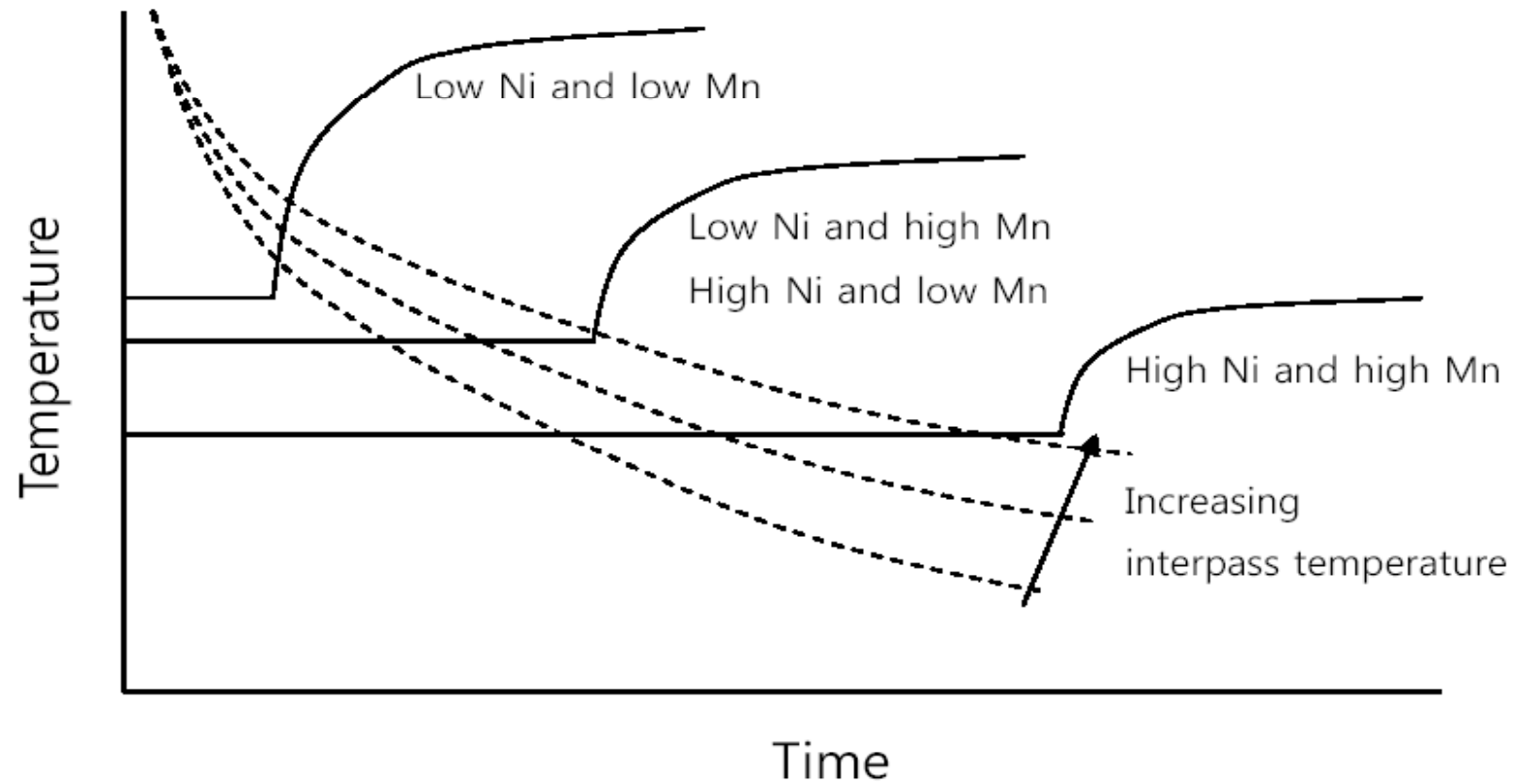
# Results (0.5Mn)



# Results (2Mn)



# Discussion (CCT and cooling curve diagram)



# Conclusions



**Using logarithmic representation of Charpy toughness introduced unjustified bias.**

**Interpass temperature cause different effect to Charpy toughness with respect to Ni and Mn.**



**Thank you**



# Input data (modelling bias)

All elements are in wt% unless otherwise specified.

C	Si	Mn	S	P	Ni	Cr	Mo
0.034	0.27	2.14	0.008	0.01	7.3	0.5	0.62
V	Cu	Co	W	O / ppmw	Ti / ppmw	N / ppmw	B / ppmw
0.011	0.03	0.009	0.005	330	80	120	10
Nb / ppmw	HI / kJ mm <sup>-1</sup>	IT / °C	PWHTT / °C	PWHTt / h	D <sub>Fe</sub>		
10	1	250	20	0	0		

HI: Heat input

IT: Interpass temperature

PWHTT: Post-weld heat treatment temperature

PWHTt: Post-weld heat treatment time

D<sub>Fe</sub>: A variable considering iron diffusion during post-weld heat treatment

# Input data (Ni-IT prediction)

All elements are in wt% unless otherwise specified.

C	Si	Mn	S	P	Ni	Cr	Mo
0.025	0.37	0.65 / 2	0.006	0.013	6.6	0.21	0.4
V	Cu	Co	W	O / ppmw	Ti / ppmw	N / ppmw	B / ppmw
0.011	0.03	0.009	0.005	380	80	180	1
Nb / ppmw	HI / kJ mm <sup>-1</sup>	IT / °C	PWHTT / °C	PWHTt / h	D <sub>Fe</sub>	TT / °C	
10	1	250	20	0	0	-60	

# Calculation of $t_{8/5}$ (Svensson *et al.*, 1986)

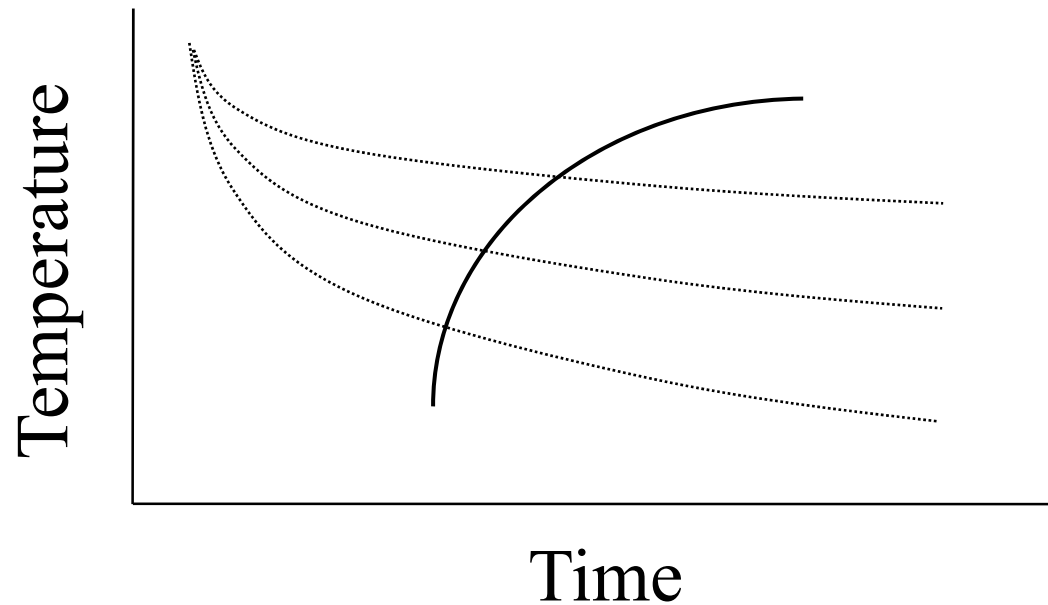
$t_{8/5}$ : cooling time from 800 °C to 500 °C

**Higher  $t_{8/5} \rightarrow$  lower cooling rate**

Under the heat input of 1.53 kJ

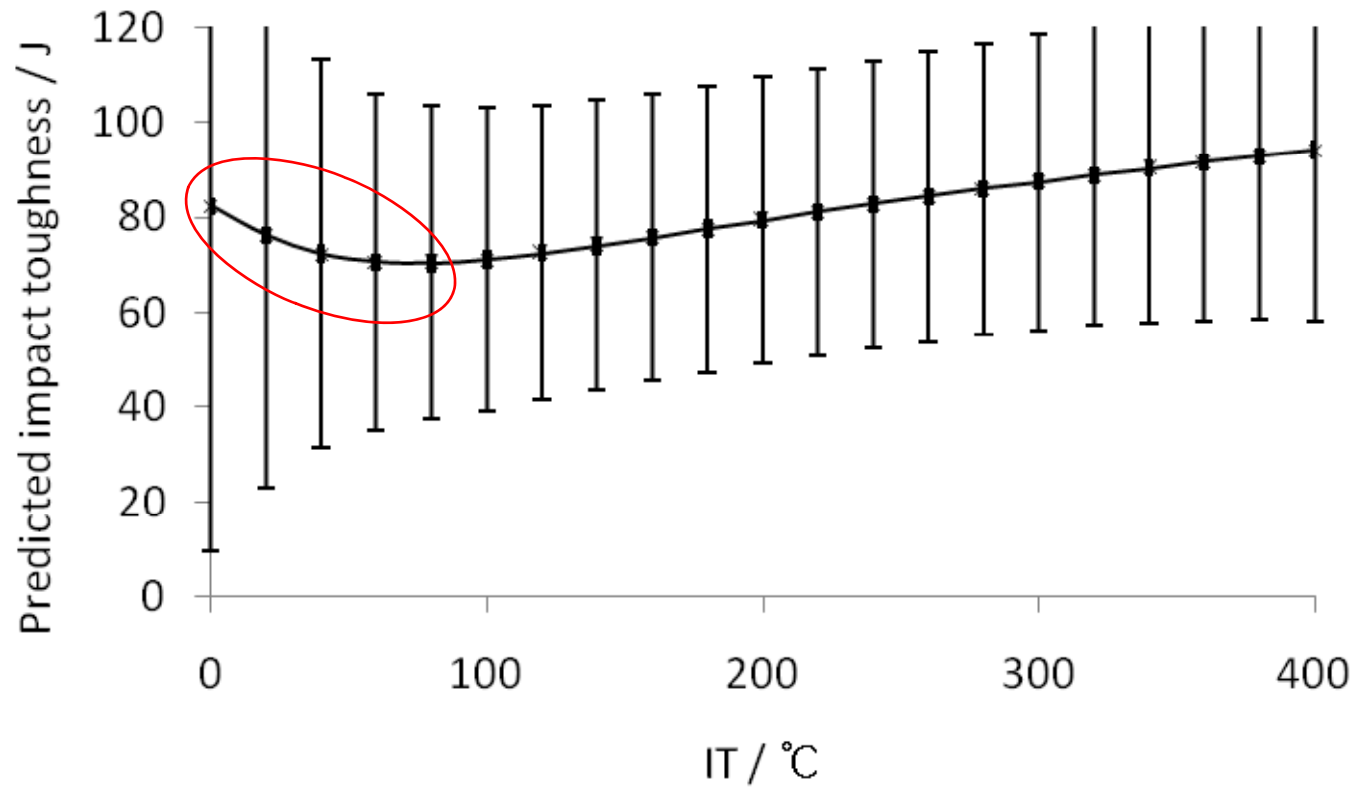
Interpass temperature (°C)	100	200	300	400
$t_{8/5}$ (s)	11.7	16.6	26.3	53.1

# Discussion

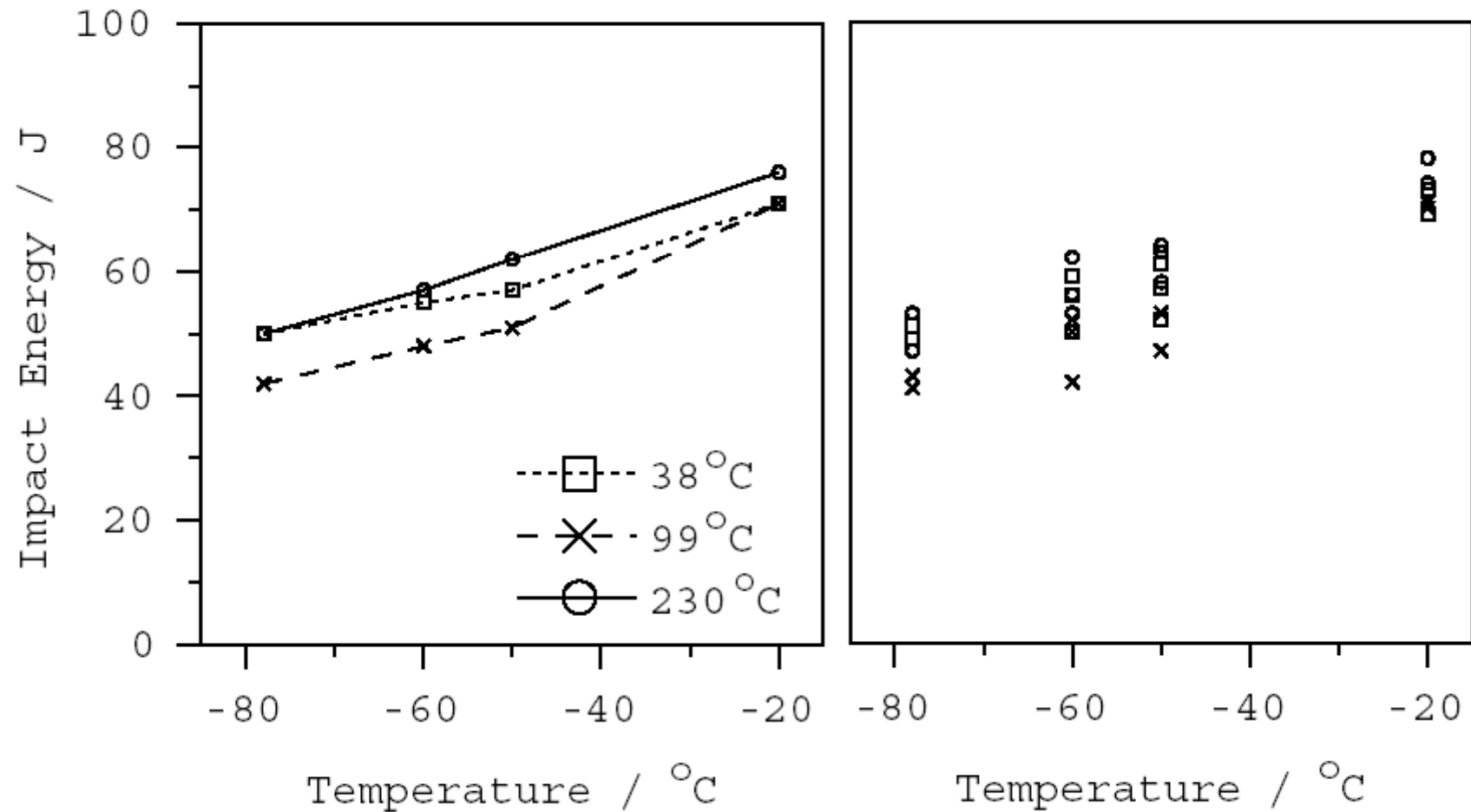


High transformation temperature  
→ coarser microstructure (Lord, 1999)

# Interpass temperature effect

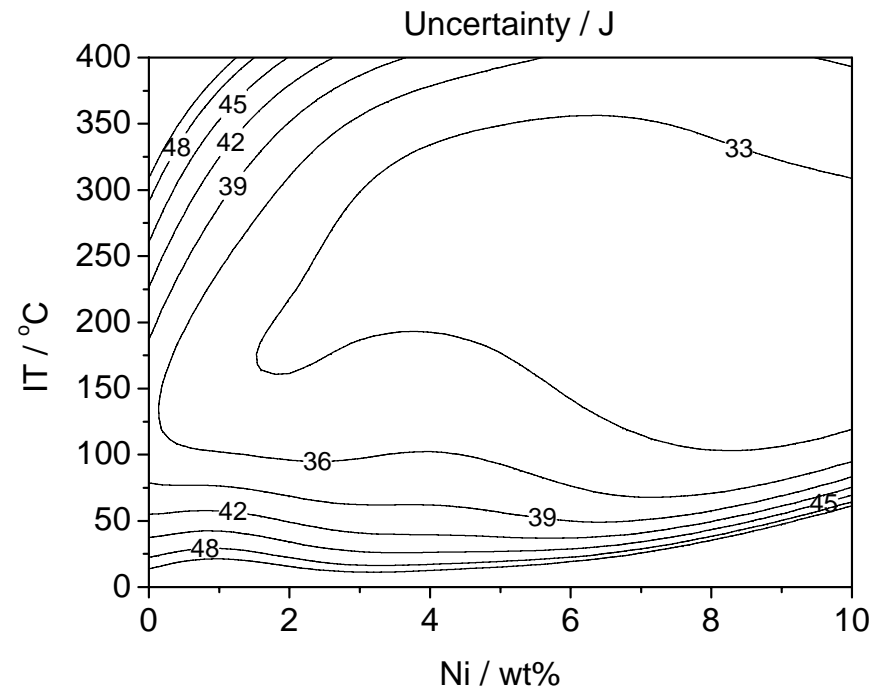
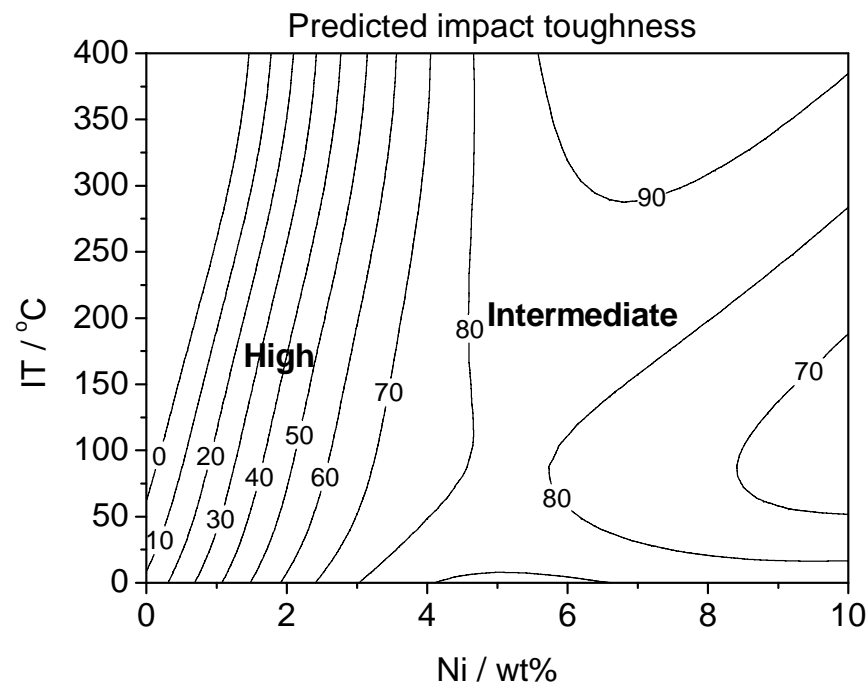


# Evidence (Lord, 1999)

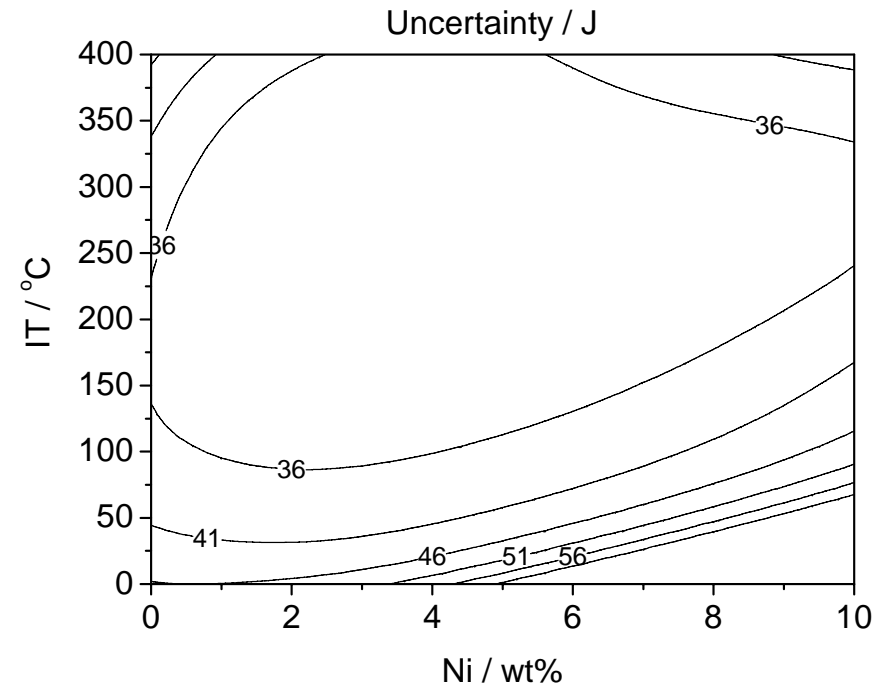
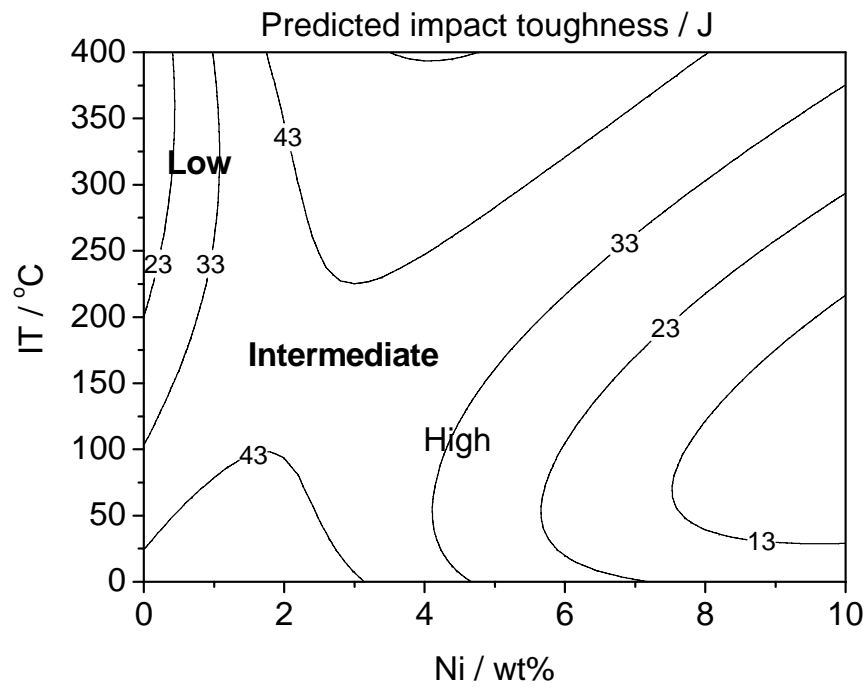


**CHV (99 °C IT) < CHV (38 °C IT)**

# Results (0.5Mn)

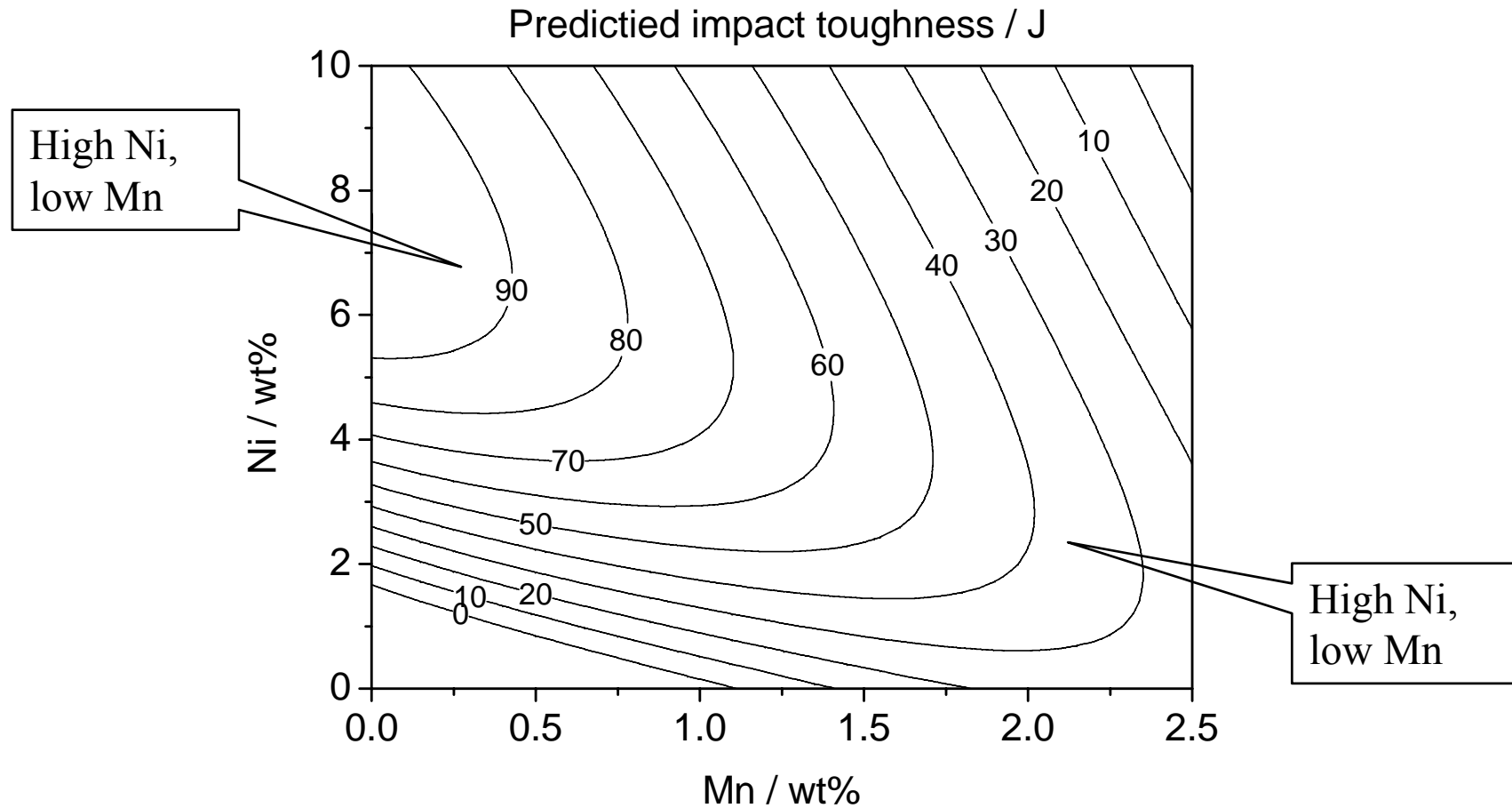


# Results (2Mn)



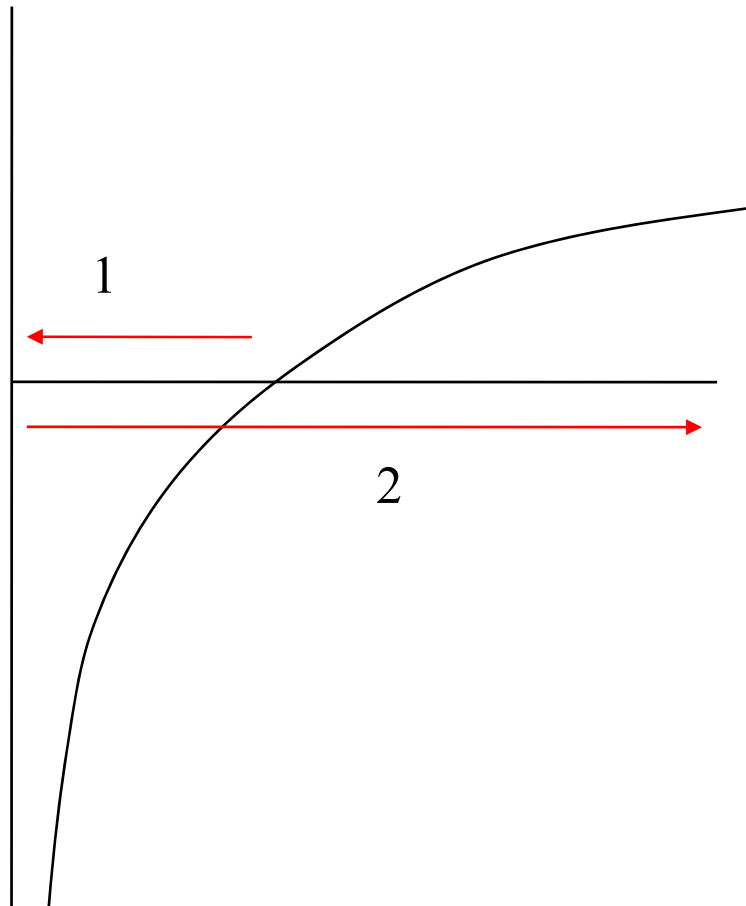


# Discussion (Ni-Mn prediction)



# Double logarithms

Yescas's work



This work

