

# Introduction to ab initio calculation and $\kappa$ -carbide

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Pt-group meeting presentation

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# First-principles (*ab initio*) calculation

$$\hat{H}\Psi = E\Psi$$

$$\hat{H}\Psi = E\Psi \quad \text{Schrödinger Equation}$$

Ground state energy for any given compound or solid

Variational principle

$$E = \min_{\phi} \langle \phi | \hat{H} | \phi \rangle, \quad \int_{-\infty}^{\infty} dx |\phi(x)|^2 = 1$$

$$\hat{H}\Psi = E\Psi \quad \text{Schrödinger Equation}$$

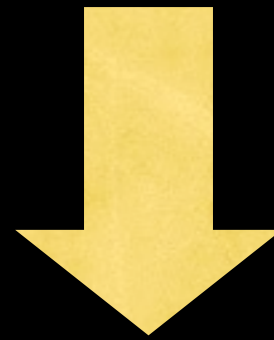
Ground state energy for any given compound or solid

$$\left\{ \sum_{i=1}^n -\frac{1}{2} \nabla_i^2 + \sum_{i=1}^n v_{ex}(r_i) + \sum_{i=1}^n v_{ext}(r_i) \right\} \Psi(r_1, r_2, \dots, r_n) = E\Psi(r_1, r_2, \dots, r_n)$$

Where,  $e^2 = \hbar = m_e = 1$

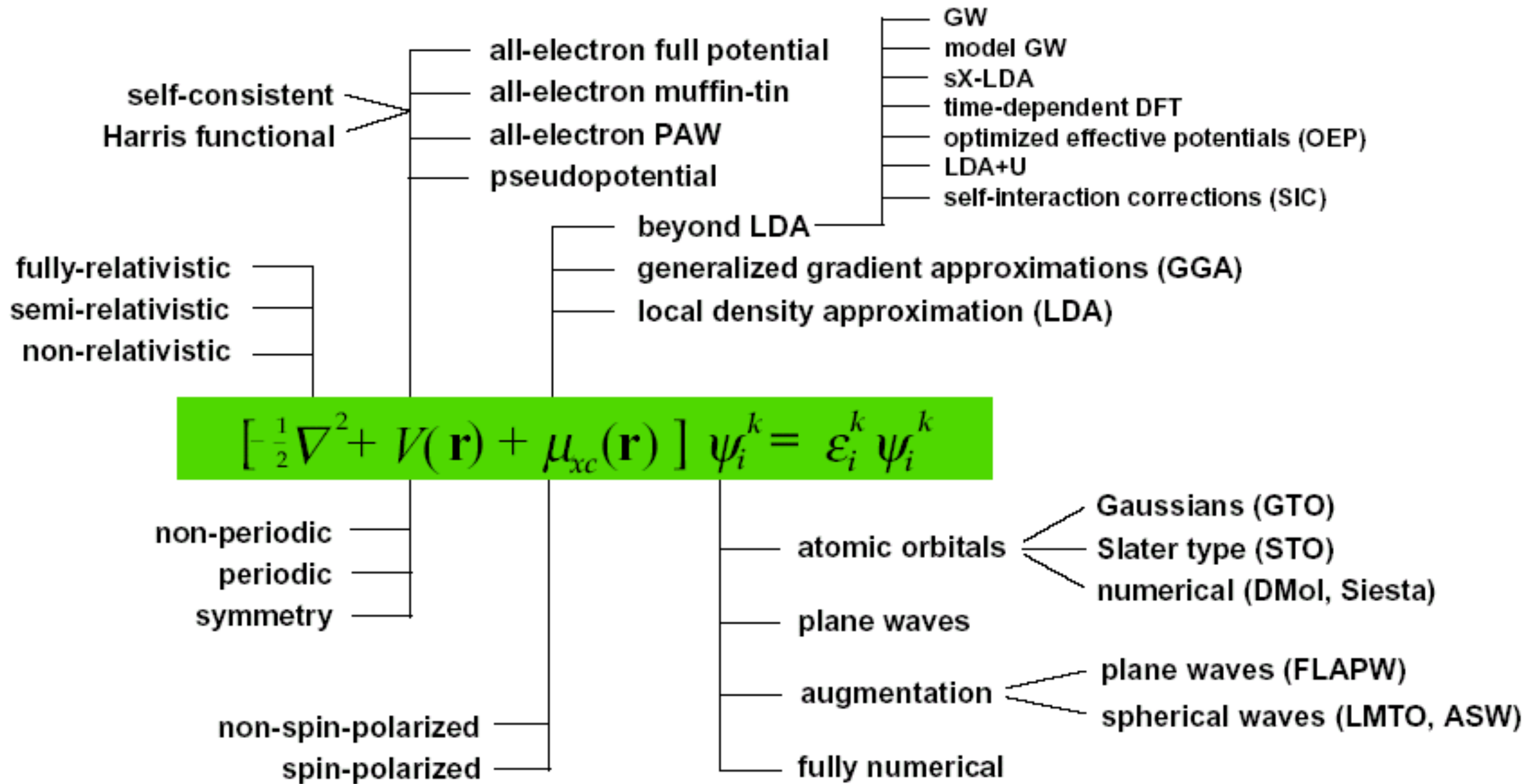
# Density Functional Theory (DFT)

$$\left\{ \sum_{i=1}^n -\frac{1}{2} \nabla_i^2 + \sum_{i=1}^n v_{ex}(r_i) + \sum_{i=1}^n v_{ext}(r_i) \right\} \Psi(r_1, r_2, \dots, r_n) = E \Psi(r_1, r_2, \dots, r_n)$$

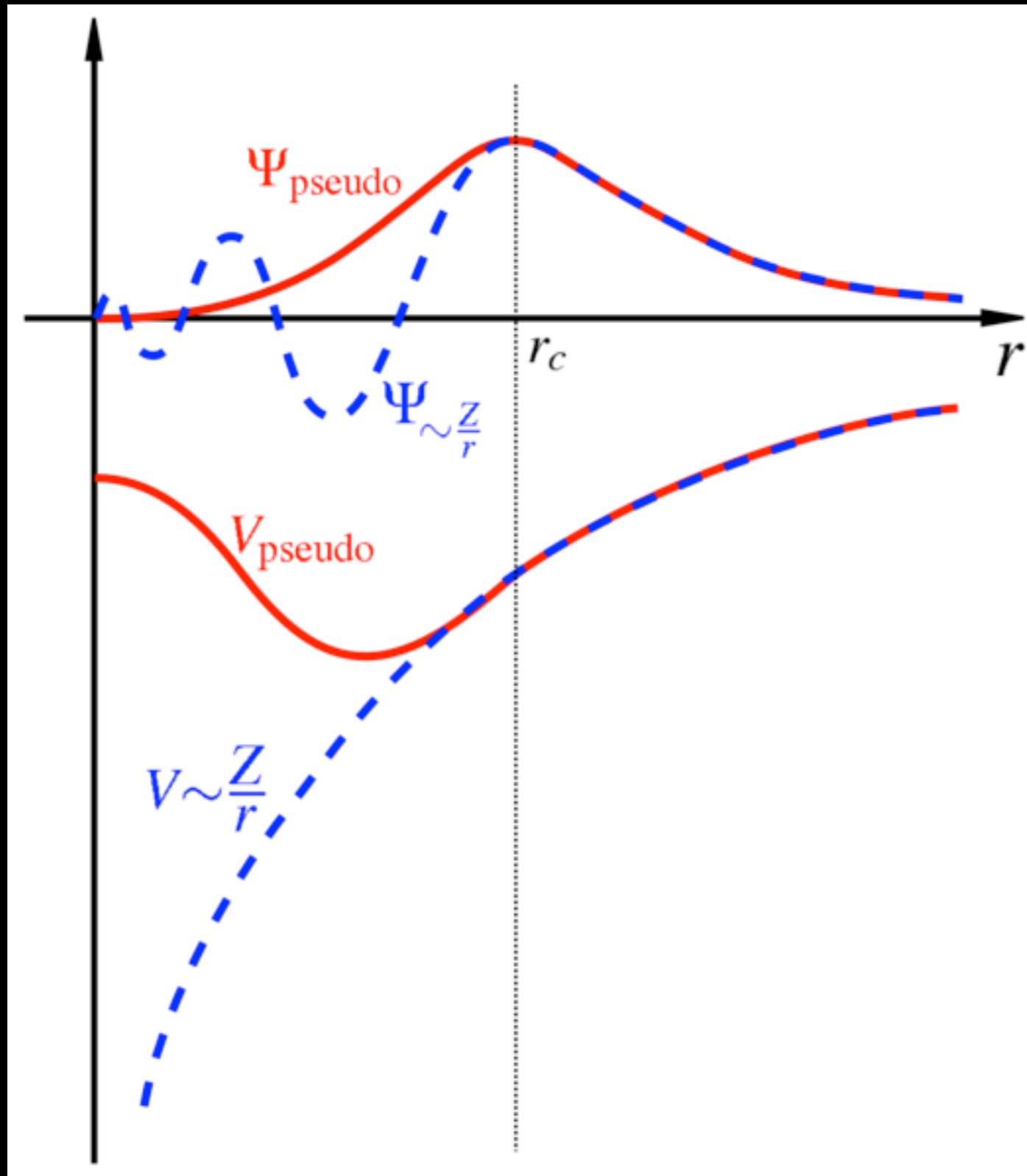


$$\left\{ -\frac{\nabla^2}{4} + \frac{|\nabla n|^2}{8n^2} + v(\mathbf{r}) \right\} n(\mathbf{r}) = E n(\mathbf{r})$$

# DFT Implementations







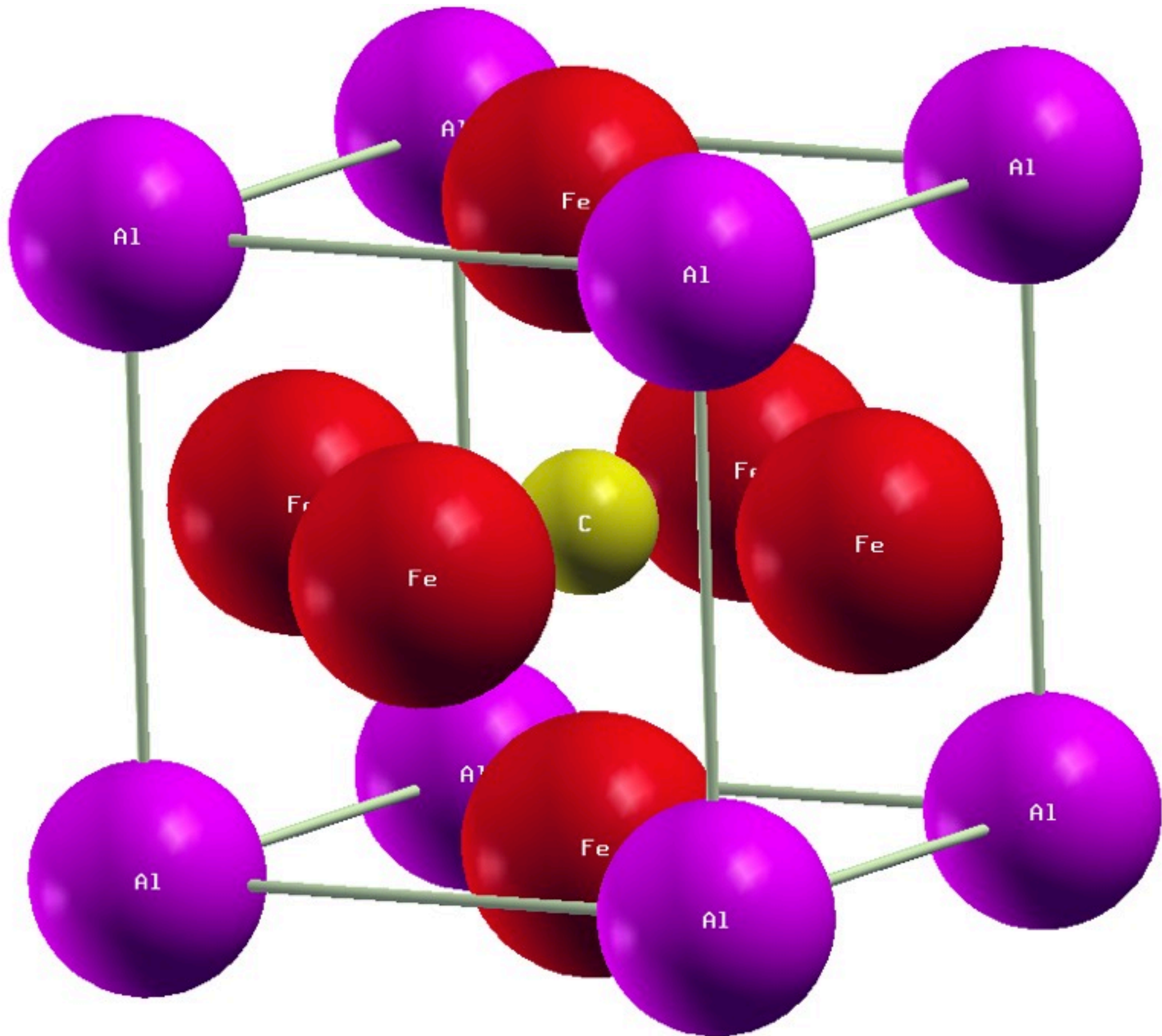
# Strong point

- Calculation at 0K is accurate (by theory).
- Making system is easy.
- Magnetic and electric properties.
- It can give thermodynamic variable.

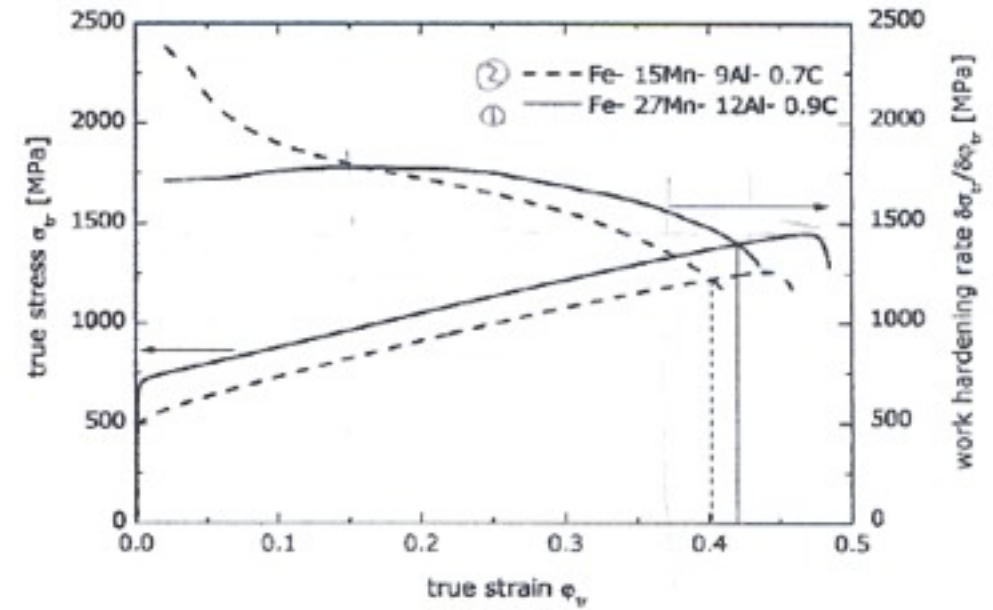
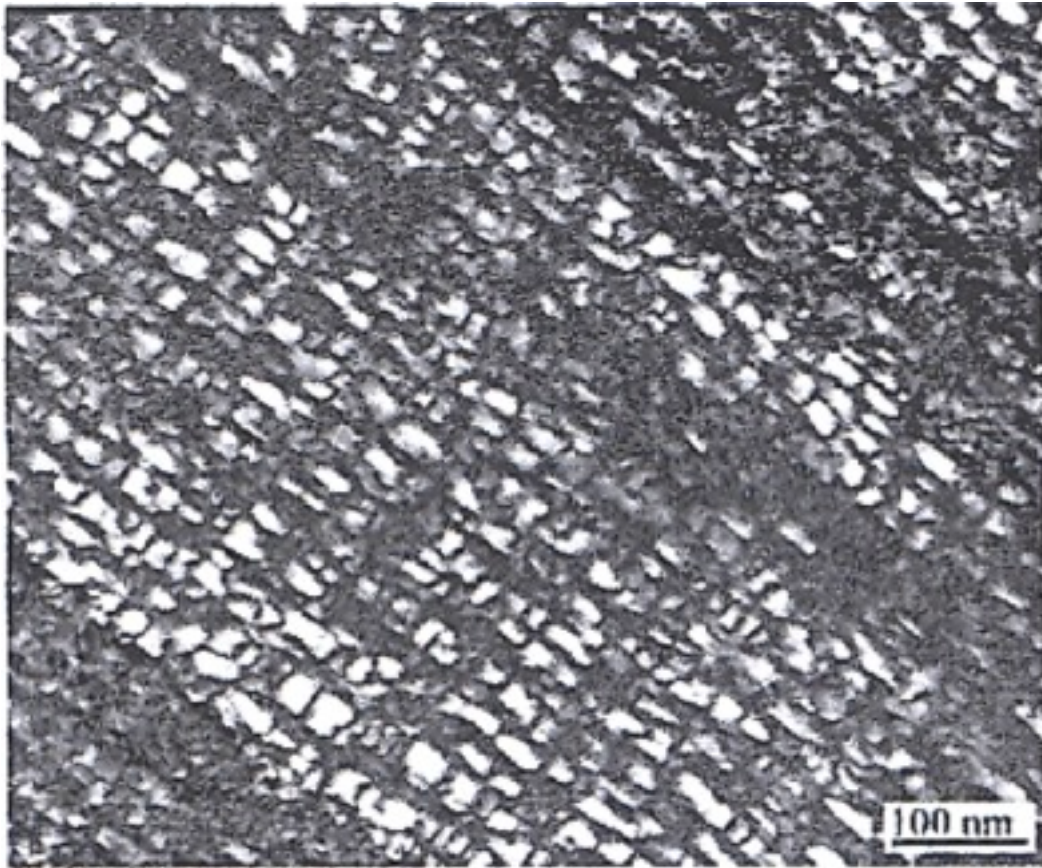
# Limitation

- It only calculate ground energy (0K).
- System size is small.
- Computer is too slow.

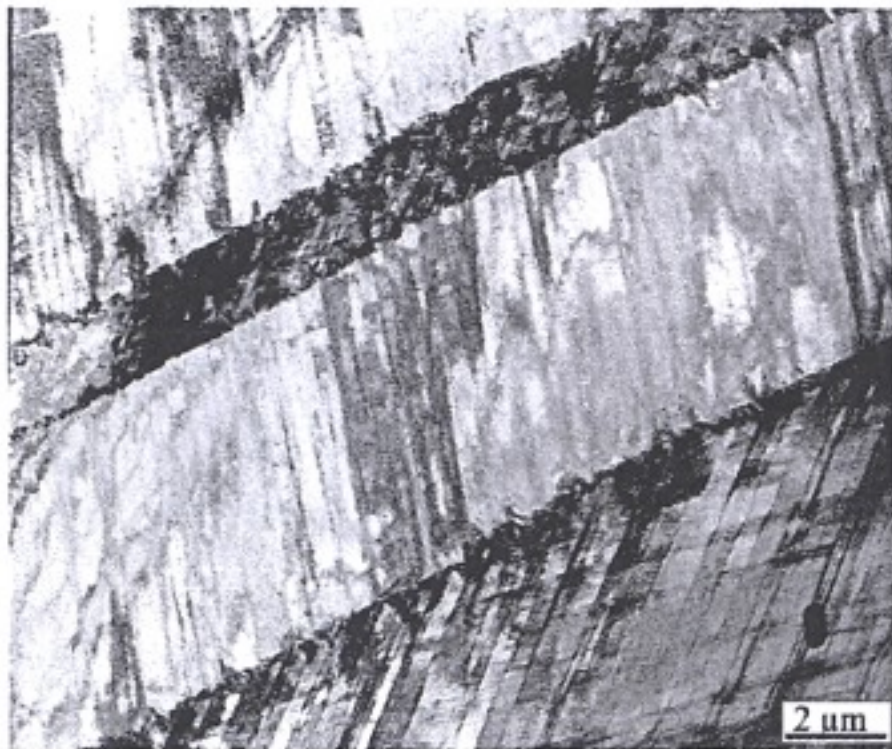
**K-carbide**



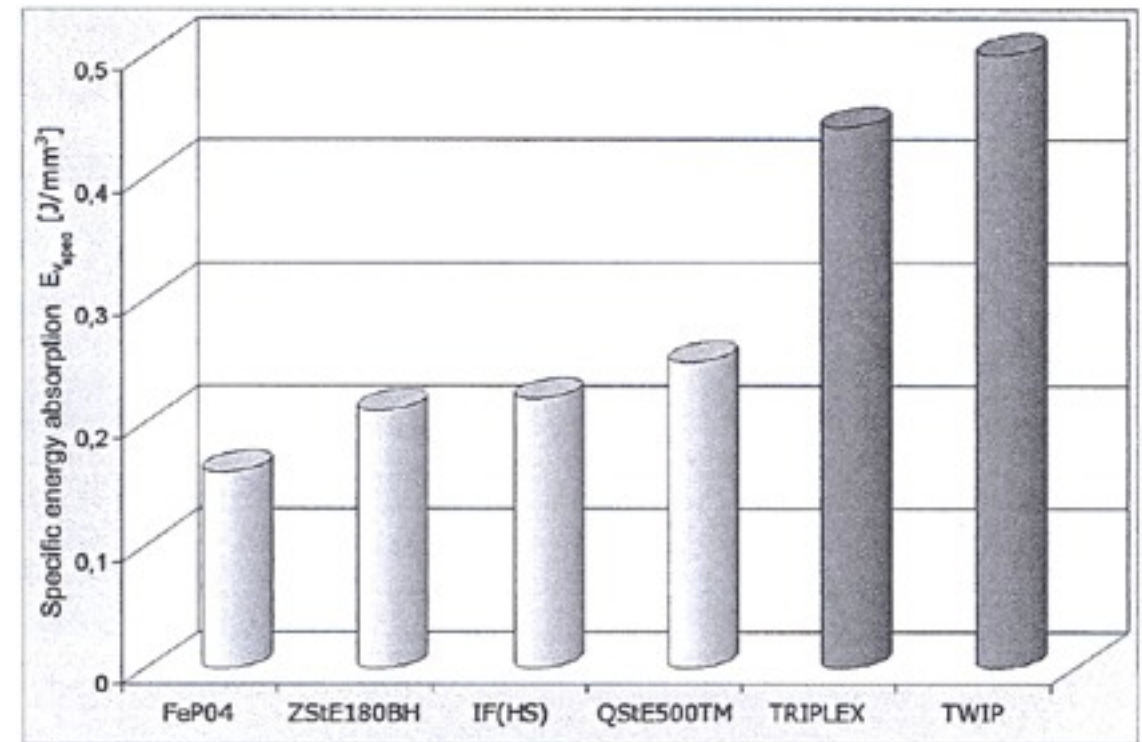




**Figure 5.** True-stress ' $\sigma_{tr}$ ' as a function of true-strain ' $\phi_{tr}$ ' and the related work hardening rate  $\delta\sigma_{tr}/\delta\phi_{tr}$  curves of two selected high-manganese-aluminium-carbon steels are showing that Considère's criterion is fulfilled for large plastic strains of about  $\phi_{tr} \approx 0.42$ .



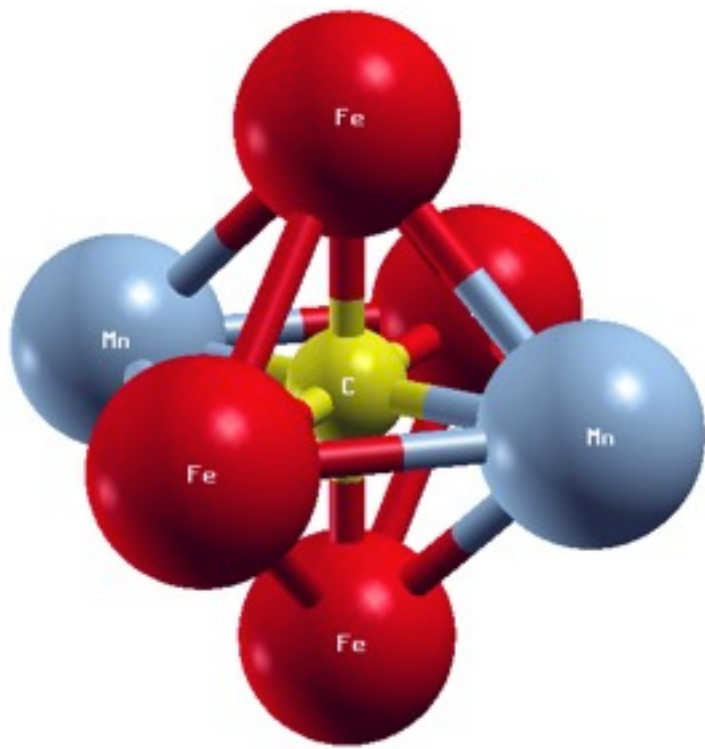
**Figure 8a.** TEM bright-field image exhibits shear bands on {111} planes in the austenitic matrix.



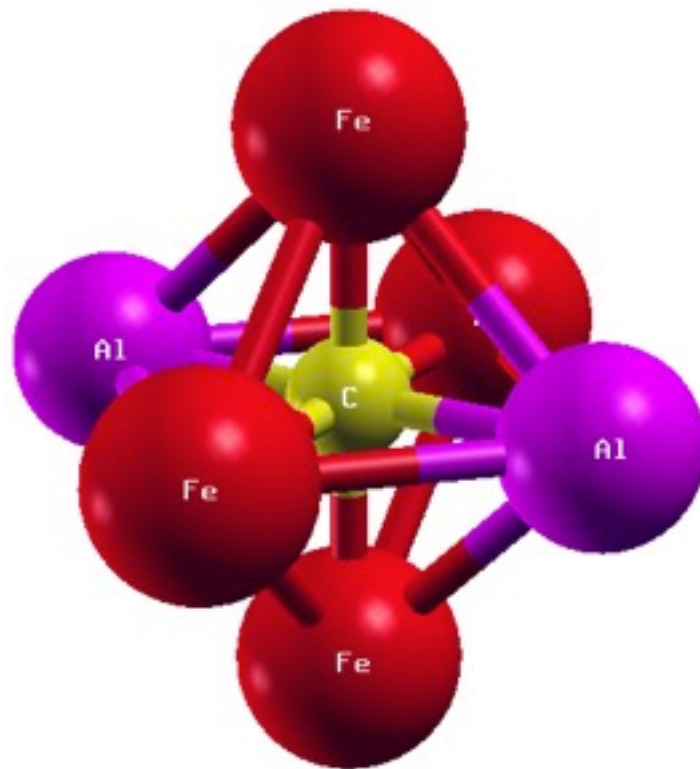
**Figure 11.** Bar diagram showing the specific energy absorption  $E_{spec}^Y$  of a TRIPLEX steel and a TWIP steel in comparison to conventional deep drawing steels at the crash relevant strain rate of  $\dot{\epsilon} = 10^2 \text{ s}^{-1}$ .

G. Frommeyer and U. Brux, 2006, steel research int. **77** (2006)

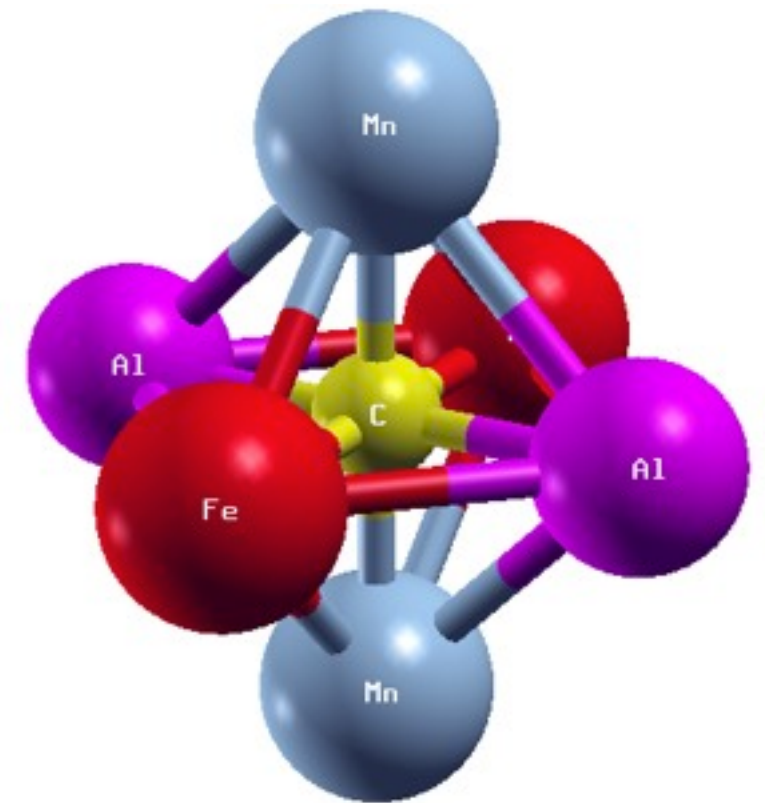




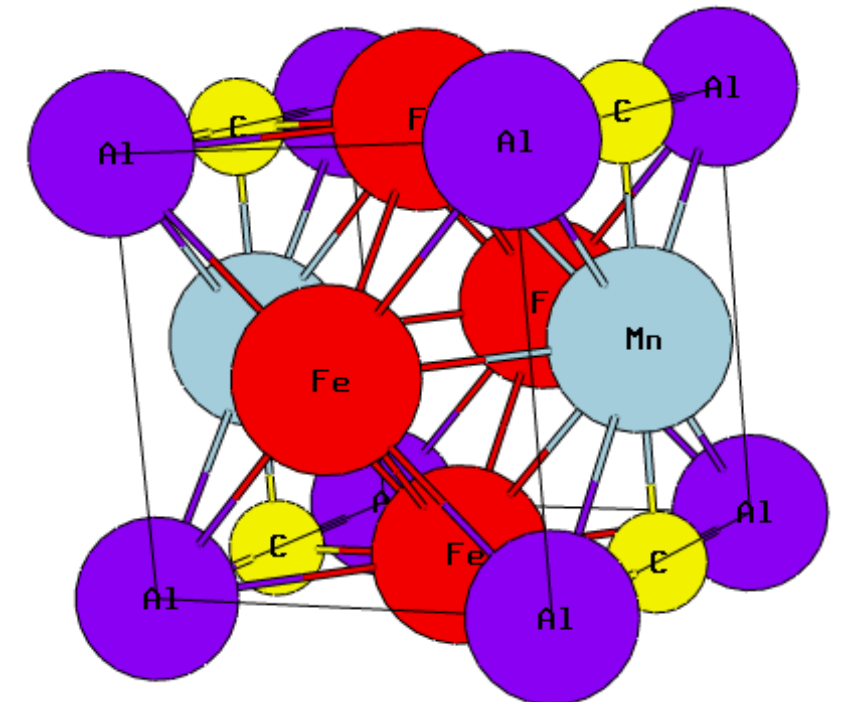
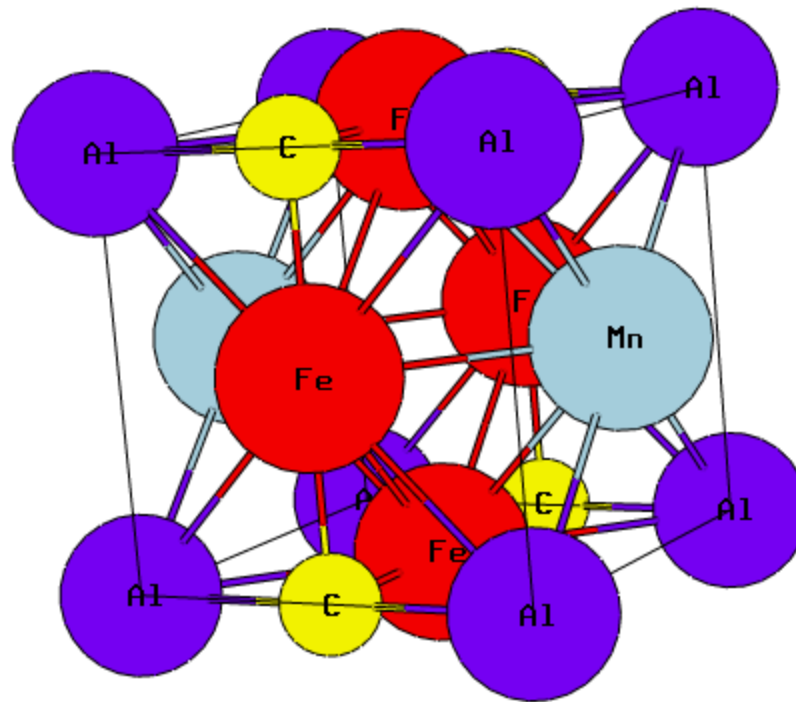
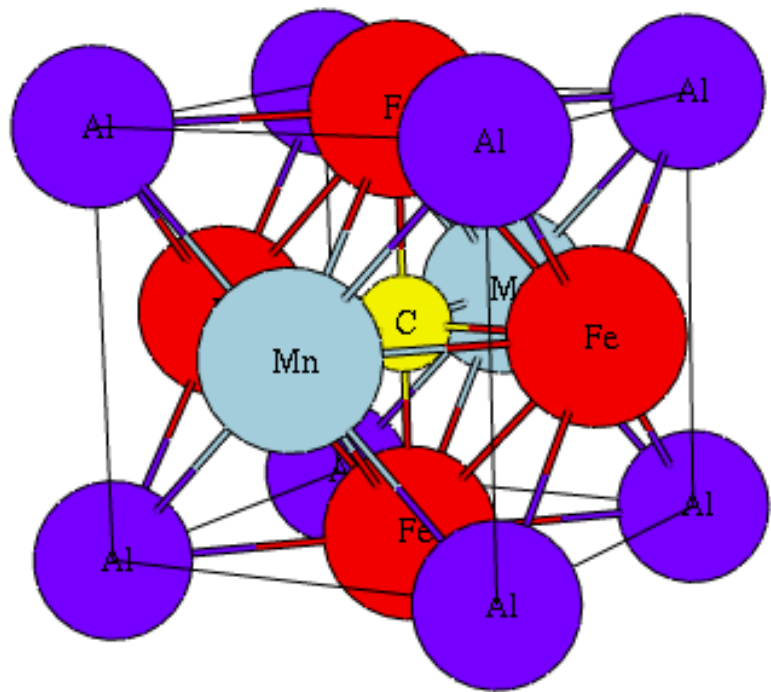
K-carbide (octa. 1)



Octa. 2



Octa. 3



# Main problem

Compounds	CALPHAD assessment	FLAPW*	Pseudo Potential*
L1 <sub>2</sub> Fe <sub>3</sub> Al	-17.5 <sup>a</sup> , -19.3 <sup>b</sup>	-8.8 <sup>c</sup>	-19.3 <sup>d</sup> , -21.4 <sup>e</sup>
E2 <sub>1</sub> Fe <sub>3</sub> AlC	-18.2 <sup>a</sup> , -16.0 <sup>b</sup>	-27.9 <sup>c</sup>	-18.4 <sup>e</sup>
E2 <sub>1</sub> Mn <sub>3</sub> AlC	-27.3 <sup>a</sup>	-	-

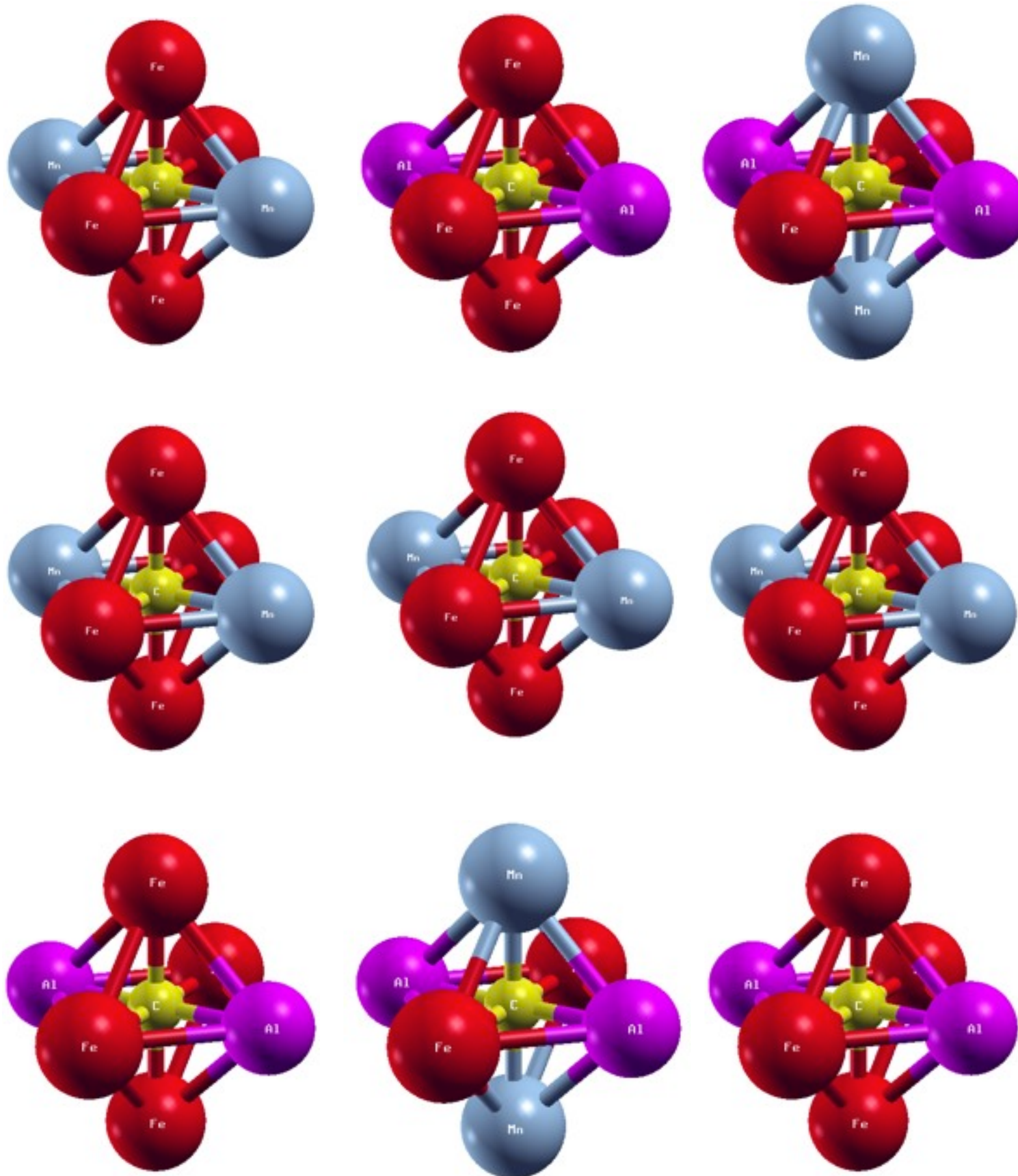
in kJ/atom – mol

Reassess the ab initio result to finite temperature.

Determine physical properties :  
bulk modulus, elastic constant, etc.

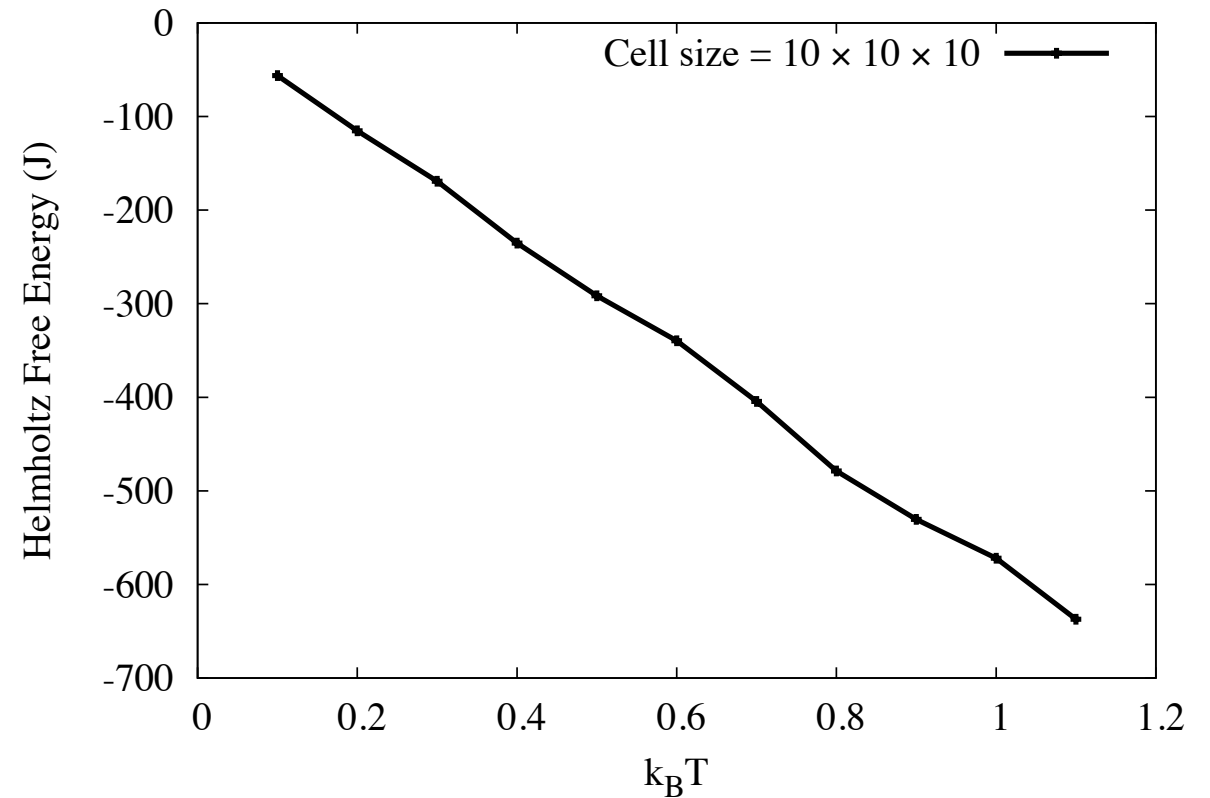


# Monte-Carlo simulation



# Monte-Carlo results

- There is no phase transition.
- C++ can't deal a number over  $10^{256}$ .
- If once the variable (for example, DOS) became bigger than limit, log value is also goes to infinite.
- $\therefore$  we should separate bottom and exponent.



$$F_{\text{Helmholtz}} = kT \ln(\text{sum of DOS})$$

Thank you!