

19/5/78

210⁻¹⁰ / Vac / 60 18/5/78 2: Lip painted @ 100°C, Cooked 450 x 5mm

		?			
<u>1+1</u>	<u>2.75+1</u>	220	51	<u>4.8+1</u>	200
640	526	646	227	267	50
530	2.8+1	58	456	220 240	220
524	602	506	456	267 204	
576	2.88+1	320 625	227	51	<u>5.2+1</u>
000	274	200	201	225	441
<u>1.2+1</u>	<u>2.95+1</u>		227	225	200
1450	617	4.0+1	212	220 = 220	444
1.0+1	621	232	203	265	220
264	257	52 404	210 201	50	217
<u>1.4+1</u>	272	202 557	461 = 62		446
201	256	454	200	<u>5+1</u>	451
<u>1.7+1</u>	272	201	461	50	177
520		1120		50	260
541	<u>2.6+1</u>	441	<u>4.6+1</u>	50 2 = 76.5	323
<u>1.9+1</u>	<u>2.45 507</u>	201 417	200	460	216
530	252	806	226	404	260
<u>2+1</u>	245		224	255	220
212	742	<u>4.44+1</u>	201	50	220
201	206	51 147	271	222 216	220
<u>2.5+1</u>		51 206	454	277	202 216
250	2941	231 226	224	220	221
201	242	204	226	441	260
405	230	227 460	474	256	50 264
<u>2.5+1</u>		57 227	225	215	67 200
404	4.1+1	207		260 220	222
405	206.457	227		50	50 221
213	445	456		215	61
	405	272		47 261	220
	202	462		216	216

5.4+1	5.8+1	264
46 215	256 211	
202 225	46 254	6e4+1
212	215 271	407
261	420	44
260 426 ⁼⁶⁴⁻²	253	210 244
212	272	44
277	261	261
212	202	1524
217	45	12 24!
212	272	
215	420	<u>flushed,</u>
264	252	
261 212		
47 217	<u>6+1</u>	
202	202	
275	252 202	
	202	
<u>5.6+1</u>	46 171	
255	204	
210	254	
256	252	
252		
46 257	6-2+1	
274	46	
274 210	200	
	62 ²² 200	
	252 201	
	200	
	250	
	46 247	
	200	
	204	

1/2 lip painted white cold, vacuum pumped cold, cooked.

<u>1+1</u>	<u>1.6+1</u>	425	<u>2.7+1</u>	<u>5.4+1</u>
21 262	772	1270 ¹⁷⁸	272	257 ²⁴
1162 1322	474 ³²	425		566 ¹¹⁰
2261		422	<u>2.8+1</u>	
1240	<u>1.8+1</u>	313	462	<u>5.5+1</u>
724	740	422		612
	671	552		772
<u>1.2+1</u>	425	424	<u>2.94+1</u>	
712 1026	1052	425	441	<u>5.8+1</u>
1121		447		305
1122	<u>2+1</u>	422	<u>4.2+1</u>	212
727	1052	422	247	
761	422	616 ^{58.55}		<u>6+1</u> ¹⁹
	724	422	<u>4.5+1</u>	226
1.5+1	1251	424	<u>4.67</u> ^{65.4}	211 ¹⁶
1000	673	422 ²⁸	614 106	
1017 1220	420	422	571 ^{80.5}	<u>6.2+1</u>
740 1112	717	717 ¹⁶ 761 ^{78.8}	217 ^{28.9}	444
711	642		245 ^{18.4}	460 ⁸²
1062	421	<u>2.2+1</u>		276 ^{104.7}
777	626	411 566	<u>4.8+1</u>	
776	422	407 602	404	<u>6.4+1</u>
251 501	421	422		257 ^{27.8}
707 1126	422	476 512	<u>5.7+1</u>	277 ⁴⁵
477 600	424	222	207	406 ⁶²
244	721			457 ^{80.2}
1014	424	<u>2.5+1</u>	<u>5.2+1</u>	262
1125	425	665	253	
1377	424	660	50	<u>6.83+1</u>
552	422	1050	<u>5.2+1</u>	202 711
	427	561	576	201
	422			410

$$1 + 192$$

$$2 + 96 + 0 = 104$$

$$3 + 64$$

Ne in - align

6.63 KV (blinky)	<u>7.5+1</u>	114 ^{6.3}	163	9.8+1.4
1 1/2 1/4 DW	422	173	420 ^{94.5}	406
	251	461 ¹⁰²	447	26 - 1/2 log
6.6+1	176	2271	427	154
~	174	210 462	40	25
6.9+1	264		1257	26
2706	257	<u>7.7+1.4</u>		26
116	175 260	442	<u>8.6+1.4</u>	27
44	42 505 ⁼¹¹⁰	42	441	406
	242 456 ^{=95.3}	41 442	440	1052
7.1+1	206	456	40	406
272	1062	2405	40	26
200	42 ⁼²²	42		26
1026	175 260		<u>8.8+1.4</u>	420
	174	7.9+1.4	27	26
7.3+1	227 ⁼²⁴	2152	422	155
221	176		1246	10+1.4
507	170	8.2+1.4	427	26
270 ⁶²		40	426	26
222 ²⁸	7.7+1	172		25
176	252	41	9.5+1.4	26
177 ^{16.5}	173		156	154
574 ¹¹²	173	8.4+1.4	156	26
176 246		444		
210 222	7.7+1.2	164 522 ⁼¹⁴⁴	Ne in	<u>10.2+1.4</u>
2221	216	220 421	- pnd @ 730?	416
222	462 ¹⁰³	446	1 1/2 1/4	<u>10.2+1.5</u>
	255 32	40	gas out-	152 400
	42	166 ^{11.8}	9.5+1.4	25
276 ²⁸	276 ²⁸	422	26	400
173	173	171 444 ^{12.6}	27	
254	254	442 ⁼¹⁰²	26	
			26	

10.2+1.6	10.7+1.6	272	147 212	144	207	3
400	272	315	267	144 206	145	
252	150	157 216		207	222	
276	214	65	11+1.7	206	205	
25	272	150	146	144 206	207	
26	215	215	210	144 205	264	
10.4+1.6	215	271	212	145	207	
51 216	214	215	265	205	206	
25	272	271	145	144 206	206	
25	112 150	151	207	206	206	
25	272	150 214	2600	205	207	
25	272	1066		25	145 205	
220	150		11.7+1.7	206	205	
25	154 265	10.9+1.6	206	145	142	
25	150 272	147	264	142	144 205	
51 217	215	212	207	144 206	206 222	
25	25 272	147 210	145	206	12 207	
25	272	210 266	210	205	206	
27 226 = 62.6	271	270	206	144	205	
17 275	147	147	206	145 261	145	
51 274	150 272	267	206	145	211	
25	215	275	206	207	206	
51	150 ¹⁶ 214	270	205	205	206	
26	271		206	144	206	
20	2542	11+1.6	207	144	207	
26	272	210	144 202	206	206	
	215	2646	144	207	206	
	215	211	145	206	272	
	157 216	211	206	206	143 206	
	147 215	265	206	206	262	
	25	210	206	145 205	206	
	271	206	262	205	206	
	214	210	142	206	207	

Blank Helm

DIV x 4 10.45

-spots/charity clean

11.7 + 1.6 wntd

206
207

206
206

145 206

207
206

205

205
206

206

12 205

206
206

207
207

210

200

64

202

144

204
206
207

206
144
206

205

207	207	206	205	205	261
206	205	206	201	204	211
205	207	210	207	206	205
	204	205		207	210
206	204	206	145 210	207	210
207	206	210	206	207	204
206	207	205	205	205	200
206	205	205	207	207	221 206
206	206	265	206	206	206
207	206			210	210
206	261	210	207	206	211
206	206	207	207	261	207
205	206	210	207	206	206
205	207	206	206	206	206
206	205	206	205	205	205
206	206	205	205	210	206
206	207	210	206	206	205
206	206	206	206	207	205
206	110	205	207	206	205
206	206	206	207	207	206
207	207	282	207	206	283
207	206 262	206	206	207	206
210	207	204	207	207	210
200	205	206	205	207	206
64	206	204	206	206	206
202	206	206	206	205	206
144	207	207	207	206	210
204	207	207	206	207	206
206	262	207	207	207	206
207	205	202	206	206	202
206	207	206	207	207	207
144	207	206	205	204	205
206	210	207	210	205	206
205	206	204	205	206	206
	205	206	206	207	207
				204	205

25/5/78 same 1v tip 3×10^{-10} / 60 / He
200

9.96 + 2.7

44
25

Atoms per plane for 1v tip @ 10.63 KV
in 4×10^{-8} He with channel plate
on and alignment & lens adjusted for
optimum catch with c-p on (i.e. not perfect
alignment)

from 200 plane

100

~~48~~ 88

96

100

94

86

90

=> \approx 100 atoms per plane (1v²⁺ & 4v³⁺
with He etc gated out).

10.63 + 2KV pulse = 12.63 total KV

= 93

= 5.2

write
100 / zone axes

125

146

107

119

122

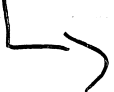
125

125.6 ± 11

Extract tip to paint (again).

Richard Oldman phoned to say green paint - (and bottle) is off
- should be brown. (!*** *!!!)

- pers for probe hole size



$$24 + 8 = 32$$

$$+ 16 = 48$$

Sat 4 June

lv trip painted paint + acetone, cold, cooled 450 - 5 mins

					245
1+1	740	426	056	240	024 052
	765	461	070 058	250	076
1.0+1	1160	410	055	069 = 01.4	246
1.45+1	450	410	065		055
	460	454	017	0.5+1	073
1.50+1	451	000 ²²⁸	050	401 407	404 = 39
	441	407	052	077 400 ⁴⁴	050
1.80+1	535	270 ¹⁵		277 ¹⁴	412 ⁴¹
	474	077 ²²⁸	0.2+1	077 ²⁸	245
	537	073	261 270	507 ⁵⁹	
	044	455	-break.	042	0.8+1
	472	270		420 ^{40.9}	1500
	474	621	0.2+1 again ⁵	1166 ²²⁰	240 255
	614	020	021	242	405
1.90+1	402	400	401	256	
2.14+1	421	075 ^{27.5}		077	0.2+1
	660	452 = 08.7	0.3+1		077
2.24	276	421	050 = 29.2	0.7+1	027 042
	424	072	002 ²⁰	600 = 28	264 410
	415 455	417 = 01.6	242 ¹⁴ 274 ¹⁴	245	406
2.27+1	026	072	076 ¹⁴	252 051	025
	564	426	256	260 420 ^{12.7}	451 = 53
2.35+1	425		1260	1256	502
	405	0+1	420 = 39.1	245	227 024
	446	056	049 ^{27.4} 512 ^{57.5}	470 = 55	226 002
	422	401	245	001 ²² 477 ⁵⁹	000
2.5+1	273	441 = 41	527 ^{68.2}	202 252 ²²	467
	474 = 40	254 441	0154	247	400
	267	241 056	064	401 ^{38.2}	045 460
	410	072	057	470 ^{50.2}	403
	072	616	073 = 00.5	045	026

410	402	295	276	277	600
404	294	55	222	275	244
225		270	52	747	225
467	41+1	262	407	462	272
24 276	225 272	220	222	241	411
244	52 212	271	225	222	277
227	242	222	271	272	400
disorder minimum to quite large	225 276	52	270	226	276
207	221 276	54	52	227	271
227	reduce 202 225	222 = 28	274	52	400
477 = 61.2	4.0 + 1	220	277	327	225
470	52 470	276 415	222	400	112
220	222	272	225	225	221
242	55	401	272	444	220
221 = 28		225 267	400	271	224
221	4.1 + 1	462	456	272	275
261	271 ^{28.9}	221	226	241	271
21	224 ¹⁴ 402 = 42	270	276	272	271
25	460 = 57.4	224	240	412	52
242	57	420	272	52	276
24	226 ²¹	217	227	271	271
1 467 (100) ²⁷	52	52	271	240	244
467	222 257 ^{14.2}	276	254	272	227 = 28.7
401 = 39.8	274	264	227	272	240
40 677 = 180	52 212 ¹²	454	224	272	272
225	242 ¹⁶	271	277	272	221
52	110	220	224	275	273
77	221	222	404	271	225
402	462 ^{100.4}	477 = 62.8	371	275	272
66 ^{57.9}	265 620	222	271	225	
264	322 ²⁰	241	240	272	
221	222	401	224	276	
670	404	276	265	52	

no ⁺⁺²

- gas in, Me, no pin.

- align (point gas signal)

top up cage, pump out.

4.1 + 1 still

277

272

477

271

277

272

236

241

272⁼¹⁵

271

277

450

72

272

274

277⁴⁸

272

272

272 > 275

272 > 275

272

240

277

77

277

372

52

374

4.2(1+1)

277

247

276

617

55

245

204 712

274

52

222

275

74

270

276

222

271

4.7+1

277

277

277

204 1127

277

77

9607

277

57

272

416

275

52

327

277 462

276

277

272

270

260

260

270

401

275

276

279

405

2001

276

276

274 402

275 = 277

276

272

276 272

276

276

277 455

455 = 59.1

275

276

340

274

274

277

271

276

275

271

275

2002

276

205

51

277

52

51

57

277

275

57

277

275

276

279

277

271 261

276

275

275

57 246

407

271

57 274

277

270

275

271

4.4+1

272

277

274

272

270 274

275

274 401

271

277

270 271[?]

276

277

274

277

270 272

272

270 274

277

275

277

272

276

275

277

446

270

276

4.5+1	275	520	50215	221	51
211	201	251442	227225	574	150
212	217	88216	50216	226	216227
512+7	217	216204	225454	5	206
222	215	226	227207	2514	212
213	221	212	410	220	220
214	221	216	222	426	215
216	262	216	207	226445	261
215	451	443701	51216	621	51
220	217	275	254	491	517
216 ²⁸	221	214	671	224	220
222	606	214	555	222	217
217		445	206	206	257
52	4.62+1	466	255	427	210
215	257	215221	225	226	215270
214	257	261	450	58226	51444
225	210	215	225	5	
213	52	220	220	206	<u>4.871</u>
217	220	220	270	257	212
215	211		441	227	226267
216	217220	<u>4.7+1</u>	215	176222	205
217	260	227220	440457	207	435
215	261	220	441	227446	51217
215	211	210	212	242	214
217	222	210	215255	516	50
217	245	215405	50407	226224	51
215	220	214	257	206	427
222	216	442	227442	206	440
215	407	52	207441 ⁶⁰	206	51
220	261	457	202	561 ⁹⁵	222
226	214	51204	274	215	226
226 ^{15.2}	50210	221	1422	262 ⁴¹	
212	51216	226516	227210	400	

4-9+1
 320 264
 50
 224
 52 214

5+1
 221
 261 422
 212
 262 421
 216
 272⁴⁶ 445²⁷
 4 7
 211 422
 50 222
 50
 220
 226

240
 222 201
 244 222

 5-2+1
 221
 424
 222 221

5-2+1
 222

5-5+1
 177
 601
 gas in, check balance, ok 27
 - ? popped

 - no more work

8+1
 752

 8-2+1
 421
 27/162
 106
 25
 27 416
 111
 416
 24
 27
 26
 27
 61 72
 27 19
 105 416
 40
 104

Now \downarrow @ 9kV
 - b/w 8-64 & 2
 - dirty w
 - ~~cleaner~~
 - cleaner, plus
 - end of file.

521 + 1
 275
 202
 215 261
 57
 212
 227
 222 201
 214
 272 425
 556
 420
 222

Argon in \rightarrow b/w 7-9kV 422
 - ^{blank (7.98)} plus 20

 7-9+2
 421
 27
 40
 145
 106
 26 - lot of H

422
 107
 36
 112 160
 40
 160
 27
 160 = 14
 222 = 85
 416

Calibration from lv	245	244	244	150 271
12.1+2.5	26 277	151	275	247
	151 244	250	150 244	157 272
240	152 244	274	72	157
150 270	26 244	155	151 245	150
152 244	150 242	151	244	150 240
151	161	151	274	157 245 ^{94.2} _(95.6 96.6)
152	151 270	150 272	1074	246
245	246	160 244	270	157 244
151 271	274	154	152 244	157 270
1161	26 270	156 244	270	157
246	150	272	245	150
1775	245	342	247	157
150 244	151 244	237	2775	152 270
247	242	215	270	152
274	275	245	2004	240
247	151 272	150 242	150	157 240
152 270	26 272	156	156	272
50 242	26 246	150 240	244	152
150	274	274	150 270	244
151 244	151	151	152 245	247
250	245	150	156 270	240
271	160	151 270	242	1250
245	26 272	245	252	240
274	272	151 244	152	270 ^{62.7} _(63.6 64.3)
147	26 146	244	152	272
272	26 270	1411	245	146
270	26	72 157	151	152
245	240	156	240	157 272
150 240	146 270	150	156	157
50 247	246	157	152 245	152 270
157 270	150	145 244	157 245	270
151 275	245	245	154 244	244

Manipulator modified \Rightarrow S-S EN585 springs & also endplates
on pulley to stop wire jumping off.

Mic baked \Rightarrow cryostat leaked.

Rebrazed.

" - leaked.

"

" - fitting of ss tubing where solder wouldn't wet it.

- rebaked \Rightarrow 110°C cold 210°C warm. 14/6/78.

4/6/78 R Dugay's specimen 10227-23 (G-L alloy)
 Fe/Si 3:2 + 100 wt ppm P 100 S 1 ppm D 20-50 Mn
 12 μm grain size 20-30 C

+ grain boundary near tip,
 50 K $5 \cdot 10^{-5}$ background $2 \cdot 10^{-5}$ Ne

N-pulse

6 shots @ DIV @ 5.87 KV
 15 pulse 1KV

6 - @ 5.95 KV

Match → 6 @ 7.27 KV
 Ne in ~~6.61~~ × 6

6 + DIV 7.26 KV Ne - bdary



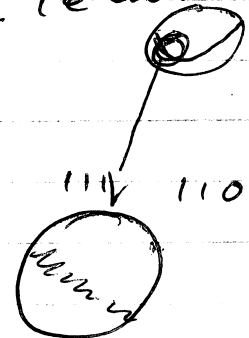
align on IAP

Fe²⁺ 28 ⇒ 65 orbit

Si²⁺ 14 ⇒ 37.5 ns = 46-45 orbit

Fe in real space

7.71 KV × 6 DIV



Dark 6 IAP

11 ± 124 DW 7-71 $7 \cdot 10^{-5}$ Ne

More slightly 6 × DIV @ ~ 6.8 KV



6.87 + 4

Fe²⁺ 20 or 65

7.6 + 1.4

Si²⁺ 20 or 40

DIV × 3



More

DIV × 3



Fe 20

Si 20

Fe 20

Sc 20 ground

cp norm

Niphr/pentox) DW x 6.

- bidury gone - H clth - note seen.
erupt to 10KV.

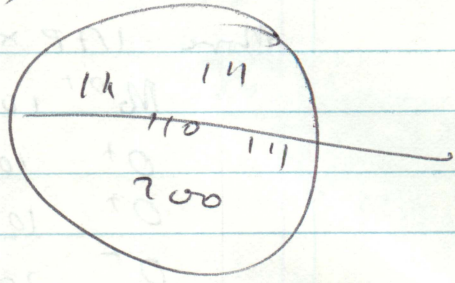
back to 1AP

3 x DIV, 200 centre (200 centre of top row, not 100)

9.33 + 2KV.

- flushed

15/6/78 Mo gb $2 \cdot 10^{-10}$ (Coulby H valve)
 50 He $2 \cdot 10^{-5}$



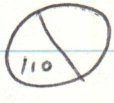
8KV DIV $\times 3$ & $\times 1.8 \times 3$

IAP 110 DIV $\times 1$

1

Na film 2

IAP 110 DIV 8KV

4 gb DIV 

$7.6 + 1.4 \text{ } ^{22}\text{Mo}^{7+} 65 = 520$

$^{48}\text{Mo}^{7+} 103 = 670 = 650 \text{ calc.}$

$^{16}\text{O}^+ = 275 \Rightarrow 46$

$8 = 265 = 33$

$6 = 220 = 27 \quad 25$

$12 = 225 = 41$

$\text{He}^{+4} = 287 = 22$

IAP $\times 2$

Mo^{7+} 10 planes 20 sec

$\text{O}^+ \sim 30' \text{ } 49 \text{ } \checkmark \text{ little}$

$\text{O}^+ \sim 30''$

IAP $\times 3$

Mo^{7+} 10 planes 10 sec

$\text{O}^+ \leftarrow$ dud - wrong time

$8.4 + 1.5 \quad \text{O}^+ ?$

$\text{O}^+ 43$

IAP $\times 2$

Mo^{7+} 10 planes

$9.1 \text{ } 105 \quad \text{O}^+ \sim \checkmark \text{ little}$
 $\text{O}^+ \sim$

IAP x 2

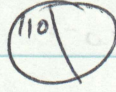
More IAP x 2

M_0^{2+} 10 μ m

O^+ 10

O^+ 10

O^+ 20



v little
↓

IAP x 2

More IAP x 2



↓

short-
change time
2KV pulse

M_0^{2+} ~ 12 μ m

O^+ "

O^+ more

10.9 + 2

Myth 3

IAP x $\frac{1}{2}$ day

M_0^{2+} 10

O^+ 10

O^+ 30

O^+ 10 non
required



50↑

100Hz

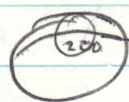
flushed

Background Fe/Si 1/gb $2 \cdot 10^{-10}$
 $4 \cdot 10^5$ Ne 160

6 x DIV ~ 9 kV

Helix

g-b



6 x DIV

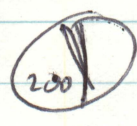
Helix

6 x DIV ~ 10.5

9.48 + 2



1AP 5 x DIV



- crossing electronics - change to old delay line

H2 ↓ ↑

DIV x 3

Fe²⁺ 20 sec

Si²⁺ < 26

1

1AP DW x 3 or 4

HC grotty again - fix
 blank

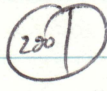
Fe²⁺ 60 20 sec

Si²⁺ 40

1AP DW x 4

PH DW x 4 - end of data

1AP DIV x 4



Fe²⁺ 25 sec

Si²⁺ 20

Si²⁺ - pop

1AP DIV

Multiplex

1AP DIV x 7

Fe 53

SE

2

$$So \tau = 450 \text{ ns} = 53$$

? ? @ ?

Si 35 sec

IAP DW

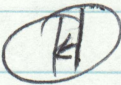
Fe 2+ 20 sec

Si 4

Si 2

Si - prep

10KV+2-2 IAP DW

Fe 20 sec ea  100 Hz

Si 4

Si 4

Si 4


Fe 4

Si 4

IAP < DW

< > DIV

< < DW

Fe  20 sec ea

Si 4

Si 1

Si 4


Fe 20 sec

Si 4

IAP DW < >


end of ph.

2 x Na films

pth op lots x DW - flare at corner 

↳ Blank

IAP

 I think



7e

Sc slight pos

Sc

Sc sp

7e

Si sp

1AP DW x>

2 slight more DIV x>

7e

Si

C²⁺ } little seen (20)

C²⁺

7e

Si

Si

47

1AP DIV x>

1AP DIV x>

7e

Sc

Si

7e

Sc

Si

1AP DW x>

end of line

light DW

4

Sc

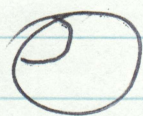
7e

Sc

Si

DIV

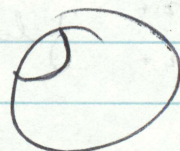
Si
 Fe
 Si
 Si
 DIV x 2



11.5KV + 2.6 ↑

Next day 16/6/78

IAP { Dunch
 Sando @ DIV, 11.92 KV



IAP Muffin

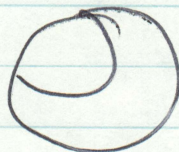
IAP DWK 405
 as DIV x 2



11.28 + 2.6

Fe²⁺ 40 sec
 Si²⁺ 40 "
 Si²⁺ 60 "

IAP (DIV } 6 or 7
 IAP DIV }



Si²⁺ 40 sec
 Fe²⁺ "
 Si²⁺ "
 P₁S⁺ "
 P₁S⁺ "


} ie tail of Fe²⁺ pin

IAP DW x 6 or 7

More IAP DIV x 2

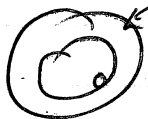



Si 60 sec
 Fe "

Σ_i 50
DIV $\times 2$
IAP Mph
IAP hls @ Dev 

ph CP 12.32 x 2 .

Mh  plane



 better

ph DW

extract ~ 12rev

16/6/78 Gold

PFM's Fe/Su 610^{10} (u) 160/Ne.
blank

phcp $\sim 1 \frac{1}{2} \sim 2$ DW 10KV

+2 DW

+2 DIV 40KV

? dishes loop $\textcircled{1}$
2KV 3+ DW

- flushed.

Newtip Mo/O gb ex same.

510^{10} (50/He (some Ne/He))

pop \Rightarrow 8KV - 10KV \#

pk 10KV DW $\times \rightarrow$



IAP DW $\times \rightarrow$ 10.67KV



IAP $\frac{1}{2}$ day @ 6V small evap.

10.5 + 1.1

$^{57}\text{Mo}^{3+}$ 57

$^{48}\text{Mo}^{2+}$ 71

$^{16}\text{O} = 332 = 41$

$^{20}\text{Ne} = 271 = 45$

$^4\text{He} = 166 = 21$

$^{14}\text{N} = 83 = 10$

Mo^{2+} 20 sens 57

O^+ 20 sens $\sqrt{\text{little}}$ 41

(lots of Ne^+ @ 45)

IAP hr $\times \rightarrow$

Mo^{2+}

O^+ little

DIV x 2 11.69

More, pulse to 1-5,

IAP DW x 3

12.07

M₀ + 54 = 440

M₀ + 2000 55,

0 + 4

0 + 25576

IAP DW

u M₀ + 54 2

IAP < DW

4 more (DIV 12.7)
2 DIV

M₀ + ? - page,

Handwritten

Div 11 11

1111 1111

1111 1111

1111 1111

1111 1111

1111 1111

1111 1111

1111 1111

1111 1111

5

1111 1111

1111 1111

1111 1111

1111 1111

1111 1111

1111 1111

26/6/78

PTMS

Te/sn ex p/c dp g-b

410'10 (Hank) 60K

Ne 310'5

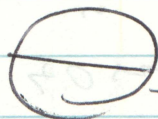
(Mtn)

4 + DIV 12.09KV

ph sp

1/4 ± 1

+ ph x 2



1AP DIV x 4



11.5 + 1.8

Te 2+ @ 53 = 420ns

6 2+ = 24 = 24 22

2+ = 281 = 24

Ne + = 263 = 44

SN + + = 618 = 76

SN + = 890 = 131 11+

SN + = 710 = 107 101

SN + = 507 = 63 55

1AP Te 2+ 40 sec

2+ 40

2+ 40

SN 2+ 40 sec

SN 2+ 40 sec

1AP x 0

Te 2+ 20 sec

SN 2+ 22

40

2+ 30 sec - like

1AP SN 2+ 20 sec
long changing line
1AP x 2 GW
units

lunch

Thank

DC exp $S_{in} N_c 12.12KV$

pulse to ~~12~~ 2KV / IAP x >

More slightly towards edge

diff DW

IAP x >

IAP Multiple

2

u DW x >

Fe²⁺ 40 sm 52

Sn²⁺ u ~ 74

Sn²⁺ u

C²⁺ 20 22-23

C²⁺ 40

IAP DIV x >

Sn²⁺

Sn²⁺

Fe²⁺ 20 sm

Sn²⁺ 30 rapider ~ 72

Sn²⁺ 20

IAP x >

~~Sn~~

~~Sn~~

C²⁺ 40 sm

C²⁺ 40

Fe²⁺ 20

Sn²⁺ 20

Sn²⁺ 20

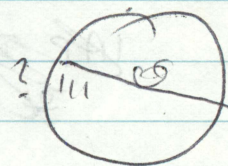
Sn²⁺ 20

2 in tail of Fe²⁺ peak

IAP x >

More across centre to RMS

~ 12KV DW IAP x 4ms



Fe²⁺ 50
Sn²⁺ 71

IAP Naphtha)

DW x 4

pub 62-3. HDKV

Fe¹

Sn

Sn

Sn

?

|
raped - not a lot of Cu

|

DIV x 3

HC ~~step~~ set dodgy - wrap

Fe²⁺ dual

Fe²⁺ 20 runs

Sn²⁺ 20

Sn²⁺ 20

Sn²⁺ 20

Sn²⁺ 100

Fe²⁺ 20

Sn²⁺ 50

↓
raped

≈ 5 planes I think

IAP DW

Flashed.

C

Handwritten notes on the left side of the page, including a vertical line and some illegible text.

Handwritten notes on the right side of the page, including a vertical line and some illegible text.

Handwritten notes in the middle section of the page, including a vertical line and some illegible text.

Handwritten notes at the bottom of the page, including a vertical line and some illegible text.

28/6/

Poshunting works! I think!

T247 Mo / 10^{-5} He / 60 / $2 \cdot 10^{-9}$ bkgnd

9.4 + 1 \rightarrow 1.13

\sim {00} region

T248 Mo / var / 9.4 + 1.32 keV

$- 5 \cdot 10^{-10}$ bkgnd

30/6 Mo 110^{-9} /60 postheating

1st spectrum 10KV, +1.35 pulse 4×10^{-7} He 60

Postheating aligned @ detector

-2.26 + 1.95(2)
from VG set 'b' energy.

T 249

2nd spectrum 10 + 1.52

No gas same analyzer settings

PFM modified program so plots time bins as well as mass to eliminate bin -itis.

Lot of spurious characters on tape - ? electronics stuff.

3/7 Some Exp $\sim 110^{-9}/60$

It passes now $\text{km} \pm \text{kt}$ - you on performance.

7280 a110 He b var \sim same alignment as before.

7281 a110 He b var in bright area ~~at~~

- rechecked so is on axis of detector (at-RH side).

Mo
92
94
95
96
97
98
100

$$\frac{dm}{m} \approx \frac{1}{2} \text{ or } \frac{1}{96} = \frac{1}{48} \text{ or } \frac{1}{96}$$

$$f = 2.6 \mu s \pm$$

$$\text{or } 3.2 \mu s \pm$$

$$\Delta t = \frac{1}{2} \frac{dm}{m}$$

$$\therefore \Delta t = 2680 \times \frac{1}{48} = 26 \text{ ns for } 27 \text{ or } 32 \text{ ns for } 2^+ \text{ peaks}$$

or 12 & 16 for other isotopes.

\therefore Limit resolution $\sim 100 \text{ MHz}$ clock. ($\pm 10 \text{ ns}$).

\therefore Limit Δt error $\Rightarrow 200 \text{ MHz}$ error or phase-locked clock.

4/7 Same Exp 110^{-9}

T282 a He / rapid with ^{detector} pulse now 50 ns long
to try to avoid jitter in timer.

5/7

Rebuild min to fix 117 insulation, remove loose ends of braid, & put ss wire rope onto manipulator. Postheating left alone.

Done 10 hrs on bakeout 1 only (dirty!!)

6/7 $\approx 2 \cdot 10^{-9}$ cold ($5 \cdot 10^{-9}$ hot)

T 283 New Mo Tip ~~X~~ write
a He 12KV + 2.04

Readjust amp to get less after pulses.

b var $1 \cdot 10^{-8} \Rightarrow 5 \cdot 10^{-10}$ eventually
same pulse (? dirty, gas present)
D1V 14KV.

Lots of ions at $m/n \approx 20$ - ? leaky Ne bottle or
Ne in the helium

Try again tomorrow to see if still there

PFM's prog apparently putting zeros into time spectrum (adding
some adjacent bins together).

7/6

3×10^{-10} cold, 60

T 284

a He 3×10^{-8} same place as yesterday ^{~ 14 KV} ~~14 KV~~

b vac ≈ 200 more pulse.
1000 + 1000

T 285

a He 1×10^{-7} same place as 284 12.5 + 2.18 KV
1000 \bar{m}

analogue voltage slightly higher than before

b vac 3×10^{-10} same condition 1000

Peak @ ≈ 20 still there

~~T 286~~ Ne 5×10^{-8} 60

~~~ 12.5 + 2.18~~

to see if new  $\approx 20$  peak or same one.  
background  $< 3 \times 10^{-10}$

1000  $\bar{m}$

I think 591

T 287

through-focus series

Exp hp

13.15 KV  
517 pulse 2.18

a 305 on HT pot

ratio 4.91

300  $\bar{m}$

b 310

"

"

c 315

"

"

d 320

"

"

e 325

"

"

f 330

"

"

Pressure  $1 \times 10^{-5}$  Ne (inadvertently!)

~~T 288~~

~~13.5 + 2.2~~

~~Exp hp 546~~

~~328~~

~~565~~

HT set increasing - abandon top

607  $\mu\text{m}$  H $\gamma$   
 15.63  $\mu\text{V} \Rightarrow$  focussed  
 15.98 = 556

$14.16 + 2.18 = 16.34$

$\Rightarrow$  focussed

552      2.23  
 T288, 14.05 + ~~2.42~~ = 16.28

b 14.05 + 2.30  
            $\downarrow$   
           2.25

$17.05 + 2.25 = 16.5$

Empirical ratio

318 H $\gamma$       565

320      "

best focus at this ratio at 15.98

$\downarrow$                        $\downarrow$   
 320      565       $60.2 \times 10^{-7} \text{ W}$   
 324      585       $\Rightarrow 3 \times 10^{-9} \text{ W}$

322      605       $1 \times 10^{-9} \text{ W}$

Tip H7 8.31 = 219 on height

Deflection 167 / 591 ratio

$5 \cdot 10^{-10} / 60 \quad / 1 \cdot 10^{-8} \text{ He}$

T289 7.00 + 1.10 167/591

- v patchy erosion, bursts of ions

? too close to 110 center

680 ions

grain boundary coming in from top,



Notes

Pico - not all on frame

more common around

more DIV,

p-h over b'dary

double focus  
obtaining

Spectrum 9KV + 1.25

235 - 545

type 290 - broke after 180 ions - restart.

check after 400 ions  $\bigcirc$  still

$1 \cdot 10^{-8} \text{ He}$

type high-resolution

T291 9.4 + 1.5

900 ions, still under p-h



10/7/78 Same top  $510^{-10}$  60

realign

blank

He  $10.54 \text{ kV} \times 3 \text{ DIV}$  c-p ph



T292 267 = 9.45 + 1.58

229 1575 ratio

(helium  $210^{-9}$ )

Inspect - @ 1200 ions - still under ph



collect 2000 total - still under ph



blank

DIV  $\times 3$  ph

more so axial -  $6 \text{ DIV}$  ph  $\times 4$

IAP DIV  $\times 4$  11.14 kV He 60

30' 3+ 60 = 480

44 2+ 70 = 590

16 = 40 = 348

20 = 47 390

24 = 50 425

He 21 170

Mo<sup>3+</sup> 50 ions

O<sup>+</sup> 50

O<sup>+</sup> 50

Ne<sup>+</sup> - accidental 20

IAP DIV  $\times 3$

" -  $\times 3$  slight more



Mo<sup>3+</sup> just in 40

O<sup>+</sup> " " v little seen

O<sup>+</sup> "

? O<sup>+</sup>

(IAP  $\times 3$ )

more 1 IAP  $\times 3$

Mo<sup>3+</sup> 40 ions

long c-l

as



~ 11x2

0+ } long c-l ~ 40-41  
0+  
0+

IAP x 3 ~ 11.5

M<sub>0</sub><sup>2+</sup> 40 short c-l

0+ 40

0+ 100

0+ 40

M<sub>0</sub><sup>2+</sup> 40m 8 planes counted

IAP DIV

IAP Mph

IAP x 3

ph bit x 3

IAP x 3

M<sub>0</sub><sup>2+</sup> ← M<sub>0</sub><sup>2+</sup> 40 hrs

0+ 4

0+ 4

0+ 1

M<sub>0</sub><sup>2+</sup> - flushed -

New Mo spec

$3 \times 10^{-10}$

T 293

$5.26 + 1 \text{KV}$   
293

121/595

200 cm only

wound tip up to  $\approx 14 \text{KV}$  - no boundaries  
- checked

T 294 Method is round robin tip

- v odd for picture  $\phi$  bright  
line down tip? g-b? overlapping? turn

Protocol over boundary - analysis

9.4 + 1.3KV

216/560

@ 200 cm scale over boundary

384

DW ph

DW axes

- ppt! s

Tantalum carbide + nitride

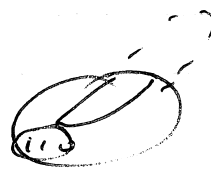
500 cm spectrum = T 294

Next day

210<sup>-10</sup> / 60 (rel + no)  
Dlunk  
IAP DIV x 4 ~ 11.5KV

10.05 + 2 crupts

19pt



? Mo<sup>3+</sup> 60 = 510ns

He 22 = 180

C<sub>6</sub> 26 = 224

C<sub>12</sub> 27 = 217

N<sub>14</sub> 42 = 242

Ne<sub>20</sub> 51 = 409

Ta<sub>60</sub> 107 = 709

Ta<sub>90</sub> 127 = 868

Ta<sup>3+</sup> <sup>Dlunk</sup> 60 sec

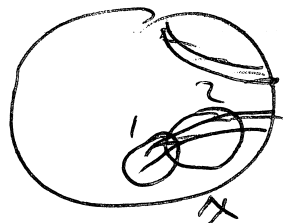
Mo<sup>3+</sup> 5

C<sup>+</sup> 4

N<sup>+</sup> 100 sec

IAP x 3

More IAP x 3 or 4



Ta<sup>3+</sup> 60 sec

Mo<sup>3+</sup> 4

C<sup>+</sup> 4

N<sup>+</sup> 80

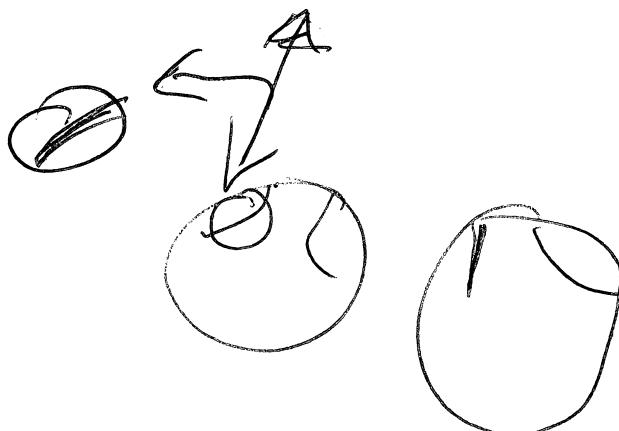
IAP x 3

ph op Mph

3AV x 3 or 4

< DIV x 2

12.15KV



10

ph cp bir x 2 or 4  
ph just outside ppt-

T 295

11.41 + 1.52  
" 452

266/561

~ 500 ions

to ionize  $2 \times 10^{-8}$  He during first 200 ions

Timer must had dodgys - fixed.

10

T 296 Matrix away from ppt-

11.60 + 1.70  
" 456

$4 \times 10^{-8}$  He/Ne

270/561

~ 600 ions

ph @ div ph cp.

14/7 Same Exp Mo V Zn  
2.5-3  $10^{-10}$  background cold,  $5 \times 10^{-10}$  warm  
110

T297 12-31 + 1.43 ( $\approx 10\%$ )  $3 \times 10^{-6}$  He+Ne ( $\approx 1 \times 10^{-5}$ )  
485 78 K 284/561  
13.1%

T298 12-67 + 800  $\approx 5\%$  methane  $3 \times 10^{-6}$  He/Ox  
538 317/561

T299 12-47 + 2  $\approx 15\%$   
492 300/561

15-23 July 1FCS Albuquerque

- paper on combined IAP/Poscherting.

28

26 July 78

Same MoV Za Zep

$4 \times 10^{-10}$  78

expt - 15.1KV in He/Ne

Spectrum T300 13.80 + 1.60 320/561  
 $2.10^{-7}$  He/Ne 78 542

T301 14.00 + 2.00 320/561  
530 var r. pump out over lunch

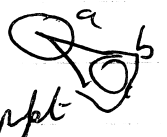
- bit fast! - reduce to 1.70 pulse after 900 ions  
HT set unstable, stop after  $\approx 1000$  ions

T302 14.16  
 $\approx 14$  KV new ht set + 1.8 320/561  
var (ht down & up, expt  $\approx 250$  ions before spectrum)

T303 14.16 + 2 var 320/561

gas in  
More Exp, ~~var~~ blank DIV  $1\frac{1}{2}$   $\frac{1}{2}$   
- defect in Exp  
- under p-h  $\frac{1}{4}$   $\frac{1}{2}$  1  $3000^+$  ions

T304 off defect,  $1.10^{-7}$  He/Ne, 78 348/561  
a, b 14.28 - 14.70 + 2.15

stop after 200, new spectrum, pnd x 2, align or new ppt   
14.7 + 2.15 352/561

input @ 500 ions - continue  
- ? ppt or funny endform.  
Exp extracted

New tip 1x polish in cold cath 2.5V ac

- lot of ? twin boundaries -  $\mu\text{m} \sim 5-50 \text{KV}$

Spectrum T 305 5.2KV + 1KV He  $3 \times 10^{-8}$  (+Ne)  
124/584

Stop after 200  $\mu\text{s}$  cos background noise on spectrum

T 306 5.6 + 1KV  $3 \times 10^{-7}$  He ~~128~~ 128/584

111/581



Some tips sprayed 20 min in Mond / Methanol detented 1110 with methanol - freeze dried

4.55 + 1

111 / 561

- 480°C x 2 min

T 207

~ 250 ions

115 / 561

- popped several times

T 208 a 12 kV + 2 kV, He  
- clean lv - 2.16 kV

003 / 570

b - 2.16  
- 2.27

u u

↑  
- to check energy focusing.

5.50 kV = 110/561 on analyser.

∴ type in  $\frac{5}{2} \times$  analyser settings as tip volts.

Pulse volts A-DC  $\Rightarrow$  0.01  $\mu$ s.

look up to  $\approx$  120/561 - 120  $\mu$ m, lot of H.

look @ tip in Ne - no image up to  $\approx$  7 kV

- looks as if cap gone, something at edge.

- align  $\approx$  on film at very edge of tip.

T 310                      162/561                      6.72 + 1.2 kV  $\uparrow$   
                                          $\rightarrow$  180/561                      - 7.3

$\approx$  410  $\mu$ m.

T 311                       $\rightarrow$  9.3                      210/561  
off axis - slatium oxide?                       $\approx$  210  $\mu$ m

1<sup>st</sup> August

Next day  $2 \times 10^{-10} / 60$

same tip 1x/coated

Ne  $2 \times 10^{-5}$  - DV

Mplu phase

DIV  $\times 4 \sim 9.53$  ( < DV )

↑ ph over oxide @ edge, where yesterday's spectra taken from.

- \$ popped while signing.

min

|                       |           |       |                      |                                  |
|-----------------------|-----------|-------|----------------------|----------------------------------|
| (6.72)                |           |       |                      |                                  |
| <del>12.02</del>      | found max |       | 386                  |                                  |
| 12.24 - 18.76         |           |       | <del>243</del> / 561 |                                  |
| 14.77 - 16.50 - 18.07 |           |       | 340                  | on ox                            |
| 12.05                 | 14.56     | 16.5  | 200                  |                                  |
| 11.27                 | 12.66     | 14.29 | 260                  |                                  |
| 9.48                  | 10.56     | 12.07 | 220                  |                                  |
| 8.25                  | 9.28      | 10.80 | 190                  | ( different phase on tip, off ox |

T 212 off matrix of 1x tip  $1 \times 10^{-7}$  He/Ne/60

$\sim 7860$  counts / 200 / near zone lines

@  $\sim$  exact focus

397 / 561

\$ \Delta 19.2KV total

2.76 pulse

SAM's Ne AC / ppts

210<sup>10</sup> Ne / 60

DW ~ 15 KV

- spots

align on ~ axial ? ppt.

T 213 a 14.2 + 2.65 @ 260/561

110<sup>-7</sup> Ne ~ 1000 cm

- image - no ppt now



ph BIV 14.2 KV x3

ph DW ~ 16 KV x3

T 213 b New system 110<sup>-7</sup> Ne / 60 14.2 + 2.65 260/561

2x < DW ph

DW ?

More to ppt



T 214 14.3 + 2.65

check @ 500 cm - ppt still ok

260/561

continue 110<sup>-7</sup>

~ 1,000 cm

Blank

ph < DW x 3

BIV x3 - pretty!

BIV x2 f1.8

Go home.

Flashed on turning system

3/ Aug / 78

Repolished Ni/Al

3, 10<sup>-10</sup> / 60

- faint picture

TJIS between 220 & 110, 1/10<sup>-7</sup> Ne  
4 x DW Ph Cr 8.9 KV

2.41 + 1.4KV  
(hard to align)

IAP DIS X 3 (111)

10<sup>-8</sup> Ne  
gas present

|                  |        |                  |
|------------------|--------|------------------|
| Ni <sup>2+</sup> | 40 sec | 5 planes counted |
| Al <sup>2+</sup> | "      | "                |
| Al <sup>2+</sup> | "      | "                |
| Ni <sup>2+</sup> | "      | 6 planes         |

IAP x 3 10, 4, 1 (faint)

gas down

|                  |        |          |
|------------------|--------|----------|
| Ni <sup>2+</sup> | 40 sec | 8 planes |
| Al <sup>2+</sup> | 40     | "        |
| Ni <sup>2+</sup> | 40     | "        |
| Al <sup>2+</sup> | 40     | "        |
| Al <sup>2+</sup> | 80     | "        |

background between Al & Ni peaks 40

IAP x 3

→ 220 IAP x 3

|    |         |
|----|---------|
| Ni | 40 sec  |
| Al | "       |
| Al | "       |
| Ni | "       |
| Ni | quicker |
| Al | "       |

10 + 2 KV

IAP x 3

IAP x 1

counted slightly

→ ? lamps (10)

|    |        |
|----|--------|
| Ni | 40 sec |
| Al | "      |
| Ni | "      |

IAP Ni/Al

2

↓ night 2

IAP x 3 (200)

Ni 40

AC ~ 50ms

AC further - pop

Ni 40 sus further

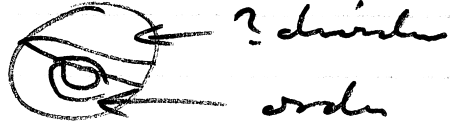
AC 50 -

IAP x 3

IAP

Ni

AC



product 57.2

— HZ at unstable - swaps

Ni

AC

Ni } ?

AC

AC

slightly { (AC ? Mg, C  
 (CAC ~ m = 12) (AC ? Mg, C  
 (Timer burst)

IAP x 3 or 4

Ph Cp x 2

Ph Nuph

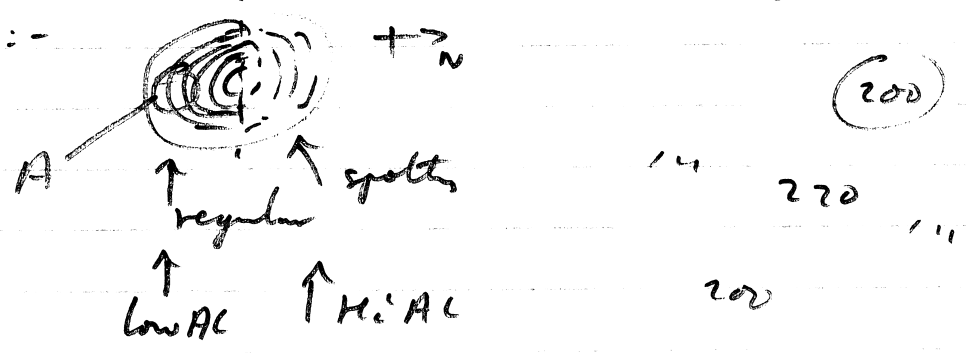
BW x 1/2 day

< DV x 2 →

go home time

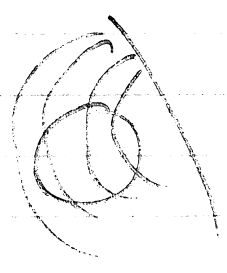
4/8/78 Same gun  $2.5 \times 10^{-10}$  / 60 / Ne.

- from yesterday's prod 200 crossed by some boundary :-



∴ Set up probe over 200 regular side A  
 $10.68 + 1.9$  // 257/290  $110^{-7}$  Ne

- T 316a
- check @ 500 count, still OK
  - check @ 1000 - OK
  - prod @  $< 4 \sim 31v$



T 316b more ph to check region - prod  
 $10.57 + 1.82$

T 317 Over interface  
 $10.96 + 2.50$  250/290  $110^{-7}$  Ne

- IAP —
- Depth
  - DW  $\times 300 \pm$  of 200
  - Ne  $2 \times 40 \times$
  - Al  $2+$  : slight  $10^{-7}$  c-p disturbance
  - Al  $2+$  -
  - Ne  $2+$  -
  - IAP  $\times 2$
  - Ne  $2+$  : 50% ground
  - Al  $2+$  -
  - Ne  $2+$  -
  - Al  $2+$  -



IAP v3

More background 220 (I think)

220 200

N<sub>i</sub>

AI

N<sub>i</sub>

AI

IAP

pk DW x 2 or 4 after physics

Dark GLMS ? !!!

⊖ ?

IAP x 2

N<sub>i</sub>

AI

N<sub>i</sub>

AI - prop

IAP x 2

pk ops x 2 1/2 1/2 1/2

crypt-DC pk ops 1/4 1/2 1

IAP after nd error, bottom of trap

N<sub>i</sub>

AI

IAP N<sub>i</sub> AI

IAP x 2

N<sub>i</sub> final, 20-40 s

AI

N<sub>i</sub>

AI

IAP

back to pk - no ppfs.

- fast crypt -> ? dark shaped ppfs

- back to IAP

IAP x 2  $\rightarrow$  N<sub>i</sub> - apparently ordered

⊖

AI

N<sub>i</sub>

AI

IAP x 2

⊖



not blank

$\mu$

$\mu > 3$



218 a  $\sim 17 + 2$

290/570

115<sup>7</sup> N

1200  $\mu$  from opt.

218 b

from matrix



empt-  $\rightarrow$  more 'lenses'

$\mu$  DW  $\times 3$

IAP of opt. on bottom 200

Ni

Al

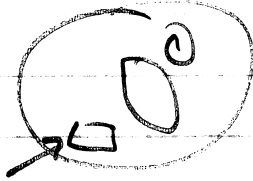
Ni

Al

IAP  $\times 3$

on limit of number

— 2.6 keV  
under  
18 keV  $\mu$

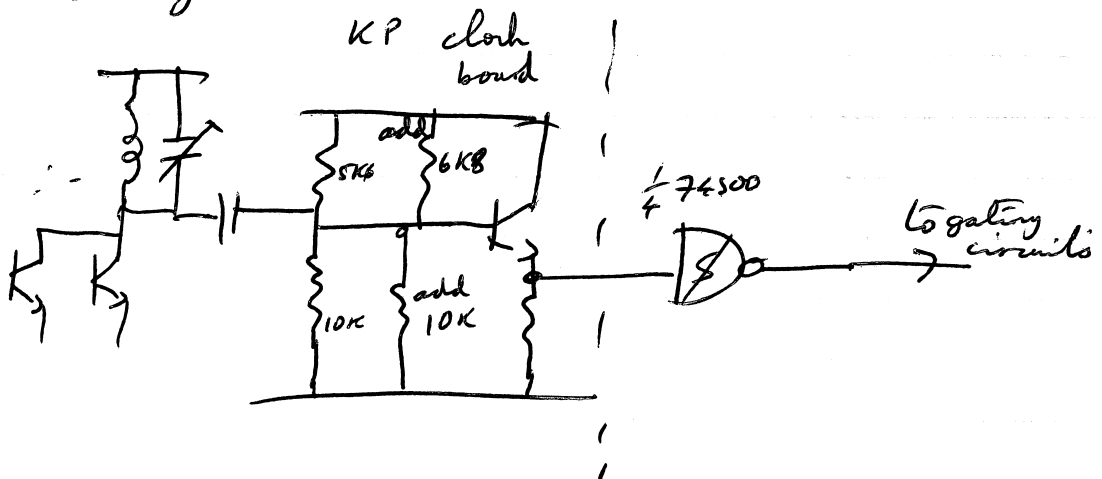


7/9

Friday activated alumina trapped to backing  
line of our diff pump (inlock) & modifying airlock  
so that purged out separately from top of diffstick.

Al<sub>2</sub>O<sub>3</sub> v wet! - needed 12 hrs baking with  $\frac{1}{2}$  trap heater  
to get < 0.2 Torr

[5/8 IAP timer adjusted, (clock not triggering electronics)  
so change



8/8 1r substrate preparation

2019 'amorphous' (not!) stainless steel Fe/Ni/C 30/15,

ex John Wood, as test specimen.

$\sim 7.5 \pm 1$  KV pulse 180/565  $2 \cdot 10^{-6} / 2 \cdot 10^{-7}$  Ne.

ARU) i/d new in operation.

$\sim 200$  ions flushed.

9/18 1x tip coated white cold with <sup>LiNe</sup> Mond 1 / Methanol 1.50  
 put on by dosing from a syringe,  
 vacuum dried  
 - cooked 5 mins @ 450°C in air

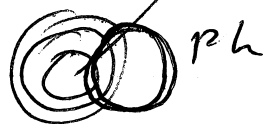
T 220a 8.1 ± 1.0  
 200/561 210<sup>-7</sup> Ne 210<sup>-10</sup>/50

~ 100 ions 1/2 pop need to exp volts ~ 400

T 220b 210/561 ~ 2 ions  
 exp volts - nil  
 260/561 11 ± 1.0

T 221 in He/Ne 370/561 390/561 @ ~ 16 + 3 MV  
 off layer on peripheral of 111  
 thro layer after 150 ions  
 - rate → much faster 17.15 ± 3

T 222 Peripheral 111 with converter on 200  
 ~ 3 planes erupted 17.15 ± 3  
 ~ 1500 ions in He & Ne  
 to see no of ~~planes~~ atoms / plane  
 400/561



9/8/78

lv printed Mandi 5mm / 450

T 223 8-12KV - not much of a file.  
 $2 \times 10^{-7}$  Ne / 60

T 224 PFM's Fe / Sn g b

$3 \times 10^{-10}$  / 60 /  $2 \times 10^{-7}$  Ne

11-11.5KV + 2KV 270/561

a on boundary checking each  $\approx$  200 ions - 1400

<sup>after washing</sup>  
pins @ 31V  $\approx$  12.5KV

b well away from boundary 110 centre of tip

pins @ 31V before probing.

11/8/78 Same gb 315" 160 / Ne

7025a off g-b. 2000 end

~12.0 + 2

300/561

keeping H<sub>2</sub> constant while ingesting gb

phop blank, 2014, after pushing

b Matrix 110 region axial

← pins axial for 2: v

14/8

Fe Sn gk IAP  
IAP D low

60/Me  $2 \times 10^{-10}$  cold

DIV x >



bottom of spec.

Fe<sup>2+</sup> 40 sec

46 380ns

Sn<sup>2+</sup> ? ~ 50 sec

20

C<sup>2+</sup> ? ~

22

IAP x 1

Fe<sup>2+</sup> 50s

Sn<sup>2+</sup> } v little seen

C<sup>2+</sup>

13.8 keV + '2-5'

IAP up

IAP x >

C<sup>+</sup> @ 30-32 50 sec

Fe<sup>2+</sup> 40s

C<sup>+</sup> 30 sec, pup

C<sup>+</sup> 50

IAP x 2

few more Fe<sup>2+</sup>, C<sup>+</sup>, C<sup>2+</sup> ?

- v little seen

IAP DW x >

More IAP DW x > top



C<sup>+</sup> ?

Fe<sup>2+</sup> long d

C<sup>+</sup> - pup

C<sup>+</sup> short d

C<sup>+</sup> ?

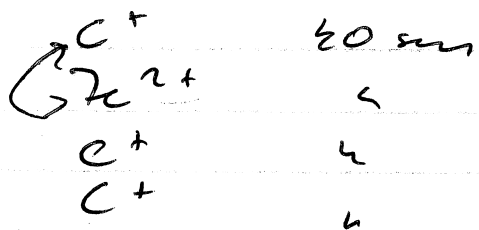
C<sup>+</sup> 100 sec

Fe<sup>2+</sup> 30 sec

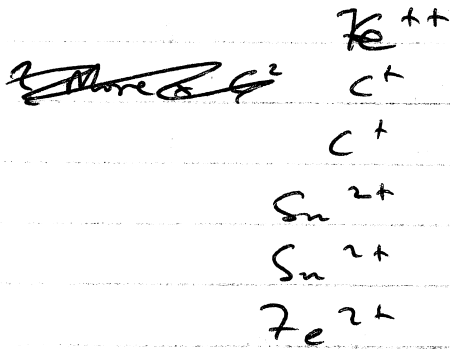
IAP x > pretty

ph DW x 5006

14.57



(APX)



(APX)



5/8

Some Fe/Sn gb

$\sim 10^{-10}$  vol

T 326



10.00 + 2.0 / 320/581

ph DW

ph DIV off ~~Q~~ over boundary for 326

IAP x 3 ~ 14-86 keV

|                  |       |        |          |
|------------------|-------|--------|----------|
| Fe <sup>2+</sup> | 45-46 | 60 sec | 14 + 2-4 |
| C <sup>+</sup>   | 30-31 | <      |          |
| C <sup>+</sup>   | <     | <      |          |

IAP x 3

|                                    |       |        |  |
|------------------------------------|-------|--------|--|
| C <sup>+</sup>                     | 30-31 | 40 sec |  |
| C <sup>+</sup>                     |       | 100    |  |
| Fe <sup>2+</sup>                   | ~45   | 40     |  |
| Sn <sup>2+</sup> , Fe <sup>+</sup> | 65-66 | 100    |  |
| Sn <sup>2+</sup>                   | 66-67 | 100    |  |

IAP x 2

More IAP x 2

|                                    |      |
|------------------------------------|------|
| C <sup>+</sup>                     | 70   |
| C <sup>+</sup>                     | 70   |
| Fe <sup>2+</sup>                   | 40   |
| Sn <sup>2+</sup> , Fe <sup>+</sup> | 70   |
| Sn <sup>2+</sup> , Li              | 70   |
| C <sup>+</sup>                     | ? 70 |



|      |    |     |
|------|----|-----|
| @218 | 70 | @36 |
| ~    | 70 |     |

IAP x 3

15-5 keV

blank, ph x 3  
cool stat, ph x 3

T 327

} off matrix on lower grain



13.00 + 2.35 320/261

T 328 off b'dary 3 10<sup>-9</sup> mag gas / 330/261 13 + 2-25

16/8 Ir coated mould 1/450/5mm  
sprayed with  $W_2$  propellant.

T329 N10 + 2 <sup>220</sup>~~300~~/240/581

off steel @ edge of top (centre cruddy Ir)  
except to 21KV in He

└ Mostly  $W_2$  but some ? Ru, Ti oxide concs at  
beginning of run.

17/8 Some legs recounted

7000 6.3 + 1.3

160/561

Holiday / cloudy advent for New Scientist for new res. stud. for P355/1111  
ch.

Difficulties plotting  $1x$  with  $Cal_2$  - that or elided.

20/9/78 PFM's Fe/Sn + % single xlat

ex 4 a/p to see if get  $Fe^+$  as well as  $Fe^{2+}$  (re grain boundary specimen which produced single  $Fe$ )

TB/a 11.15+2 / 280 /  $3 \times 10^{-8} Ne$  / 60  $2 \times 10^{-10} \text{ old}$

- 11.85 280/561

2000  $\mu m$

b New spectrum same place 11.5+2 280 / 561  $3 \times 10^{-8} Ne$

2000  $\mu m$

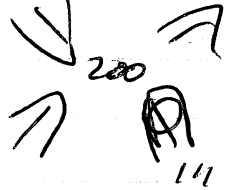
11.5 - 11.9

21/9/78

Same specimen Fe / Sn

T 332 off dash region near 200

100<sup>-9</sup> hot 210<sup>-10</sup> cold



a 11.5 + 2 / 280/561 60 / 310<sup>-8</sup> Ne.

11.6

11.7

11.8

11.9

2000 ions

b 11.9 + 2 as b4

back to 200 on 200 now dash / rugged

12 + 2

110 bits

200 -> writing end of trace

T 333 - on (now dashy) 110

300/561

12 + 2

300/561

210<sup>-8</sup> Ne 60

2000 all @ 12 kV.

T 334

12 + 2

12.1

12.2

300/561

after decreasing Bernier timer's minimum allowed time ( $RC = 270 : 2n2 \Rightarrow 270 : 1n$ )

same plane / volts => now lots of hydrogen (seen on scope previously but not recorded by timer) 2000

b

Back to dash region - now H but little Fe<sup>+</sup> (??)

1500

check after words, still on dash region, fuller image now.

System baked  $\Rightarrow 1.5 \cdot 10^{-10}$  (cold) on t-g  
 best  $0.2 \cdot 10^{-10}$  leak in cryostat (again)

Same Fe / Sr single xtal baked in nit.

27 / 9 / 78


c-p (chevron) outgassed by putting large  $Ne^+$  current on @ 2.4 kV applied volts, defocused spot, for  $\sim 4$  hrs,

Up detector sensitivity & chevron v from 2.1 to 2.2 kV to restore reasonable detn efficiency,

Spectrum 12.1 + 2      300 / 581       $3 \cdot 10^{-8} Ne / 60$   
 7 335      200  
 still lots of  $H_2$

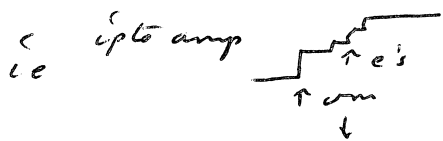
2000 ions @ one setting

$\rightarrow$  it was observed previous to adjusting the gain that when putting a wide ion beam onto the detector, & getting a lot of unfocused 'scattered' signal as well, that the scattered signal could be moved / almost eliminated with a magnet -  $\therefore$  ? electrons ? parity's ? electrons off c-plate



Calc suggests for 10 eV electrons  $t_{ion} \approx 3 ns$

so, if extra e's give extra gain, would get a late pulse from amp if didn't trigger on ion



$\therefore$  increasing / sensitivity of det-amp to just above noise level should improve time resolu

T326 Same tip same place, gas out  $\rightarrow 6 \cdot 10^{-10}$  (ugh)

except  $\sim 5$  ~~sec~~ 200 ~~sec~~ before taking spectrum,

H $\gamma$  12.3  $\rightarrow$  13.6 (!!) )

So spectrum 13.6 + 2 / 220 / 561 vac, 60 $^\circ$

13.6 - 14 KV <sup>rate is</sup>  $\sim$  insensitive to  $V_{tip}$

Much less H $\alpha^+$ .

? is neon (ie He or He $\alpha$ )



28/9/78

7027 Same tip UMRV (2310<sup>14</sup>) no gas at all

60

13-13.7 1320/561 1000 ins

+2

Some H.

7028 13.8 +2 1320/561

-14.2

1450 ins

q. rapid → less H.  
- flushed.

3/70/78 PPMs Fe/Sn  
g-b ex PPTdp

$< 110^{-10}$  background.

T 339

330/561  
350

2.2  $\mu$ m<sup>2</sup>/14.3 - 14.8 kV

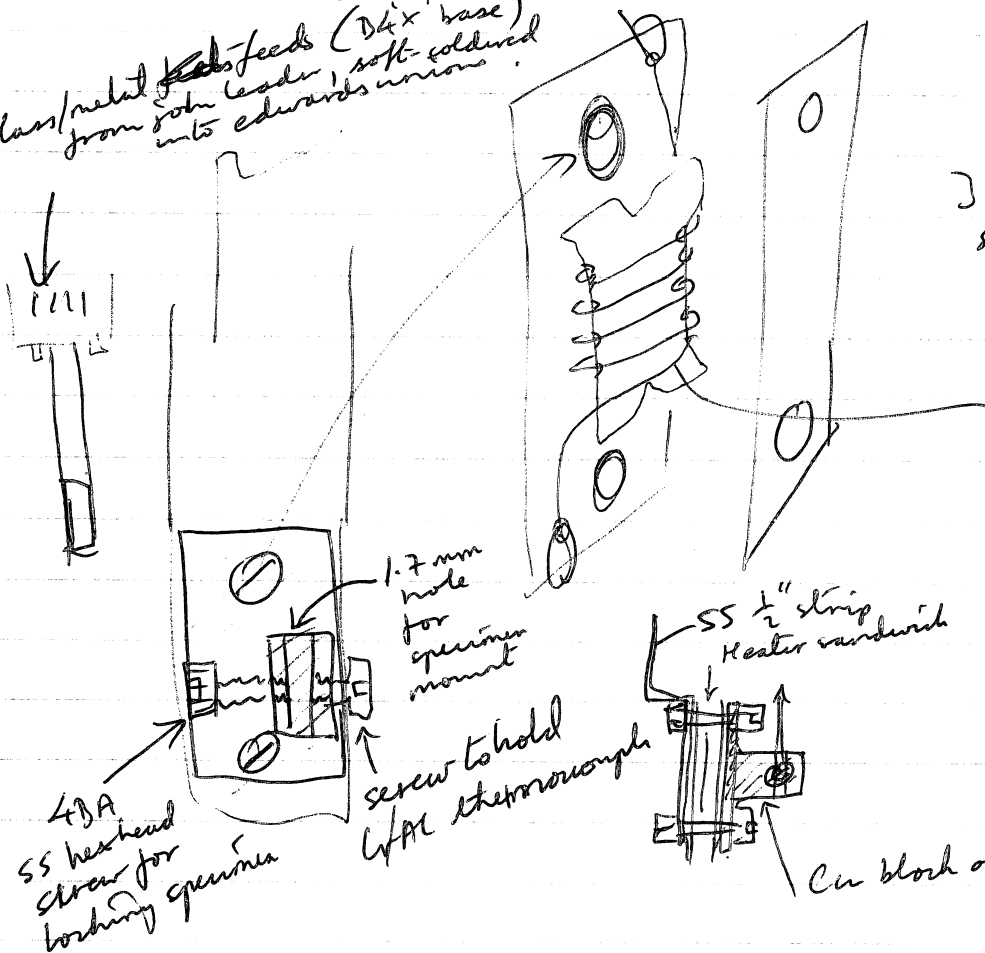
$3 \times 10^{-8}$  Ne / 60

45000s off grain boundary, moved 7h  
around & kept over today.  $\odot$

Refrubing Eds a/c - putting lines into sub-pump chimneys  
- new filaments  
? rad shield.

Hydrogen outgassing adj completed (fits onto oil diff pump on F-P autochanger)

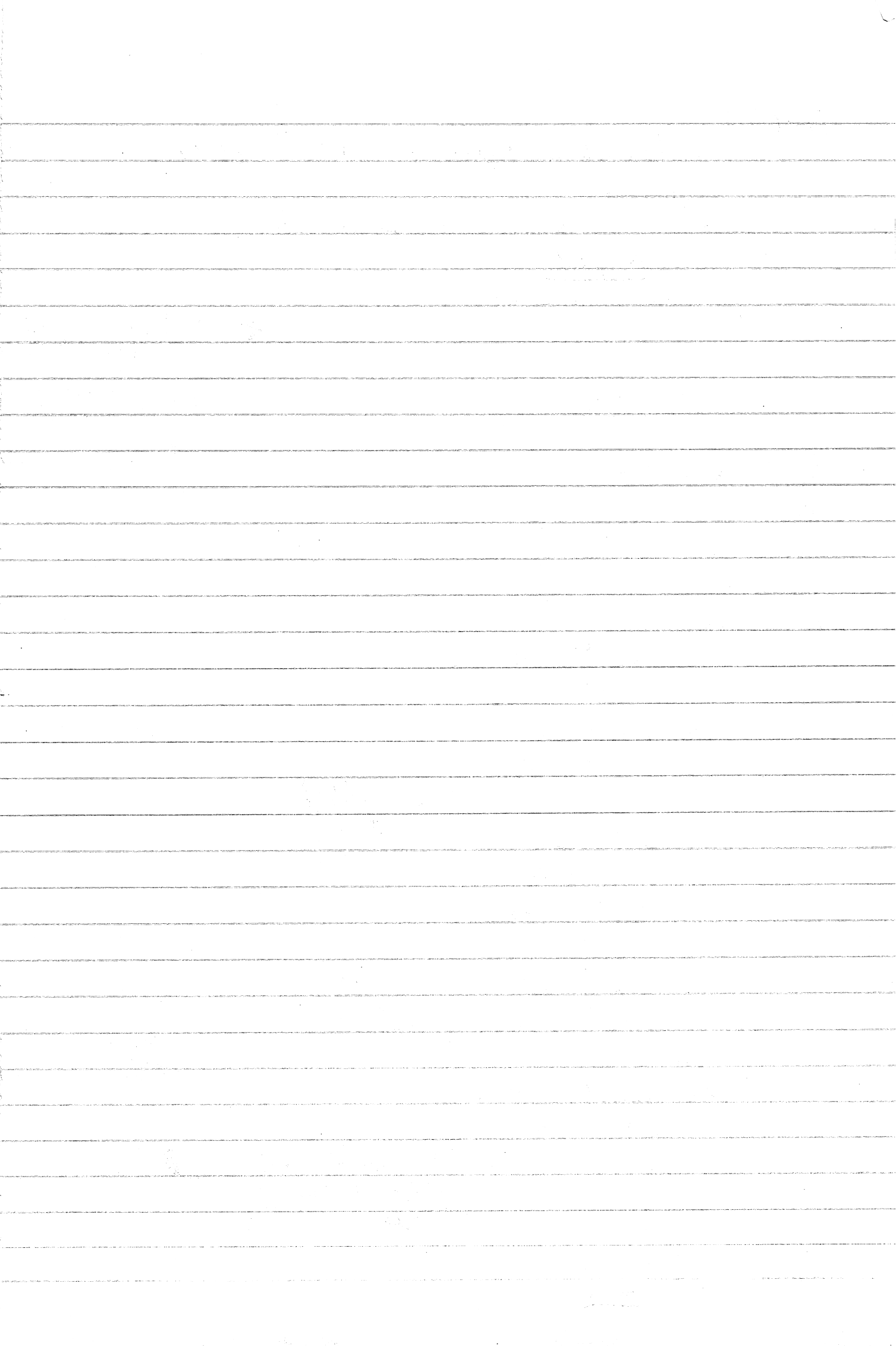
4 glass/metal feed (Dix' base)  
from soln leads, soft-soldered  
into Edwards union.



3 mica  
shims

heater ~ 6-8" of  
constantan wire  
8.5  $\Omega$ /yd.  
~ 5 volts needed  
for red heat.

Cu block on Cu plate



6/10/78

Fe/Sn gb as before.  $110^{-10}$  60/Ne

ph 3W } Blank  
15.06 kV  $1\frac{1}{2}$  phover gb

ph Mufik  
ph  $\frac{1}{2}$   $\frac{1}{4}$   $1\frac{1}{2}$   $\frac{1}{4}$  axial

$$\frac{1}{2}mv^2 = \frac{1}{2}m\frac{v^2}{c^2} = neE$$

$$t = \sqrt{\frac{1}{2} \frac{m c^2}{ne E}}$$

$$\propto \sqrt{\frac{h}{ne E}}$$

iAP Mufik

Fe<sup>2+</sup> 44 = 360

C<sub>6</sub> 27 166

Li 30

Su<sup>2+</sup> 60 65

Ne<sub>20</sub> 36

Fe<sup>2+</sup> 40 sec

C<sup>2+</sup> "

iAP 3W x 1su

Fe<sup>2+</sup> 20

C<sup>2+</sup> 60

C<sup>+</sup> 60

C<sup>2+</sup> ~ 50

Su<sup>2+</sup> 60

Su<sup>2+</sup> "

Su<sup>2+</sup> " 65

Fe<sup>2+</sup> 30 q rapid. 42

iAP x 3

More slightly iAP x 3

Fe<sup>2+</sup> 20

Su<sup>2+</sup>

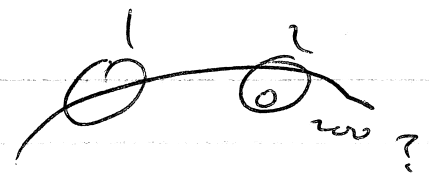
⋮

last one dud  
blunk

- ht? sparking over  
- stripe at side of  
picture



DIV x 3  
More DIV x 2  
WAPMph



IAP x 3  
Su 2+ x 2000 6000

blank  
C+ 2000 2 vhhly →

Fe 2+ 2000

Ne+

~~as~~ ? Su

IAP x 3

ph DW x 2 days or so 17-6KV, - pretty!  
extracted

2/10/78 sat Stearns PSW 3rd batch 300 mins @ 200  
110<sup>-10</sup>/60/No

T 240 200 ~~mins~~ mostly H ~ 5KV + 800-1000V 110/561

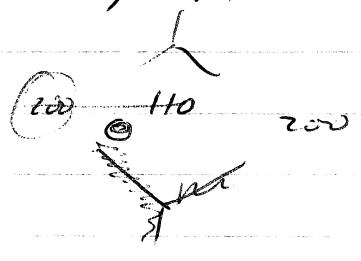
T 241 a 4.7 - 5.1 + 1KV 120/561 off? dark line  
± 500 + 500

b 5.1 - 5.35 120/561 New plane, dark

ph <sup>blank</sup> 31V x 3 where ph was

ph DIV x 3 axial

ph DIV x 3 ph aligned better with dark spot



T 242 5.35 120/561  
5.75 150/561 → (200V)  
6:00 1800 ~~mins~~ total  
ph DW x 3 6.15KV  
blank

9/10/78 Same spec 110°/60/No

Some dark hole 200

carefully aligned.



T343

150/561 a 5.8 + 9

6.16 + 1.18

8000 ions

Cloned off - ? carbide gone

b off matrix adjacent to previous specimen

160/561

6.2 + 1.2

6.34 + 1.35

5300 ions

Mostly Fe<sup>2+</sup>

ph DW x 3 at norm b

u ~ x 3 axial

u u x 3 over dark area top left.

move to line of original dark hole (2000) 110

T344

a 1100 of 'bdms'

160/561

b 600 off other dark hole on bottom 110

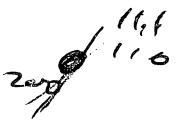
T345

a 6.76 + 1.3

1.6

170/561 off dash line

2000 ions



b 6.8 + 1.7

6.8 - 1.75

dash line, 1 ph diam. south.

3000 ions

ph Bin x 1

ph Mipha

ph DW x 3 7.60KV

ph axial ph x 3

ph dark spot on RHS 110 region x 3

T346

a 6.90 + 1.75 140/561

1.85

blank


ph x 3 us after 346a 7.49KV

190/561

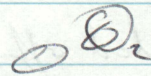
b axial 110 away from dark areas 6.90 + 1.9 10000 ions

ph BW ~ usual x)  
 back to original blank hole x)

T 247 ph ≈ ring of hole 7 + 1.9 190/581

at 2447 ins check -  - dark center  
 - realign ph over dark hole

4000 ins total

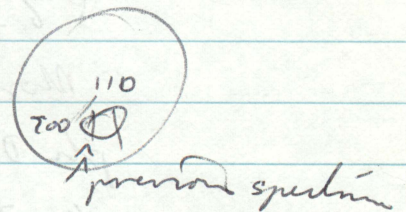


blank

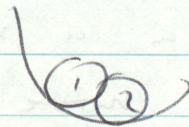
ph BW ??

IAP blank

IAP x) 200 bottom left.  
 shift with IAP x)



|                                           |         |        |
|-------------------------------------------|---------|--------|
| Fe <sup>2+</sup>                          | 62/64 = | 520 ns |
| C <sup>2+</sup> <sub>6</sub>              | 30      | 241    |
| C <sup>+</sup> <sub>12</sub>              | 42      | 340    |
| C <sub>3</sub> <sup>2+</sup> (18)         | 52      | 417    |
| C <sub>2</sub> <sup>+</sup> <sub>24</sub> | 60      | 481    |
| N <sup>+</sup>                            | 45      | 367    |
| N <sub>c</sub> <sup>+</sup>               | 54      | 440    |



Fe<sup>2+</sup> 50

C<sup>2+</sup> 50

C<sup>2+</sup> 50

Fe<sup>2+</sup> 40

C<sup>2+</sup> "

C<sup>2+</sup> "

C<sup>+</sup> "

C<sub>2</sub><sup>3+</sup> "

8.07 ± 1.8

IAP x)



Move site IAP x 3 8.62 KV DW

Fe<sup>2+</sup> 40 m  
C<sup>2+</sup> 40  
C<sup>2+</sup> 40  
C<sup>2+</sup> 120

IAP x 3

IAP Mph 2  
IAP x 3

move to usual 110 IAP x 3

Fe<sup>2+</sup> 40  
C<sup>2+</sup> -  
C<sup>2+</sup> -

IAP x 3

move right- IAP x 7

Fe<sup>2+</sup> 40  
C<sup>2+</sup> 40  
C<sup>2+</sup> 50

IAP x 2

Mh Div x 5, Iph blank 8.75 KV


IAP blank

cont'd

Tues 10/10/18 same spec 60/110<sup>-10</sup>/Ne.  
 IAP (blank)

|                  |    |                        |
|------------------|----|------------------------|
| Fe <sup>2+</sup> | 28 | 160 = 480              |
| C <sup>2+</sup>  | 6  | 25 = 220               |
|                  | 12 | <del>36</del> 72 = 214 |

IAP x 3  
 Fe<sup>2+</sup>  
 C<sup>2+</sup>  
 C<sup>2+</sup>

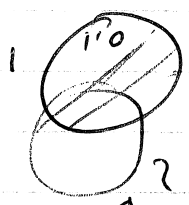
110 oval 

IAP M/L

IAP x 3

more IAP x 3

|                  |    |
|------------------|----|
| Fe <sup>2+</sup> | 30 |
| C <sup>2+</sup>  | "  |
| C <sup>2+</sup>  | "  |
| C <sup>2+</sup>  | "  |



IAP x 3

more down IAP x 3

|                  |    |
|------------------|----|
| Fe <sup>2+</sup> | 30 |
| C <sup>2+</sup>  | 30 |
| C <sup>2+</sup>  | 30 |
| C <sup>2+</sup>  | 60 |

IAP x 3

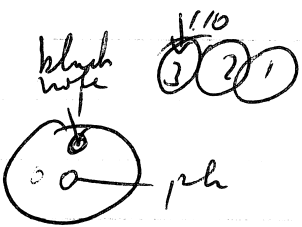
black hole @ t. of centre



IAP x 3  
 Fe<sup>2+</sup>  
 C<sup>2+</sup>  
 C<sup>2+</sup>

IAP x 3

sequence IAP  
 ph DIV x 5



↑  
 9 + 1.67

T 348 off dark hole (? exact or not point?)

a 220/561 8.48 +1.7-1.8...

No C after 500 wires - check

- dark hole gone - move to adjacent dark line

b 8.48 + 1.9

T 349 dark line near 110

10

a get to 2000 wires - ph blank

ph DW x 2 8.74 kV

more Napht

ph DW x 3

move to bigger dark line

ph DW x 3

b 8.3-8.6 + 1.96

220/561

ph DW 1 ± 1/4

9.53 kV

→ axial

ph DW 1/2 ± 1

T 350 8.5 + 1.95 220/561

off small dark hole, bottom left

1000 wires

ph blank

IAP x 3

Fe<sup>2+</sup> 20

C<sup>2+</sup> "

IAP Napht

Fe<sup>2+</sup> 30

C<sup>2+</sup> "

C<sup>2+</sup> "

IAP x 3

More slightly IAP x 3

Fe<sup>2+</sup> 30 s

C<sup>2+</sup> "

C<sup>2+</sup> "

90110



11/10/78

same top blank <sup>line</sup> ~~hole~~ RVS

115° / 60 / Ne

T 352

9.80 + 1.5

240/561

-1000  $\omega$

60K

leave to pump out over lunch  
except 250  $\omega$

T 353 a same place 9.90 + 1.8

240/561

60K

P 710" acc. to t-gauge.

1000  $\omega$

2

b same again

1000  $\omega$

-

ph blank

M DIV x 3 10.22 VU

T 354

dark line LHS . ~~9.8~~ 8.8 - 9.5 / 240

- 400  $\omega$

b - rapid 9.6 + 2

- type run out - region at 1800 on counter

- 6000  $\omega$  - 9.65 + 2

240/561

a cut off -> T 3546 only.

12/10

Ti  $10^{-10}$  / 60 / Ne

|       |           |                |
|-------|-----------|----------------|
| T 355 | 130 / 561 | 5.4 to 6 → 1KV |
| a     | 140 / 561 | 5.6 - 5.85 + 1 |
|       | 150       | - - ↓ + 1      |
|       | 160       | 6.3 + 1        |

§

New spectrum @ 600 ions ↑

|   |           |           |
|---|-----------|-----------|
| b | 6.45 + 1  | 160 / 561 |
|   | 7.0 ↓ + 1 | 170 / 561 |
|   |           | 180 / 561 |

Step @ 1300

|       |          |           |
|-------|----------|-----------|
| T 356 | 7.0 + 1  | 180 / 561 |
| a     | 8 + 1.23 | 200 / 561 |

2000 ions ↑

|   |                 |           |
|---|-----------------|-----------|
| b | 8 + 1.23 - 1.25 | 200 / 561 |
|---|-----------------|-----------|

resolv check .

↳ 50 volt change only  
1700 ions .

T 257      ① painted with Wood No, No 70  
on it.

18/10

T 758

Ir painted Mond 1 (no  $\bar{e}$ )

7359

Ir substrate

7360

378/600

2200 ions from III He(+Ne)

2.2 + 46(?) all at 1 voltage to see how resolu  
depends on voltage ratio - set to give asymmetrical  
spot on detector as nearly focussed as poss.



18/10

T261

8.51 + 1      200 / 561      ~ 30200  
off/1st layer of a Fe/C PSW 20/200° (SP) wire  
- flushed

T262

More PSW, same 20/200° orientation.

Spectrum off black region at side of bright ferrite —  
? Carbide or ? oxide

5.9 + 600 } 140 / 561       $210^{-7} \text{Ne}$   
6.0 + 1.00 }      78 K



↓  
6.30 +      150 / 561      c

~ 800 eV

going home time

h

19/10/78 Subpump filament gone (TSP subed off overnight to keep it clean)

T363 Same oxidized PSLW,  
6.5 + 1 160/561

a ~ same place

b a bit further away from metal.

T364 @ the metal oxide interface  
- move back to ~ in after ~ 600 ions

T365 8.4 + 1.5 200/561 oxide

a bit further out than 364

ph <sup>region</sup> DVV off axes x)  
on axes x)

366 Black line in matrix

2000 ions after fixed amp calk - long  
ions + lots of byproducts

ph DV x)

~~367~~ a 2000 move off black line

ph x)

220/561

Move to black hole @ bottom

ph x)

b ~ 9.3 + 1.6?

230/561

ph x)

~~368~~

ph x) center

ph x) off black hole

@ bottom left

368

~ 9.8 1.8

240/561

no C in last 1000 years

- realign @ 650 years  $\rightarrow$  increased carbon captures  
onto black hole — 1000

ph  $\times$  3

actual ph  $\times$  3

going home time

T 3 69

off oxide @ bottom of tip  
~ 4k  $\Delta$

260/561

270/561

ph blank  
ph axial x3

ph on dark line x3

T 3 70

4200 end off dark line 270/561

~ 11 + 2

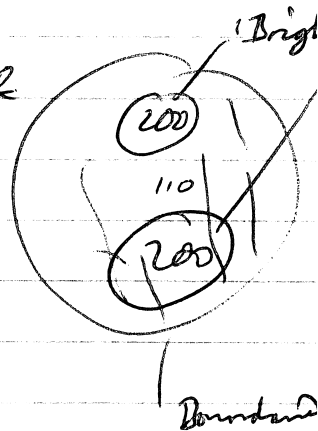
280/561

Series of pics @ various orientations

Notes

More pics, excepting up to ~14.5 kV @ end.

Some below 3'v showing orientation & low-angle nature of boundaries



Attempted to extract tip for em pics, manipulator broke - rats.

to top, much painted, looked @ in stereoscan - no  $\frac{1}{2}$  day prob  
- few bits of paint, but no signs of a coherent layer.

$\sim 115^9$  after kube - ??

31/10/78

T371

Mo /  $110^6$  He  $\sim 6.2 \pm 0.8$  RU

150/561

H $\gamma$  set dodgy - quiet

$\sim 500$  b  $\sim 50$

Chinese visitors

Neil Pashley says vac system for Culham in 1-2 weeks.

1/Nov 78

Order for repair/calibration of Marconi scope #165  $\approx$  3 wks. OK.

7372 160/581 Mo 6.5KV+1 /  $5 \times 10^{-7}$  He

same spec  $6 \times 10^{-10}$  pressure  $\hat{c}$ g

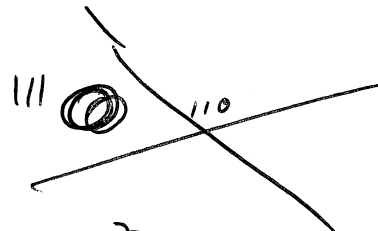
MoO, last 200 @ 1.05  $\mu$ bar

[ ion gauge (off eds 7-E system) now replaces trigger gauge, which shorted out internal (metallic gauge collected by field inside) ]

2 Nov 78

T 273 Mo var 170/561 same region  
 as yesterday for comparison, to see if tail on Mo<sup>3+</sup>  
 @ Mo<sub>c</sub><sup>3+</sup> b-8 + 1.1-1.2 a 1000  
 ← excellent resolu 6.8 + 1.3 b

T 274 a

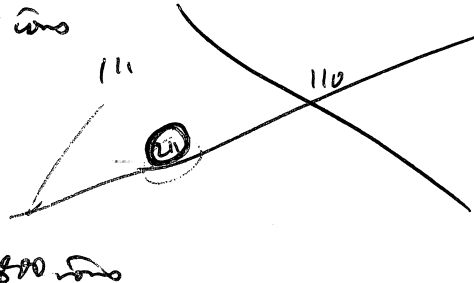


7.4 + 1.1

in He 5 10<sup>-7</sup>  
500 cm

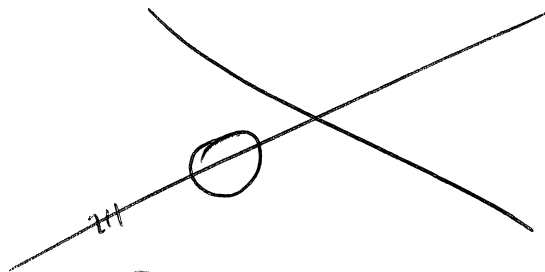
180/561

b



7.4 + 1.1

T 275

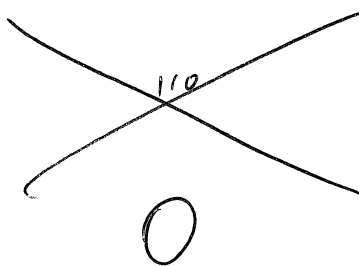


7.4 + 1.3

180/561

a

b



7.4 1.4

wo



10/11/78

Same Mo

T 376 Var, 60 (210<sup>-4</sup>!) 205/561 a 7.83 + 1.37 - 7.85 1200 wds

205/561 b 8.00 + 1.37

T 377 4 4 8.15 -> dropped below 8 during run  
w/ hit set unstable 2000 wds

H7 down, then up again

T 378 205/561 8.15 + 1.37 - 8.19

Stop @ 500 wds to change H7 set - still drifting  
H7 ↓ ↑ - pulse clean.

T 379 a 8.30 + 1.37 2200 *reps!*  
b 8.45 + 1.37 2400

T 380 8.60 + 1.37 1780

(New tape)

Inspect range, except some

T 381 tape labelled 381 var 8.80 + 1.37 1100

except some

T 382 9.15 + 1.37 1500 *reps!*  
except -

T 383 9.15 + 1.57 1300

except

T 384 9.6 + 1.57 500

Stop.

U

8.8 - 11.2 = 2.4  
9.3 - 9.82 = 0.52

14/11/78

T 385

$M_2/60$        $110^7$  var.  
 $600/240$        $10.3 + 1.6$  (~ best form)       $1000$   
 $600/255$       " +  $1.63$        $1000$

T 386

$220/800$        $10.3 + 1.65$        $800$

11.77

690      230

11 KV

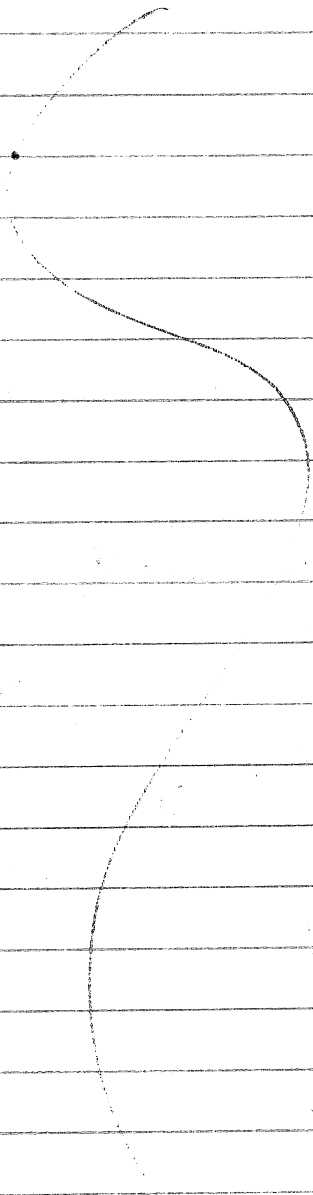
|     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|
| 690 | 197 | 222 | 255 | 610 | 200 | 219 | 255 |
| 590 | 146 | 223 | 254 | 620 |     | 214 |     |
| 580 | 194 | 224 | 254 | 630 | 202 | 218 | 256 |
| 570 |     | 226 |     | 640 |     | 217 |     |
| 560 | 192 | 228 | 252 | 650 |     | 217 |     |
| 550 |     | 231 |     | 660 | 205 | 216 | 257 |
| 540 | 192 | 236 | 252 |     |     |     |     |
| 530 |     | 247 |     |     |     |     |     |

T 387

a  $580/245$        $10.5 + 1.6$        $1000$   
 $580/264$       "      "

T 388

a  $630/237$        $10.5 + 1.7$   
b  $540/262$

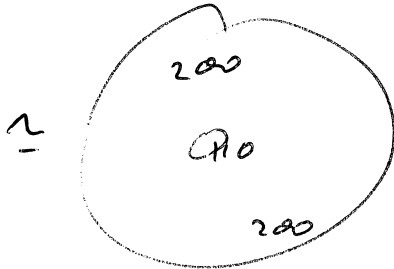


31/1/79

Davyguths Fe/Si specimen (polished August last year!)

Ne/60/50<sup>-10</sup>

(IAT) ph op 7.5KV 1/4 1/2 | 2 1/2 | 3w as usual



Spectrum 110 using store. 703 + 1075 ~ 1/sec.  
190/561

-1900 ions spectrum - gas 210<sup>-9</sup> Ne dunn, mm

| Time | No  |        | T   | N   |       | T   | N        |
|------|-----|--------|-----|-----|-------|-----|----------|
| 0    | 1   | ①      | 258 | 1   |       | 311 | 1        |
| 61   | 2   |        | 259 | 4   |       | 2   | 1        |
| 62   | 49  | [1-25] | 260 | 5   | [-20] |     |          |
| 63   | 101 |        | 261 | 1   |       | 429 | 1 [55-2] |
| 64   | 10  |        | 272 | 1   |       |     |          |
|      |     |        | 273 | 1   |       |     |          |
| 96   | 1   |        | 298 | 2   |       |     |          |
| 112  | 1   |        | 299 | 10  |       |     |          |
| 215  | 2   |        | 300 | 27  |       |     |          |
| 216  | 2   |        | 301 | 5   |       |     |          |
| 217  | 30  |        | 302 | 1   |       |     |          |
| 218  | 45  | [14-3] | 304 | 41  |       |     |          |
| 219  | 2   |        | 305 | 327 |       |     |          |
| 221  | 2   |        | 306 | 296 |       |     |          |
| 224  | 1   |        | 307 | 16  |       |     |          |
| 225  | 2   |        | 308 | 11  |       |     |          |
| 232  | 1   |        | 309 | 3   |       |     |          |
| 233  | 1   |        | 310 | 4   |       |     |          |

↑ 88

745

Blank

pl DIV x 4 7.9KV

more off 110 towards 200, realign

DIV x 3 ± 12

(2) [ 7.7 + 1.4 190/561 710<sup>-7</sup> Ne  
7.7 - 1.5 -1200 ~~cm~~

|    |     |     |    |
|----|-----|-----|----|
| T  | N   | 307 | 11 |
| 0  | 1   | 308 | 5  |
| 61 | 3   |     |    |
| 62 | 67  | 311 | 1  |
| 63 | 178 | 669 | 1  |
| 64 | 4   |     |    |
| 65 | 2   |     |    |
| 87 | 1   |     |    |

|     |    |
|-----|----|
| 216 | 4  |
| 217 | 45 |
| 218 | 11 |
| 219 | 1  |
| 221 | 1  |
| 224 | 1  |

6.33 <sup>4</sup>/<sub>6</sub> ± .80

|     |     |
|-----|-----|
| 298 | 3   |
| 299 | 41  |
| 300 | 17  |
| 302 | 1   |
| 303 | 16  |
| 304 | 42  |
| 305 | 542 |
| 06  | 83  |

932

More to 200 <sup>blank</sup> DW x 4

7.8 + 1.65      Spectrum 190/361  
 - 1.85

②

|    |     |     |    |
|----|-----|-----|----|
| 10 | 1   | 207 | 11 |
| 11 | 2   | 208 | 7  |
|    |     | 209 | 1  |
| 61 | 9   | 210 | 1  |
| 62 | 75  | 212 | 1  |
| 63 | 120 |     |    |
| 64 | 3   |     |    |

86 2

|     |    |
|-----|----|
| 121 | 1  |
| 141 | 1  |
| 215 | 1  |
| 216 | 9  |
| 217 | 29 |
| 218 | 8  |
| 221 | 3  |
| 225 | 2  |

52 5.28% ± .73

|     |     |
|-----|-----|
| 298 | 10  |
| 299 | 44  |
| 300 | 10  |
| 301 | 3   |
| 303 | 61  |
| 304 | 424 |
| 305 | 332 |
| 306 | 27  |

932

Dark to 110 - ph x 4 8.1 KV

8.2 + 1.7 200/61 5157W. 60

→ 200 KV - 300  $\Omega$  only, so  
realize & continue @ 8.2 + 2 - 8.2 + 2

|     |     |    |                             |
|-----|-----|----|-----------------------------|
| 0   | 0   |    | $\sim 1000 \text{ } \Omega$ |
| 10  | 1   |    | 299 8                       |
| 11  | 0   |    | 300 0                       |
| 60  | 27  |    | 303 1                       |
| 61  | 142 |    | 304 1                       |
| 62  | 29  |    |                             |
| 63  | 2   |    | 307 1                       |
|     |     |    | 311 1                       |
| 210 | 1   |    | 312 1                       |
| 211 | 19  |    | 317 1                       |
| 212 | 5   | 26 |                             |
| 215 | 1   |    | 328 1                       |
|     |     |    | 386 1                       |
|     |     |    | 417 1                       |
| 256 | 1   |    |                             |

|     |     |
|-----|-----|
| 289 | 1   |
| 290 | 12  |
| 291 | 23  |
| 292 | 6   |
| 293 | 1   |
| 294 | 2   |
| 295 | 87  |
| 296 | 429 |
| 297 | 202 |
| 298 | 21  |

748

Blank

ph  $\frac{1}{2}$   $\frac{1}{2}$  1 2 9.2 KV  
going home later

3.18  $\pm .62$   
~~3.266~~  $\pm$

1/2/79

Some Fe/Si

VAD Blank

IAP Div x 4 or 5      ~ 9KV  
pulse 8.85 + 2.0 (delay cable)  
DW x 3 or so

1 ans @ 67, 105 <sup>total</sup>  
550ns      690ns

No start pulse direct from  
pulsar, so have to subtract  $\tau_d$   
from these time to get title line

Require  $\frac{690 - \Delta}{\sqrt{28}} = \frac{550 - \Delta}{\sqrt{14}}$

$690 - \Delta = 778 - 1.4\Delta$

$141\Delta = 88$

$\Delta = 212.5 \text{ ns}$

$\therefore T_{Fe} = 480$

$T_{Si} = 340$

$\therefore T_{H_2} = 90 \Rightarrow 300 \Rightarrow 36$

$T_{D_{11}} = 300 \Rightarrow 510 \Rightarrow 60$

$T_{C_{12}} = 214 \Rightarrow 525 \Rightarrow 65$

$C_6 = 222 \Rightarrow 435 \Rightarrow 54$

$D_{10} = 287 \Rightarrow 500 \Rightarrow 62$

Fe<sup>2+</sup> 60

Si<sup>2+</sup> a

Fe<sup>2+</sup> 20 quader ~ 1 plane / 10 users

100 Hz

Si<sup>2+</sup> 30

C<sup>2+</sup> (54) 20

noise (57) 30

((? DIV))



Spec 04017-19-6 1thick

|                  |    |       |                      |
|------------------|----|-------|----------------------|
| Fe <sup>2+</sup> | 60 | rapid | } ~ (plane / 10 sec) |
| Si <sup>2+</sup> | 1  |       |                      |
| Sc <sup>2+</sup> | 1  |       |                      |

IAP Div X 4 or 5  
IAP Blank.

Move to LH 200 IAP x 3

IAP N film 2

200 x 3

pulse - popped  
- corrupt

IAP x 2 or 4

- ?slightly

(6)

IAP x 3

ph x 4

up volts ph x 4

shift slightly ph x 1 or 2

(110  
200)

ph x 4  
ph Nuph

evapst ~ x 10 ph x 4

~~IAP x 4~~ IAP blank

IAP x 4

lunch, HT down (unstable, cool off)

ph blank

ph x 4 ~ 12-2 kV

ph x 2 with steady pulsing.

- Flushed

ph blank IAP blank

New Fe/Si tip ex Dargunguh

FS14-5 [1 think]

Spectrum, usual,  $610^{-7}$  Ne 6.80 + 1 — 1.25 keV 160/561

| T              | No. |       |
|----------------|-----|-------|
| 0              | 1   | 225 1 |
| 2              | 1   | 226 2 |
| 66             | 3   | 227 1 |
| 67             | 28  | 228 1 |
| 68             | 40  |       |
| 69             | 4   |       |
| 71             | 1   | 253 1 |
|                |     | 465 1 |
| 225            | 27  | 466 1 |
| 226            | 22  |       |
| 227            | 4   |       |
| 240            | 4   |       |
| 243            | 1   |       |
| 244            | 1   |       |
| 281            | 1   |       |
| 284            | 1   |       |
| 324            | 9   |       |
| 325            | 25  |       |
| 326            | 10  |       |
| <del>327</del> | 1   |       |
| 329            | 3   |       |
| 220            | 209 |       |
| 221            | 458 |       |
| 222            | 105 |       |
| 223            | 6   |       |
| 224            | 6   |       |

5

(1)

70

$$7.63 \pm .91\%$$

847

$$6.8 + 1.25 - 1.55$$

1575/561

| T  | N   |
|----|-----|
| 63 | 1   |
| 64 | 21  |
| 65 | 111 |
| 66 | 76  |
| 67 | 1   |

1140 ions

(2)

|    |   |
|----|---|
| 89 | 2 |
| 90 | 4 |

|     |    |
|-----|----|
| 225 | 4  |
| 226 | 22 |
| 227 | 21 |
| 229 | 1  |
| 230 | 6  |
| 231 | 2  |
| 234 | 1  |

57

$$6.20 \pm .826$$

|     |    |
|-----|----|
| 310 | 1  |
| 311 | 13 |
| 312 | 24 |
| 313 | 8  |

316 50

|     |     |
|-----|-----|
| 317 | 209 |
| 318 | 405 |
| 319 | 33  |
| 320 | 8   |
| 321 | 10  |
| 322 | 1   |

862

446 1

ph blank

ph 5 4 7.62 mV

good home time

2/2/79

Same Exp IAP BW x 2 or 4

0.3/10

$Fe^{2+} 60$   
 $Si^{2+} 60$

?  $\left\{ \begin{array}{l} Fe^{2+} \\ Si^{2+} \end{array} \right.$

$Fe^{2+} 45$  pop

These @ 200 Hz - joint

reduce to 100 Hz  $\rightarrow$  brighter spots @ low cp input - v

$Si^{2+} 45$  71-72

$Fe^{2+} 40$

$Si^{2+}$  pop

$Si^{2+} 40$

$\sim 10$  sec / plane

IAP x 3

pk x 3

more to 200 IAP x 3

$Fe - ?$  pop )

(  $Fe$

$Si^{2+} ?$  pop

$Si^{2+}$

$Si^{2+} 20$  sec

IAP blank

$Fe^{2+} \frac{1}{8}$

IAP pop

$\frac{1}{8}$  sec  $Fe^{2+}$

$\frac{1}{8}$   $Fe^{2+}$

10 sec "

3 " "

10 sec  $Si^{2+}$

10 sec  $Si^{2+}$

? varying length exposure to relate concentrations of different species

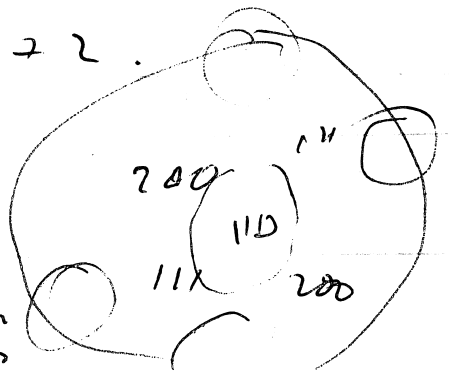
7 8 7 2 .

IAP | Blank  
DIV x 3

$\sim 7.8$  KV

pk x 4 1 2  $\frac{1}{2}$   $\frac{1}{4}$

pk x  $\frac{1}{2}$  after pop  
flashed when turned up ch monitors



6/2/78

| Mo/He $10^{-5}$ |    | 60  |    | 4.9 + 0.8 - 1.0 keV |    | 136/561 |
|-----------------|----|-----|----|---------------------|----|---------|
| 0               | 1  | 400 | 12 | 488                 | 7  |         |
| 142             | 6  | 1   | 11 | 9                   | 0  |         |
| 143             | 12 | 2   | 26 | 40                  | 2  |         |
| 144             | 16 | 3   | 17 | 1                   | 11 |         |
|                 |    | 4   | 12 | 2                   | 7  |         |
|                 |    | 5   | 4  | 0                   | 4  |         |
| 312             | 1  | 6   | 9  |                     |    |         |
|                 |    | 7   | 7  |                     |    |         |
| 335             | 2  | 8   | 1  | 546                 | 1  |         |
|                 |    | 9   | 1  |                     |    |         |
| 342             | 2  | 10  | 0  |                     |    |         |
| 343             | 4  |     |    |                     |    |         |
| 346             | 4  | 470 | 4  |                     |    |         |
|                 |    | 1   | 8  |                     |    |         |
| 384             | 1  | 2   | 14 |                     |    |         |
| 385             | 13 | 0   | 6  |                     |    |         |
| 386             | 45 | 4   | 2  |                     |    |         |
| 387             | 27 | 5   | 1  |                     |    |         |
| 388             | 0  | 6   | 5  |                     |    |         |
| 389             | 1  | 7   | 10 |                     |    |         |
| 390             | 23 | 8   | 9  |                     |    |         |
| 391             | 32 | 9   | 20 |                     |    |         |
| 2               | 49 | 80  | 18 |                     |    |         |
| 3               | 57 | 1   | 15 |                     |    |         |
| 4               | 61 | 2   | 20 |                     |    |         |
| 5               | 46 | 3   | 12 |                     |    |         |
| 6               | 49 | 4   | 12 |                     |    |         |
| 7               | 51 | 5   | 11 |                     |    |         |
| 8               | 68 | 6   | 16 |                     |    |         |
| 9               | 74 | 7   | 21 |                     |    |         |

| a      | b     |
|--------|-------|
| 511+   |       |
| 1Kvmbc | +15   |
| 75 1   |       |
| 142 1  | 2     |
| 147 2  | 12    |
| 144 11 | 4     |
|        | 145 1 |
| 229 1  | 224 1 |
| 42 1   | 5 1   |
| 2 1    | 7 2   |
| 4 1    | 9 3   |
|        | 40 3  |
|        | 1 1   |
|        | 2 2   |
|        | 346 1 |
|        | 4 2   |
|        | 5 2   |
|        | 55 1  |
|        | 55 1  |
| 286 10 | 284 2 |
| 7 21   | 5 26  |
| 8 2    | 6 74  |
| 90 6   | 7 25  |
| 91 15  | 8 1   |
| 2 12   | 9 15  |
| 2 12   | 90 24 |
| 2 12   | 1 22  |
| 4 22   | 2 53  |
| 5 18   | 3 41  |
| 6 10   | 4 57  |
| 7 10   | 5 21  |
| 8 17   | 6 26  |
| 9 22   | 7 41  |
| 400 3  | 72 72 |
| 1 9    | 20 20 |
| 2 6    | 4 4   |
| 2 11   | 10 10 |
| 4 2    | 24 24 |
| 6 5    | 22 22 |
| 7 6    | 6 6   |
| 8 2    | 5 4   |
| 10 1   | 8 5   |
|        | 9 1   |
|        | 10 4  |
|        | 11 2  |

| a    | b      |
|------|--------|
| 11 2 |        |
| 21   |        |
| 71 2 | 468 11 |
| 2 2  | 70 2   |
|      | 71 22  |
|      | 72 11  |
| 7 2  | 75 1   |
|      | 77 6   |
| 9 2  | 78 18  |
| 80 6 | 9 9    |
| 1 2  | 80 22  |
| 2 6  | 81 8   |
| 2 4  | 2 15   |
| 4 2  | 2 12   |
| 5 1  | 4 8    |
| 6 2  | 5 12   |
| 7 4  | 6 5    |
| 8 6  | 7 24   |
|      | 8 30   |
| 91 1 | 489 1  |
| 2 4  | 90 2   |
| 2 1  | 1 1    |
| 4 1  | 11 11  |
|      | 490 6  |

Gas pressure down 1000 pulse

74 ~~254~~ 2  
5 6

142 1  
2 2

396 88  
7 18

490 5  
1 1

222 1  
4 1  
7 1  
8 1  
9 1  
40 2

99 9  
490 22  
1 8  
2 1

898 1  
902 1

1 2  
2 1  
2 1  
4 2  
7 1

468 2  
7 12  
470 2  
1 2

282 2  
2 25  
4 52  
5 22  
6 1  
7 16  
8 25  
9 25  
90 56  
1 42  
2 75  
3 24  
4 48  
5 26

772 5  
474 12  
5 2  
6 7  
7 14  
8 9  
9 18  
80 5  
1 6  
2 5  
3 15  
4 24  
5 7  
488 4  
9 5



Wed 7/2/79 ph blank

Diggs and Fe/Si c/s spec DW

ph Mph

4-5 ph DW 11.5KV Ne 60

New HT set - old, unstable

ph DW x 4 14KV

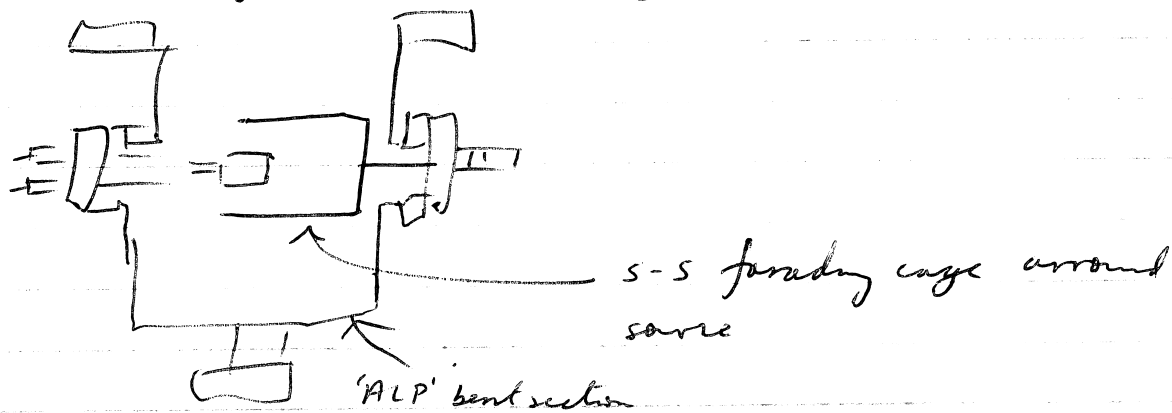
Flushed @ ~ 16KV

← qb ? just starting to be seen,

ph blank

The Gallium ion source arrived from Culham yesterday (brought by Phil Perrett).

Put into primary sb system today: -



500

Reposited Keithley 602 electrometer from D. Ashlund (has had it since 1973!) Serial No 20395 (Bought by Ed Diggs 1972 or 73)

Stepons pro ↓

Stefans PSU 300 mins / 200C

Ne/60 7.9 KV

①  
ph 4 x BIV

1000in Spectrum off black hole

185/561

7.56 + 1 - 1.15

1020

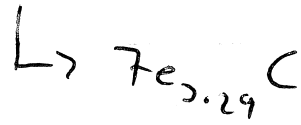
ph BIV x 4 7.56 KV  
ph DIV x 4 8.2

|                              |     |     |                              |     |     |                        |
|------------------------------|-----|-----|------------------------------|-----|-----|------------------------|
|                              | 62  | 18  |                              | 254 | 1   |                        |
|                              | 63  | 101 |                              |     |     | C <sup>+</sup> { 250 1 |
| H <sup>+</sup>               | 64  | 103 |                              |     |     | 251 1                  |
|                              | 65  | 8   | Ne                           | 263 | 1   | 255 1                  |
|                              | 69  | 1   |                              | 264 | 1   |                        |
|                              |     |     |                              | 265 | 1   |                        |
|                              |     |     |                              |     |     | Fe <sup>+</sup> 407 1  |
|                              | 145 | 2   |                              | 286 | 10  |                        |
| C <sup>++</sup>              | 146 | 32  | C <sub>2</sub> <sup>24</sup> | 287 | 6   | M <sub>130</sub> 678 1 |
|                              | 147 | 37  |                              | 288 | 5   |                        |
|                              | 148 | 2   |                              |     |     |                        |
|                              | 150 | 1   |                              |     |     |                        |
|                              |     |     |                              | 302 | 1   |                        |
|                              |     |     |                              | 303 | 5   |                        |
|                              | 204 | 9   |                              | 304 | 12  |                        |
| C <sup>+</sup>               | 205 | 8   |                              | 305 | 8   |                        |
|                              | 206 | 3   |                              | 306 | 1   |                        |
|                              |     |     |                              | 307 | 4   |                        |
| M <sub>13</sub> <sup>2</sup> | 214 | 1   | Fe <sup>2+</sup>             | 308 | 58  |                        |
|                              |     |     |                              | 309 | 237 |                        |
|                              | 220 | 2   |                              | 310 | 279 |                        |
|                              |     |     |                              | 311 | 28  |                        |
|                              | 248 | 2   |                              | 312 | 7   |                        |
|                              | 249 | 4   |                              | 313 | 7   |                        |
|                              | 250 | 7   |                              |     |     |                        |
|                              | 251 | 2   |                              | 315 | 2   |                        |
|                              | 252 | 1   |                              |     |     |                        |

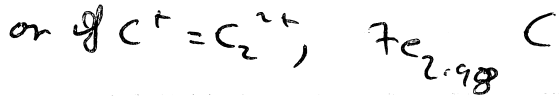
$$C^{2+} = 74$$

$$C = 74 + 21 + 51 + 42 + 9 = 197$$

$$C^+ = 21$$



$$C_2^{2+} = 17$$



$$C_2 = 21$$

$$C_2^+ = 3$$

$$Fe^{2+} = 649 \quad \therefore 216$$

Axial ph DIV  $\times 4$

Move to edge of carbide

lower gas pressure ( $3 \times 10^{-5}$   $\uparrow$  Ne last spectrum)

207 + 1 - 1.22 185/561

Spectrum

ph DIV  $\times 4$  8.68 keV

axial ph DIV  $\times 3$

M Ni fit

axial ph  $\times 4$

back to carbide  $\times 3$  cos not sure if camera focused

ph blank

spectrum overlap 1020  $\text{\AA}$



2

|    |    |
|----|----|
| 62 | 7  |
| 63 | 63 |
| 64 | 74 |
| 65 | 3  |

|     |     |
|-----|-----|
| 203 | 15  |
| 204 | 27  |
| 205 | 9   |
| 206 | 3   |
| 207 | 4   |
| 205 | 51  |
| 209 | 325 |
| 210 | 263 |
| 211 | 21  |
| 212 | 19  |
| 213 | 4   |
| 214 | 2   |
| 215 | 1   |
| 217 | 1   |

|     |   |
|-----|---|
| 126 | 1 |
|-----|---|

|                 |     |   |
|-----------------|-----|---|
| C <sup>++</sup> | 146 | 4 |
|                 | 147 | 3 |
|                 | 152 | 1 |

|     |   |
|-----|---|
| 189 | 1 |
|-----|---|

40<sup>2</sup> 2 70 1

|                |     |   |
|----------------|-----|---|
| C <sup>+</sup> | 204 | 1 |
|                | 205 | 2 |
|                | 206 | 1 |
|                | 213 | 1 |

Going home time

|                           |     |   |
|---------------------------|-----|---|
| <u>165</u> <sup>2+?</sup> | 223 | 2 |
|---------------------------|-----|---|

|                 |     |   |
|-----------------|-----|---|
| C <sup>++</sup> | 250 | 3 |
|                 | 251 | 1 |

|    |     |   |
|----|-----|---|
| Ne | 264 | 1 |
|    | 265 | 1 |

|                |     |   |
|----------------|-----|---|
| C <sup>+</sup> | 287 | 1 |
|----------------|-----|---|

|     |   |
|-----|---|
| 299 | 1 |
|-----|---|

|     |   |
|-----|---|
| 302 | 1 |
|-----|---|

8/2/79 Same Fe/C PSC 200/200  
min

IAP 6 x DIV  
+ 1

8.20  
8.6 KV



gestrodinge  
carbide

$$Fe^{2+} = 110 = 720ms$$

$$\delta = 210$$

$$\therefore Fe^1 = 510ms$$

$$\therefore C_6 = 236 = 450 = 55 + 1 = 960$$

$$C_{12} = 374 = 544 = 66$$

$$C_{18} = 409 = 620 = 76$$

$$S_6, N_{14} = 261 = 570 = 71$$

$$C_{24} = 472 = 680 = 104$$

$$C_{36} = 578 = 790 = 117$$

$$S_{16}^2 = 285 = 600 = 74$$

Fe<sup>2+</sup>

E<sup>2+</sup>

Fe<sup>2+</sup>

C<sup>2+</sup>



nk DIV x 3

more DIV x 4



Fe 40 sens q. varied

C<sup>1</sup> "

C<sup>1</sup> "

? S<sup>2</sup> "

? N<sup>+</sup>, S<sup>1</sup> "

~~IAP~~ IAP x 3

LHS



IAP x 3 9KV

v little c - edged top, so  
 move to n centre



IAP x 1  
 IAP N up to  
 IAP x 2

Fe<sup>2+</sup> 40,

C<sup>2+</sup> - abandoned

C<sup>2+</sup> 4

C<sup>2+</sup> 4

IAP x 2



More

IAP x 2

Fe<sup>2+</sup> 40

C<sup>2+</sup> 4

C<sup>2+</sup> 1

Fe<sup>2+</sup> 20

C<sup>2+</sup> 20

IAP x 2

ph x 4

ph x 4

ph x 2, over black hole yes before - spectrum



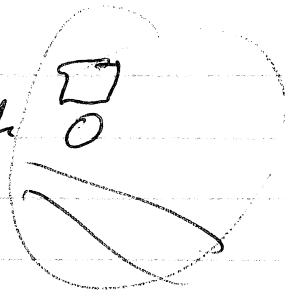
# Spectrum of carbide

|     |    |    |     |     |    |            |          |
|-----|----|----|-----|-----|----|------------|----------|
| 57  | 7  |    | 265 | 2   |    | 8.69 + 1.8 | 180/561  |
| 58  | 45 |    |     |     |    |            |          |
| 59  | 62 |    | 267 | 1   |    |            |          |
| 60  | 4  |    |     |     |    |            |          |
|     |    |    | 269 | 3   | 25 |            |          |
| 133 | 12 | 6  |     |     |    |            |          |
| 134 | 48 |    | 277 | 5   |    |            |          |
| 135 | 38 |    | 278 | 24  |    |            |          |
| 136 | 5  |    | 279 | 32  |    |            |          |
|     |    |    | 280 | 8   |    |            |          |
| 187 | 13 | 12 | 281 | 17  |    |            |          |
| 188 | 21 |    | 282 | 69  |    |            |          |
| 189 | 8  |    | 283 | 292 |    |            |          |
|     |    |    | 284 | 500 |    |            |          |
| 195 | 1  | 13 | 285 | 71  |    |            |          |
| 196 | 3  |    | 286 | 20  |    |            |          |
|     |    |    | 287 | 5   |    |            |          |
| 203 | 2  | 14 | 288 | 3   |    |            | C 315    |
|     |    |    | 289 | 3   |    |            |          |
| 227 | 1  | 18 |     |     |    |            | Fe 112 1 |
| 228 | 6  |    | 292 | 2   |    |            |          |
| 229 | 17 |    |     |     |    |            |          |
|     |    |    | 290 | 1   |    |            |          |
| 233 | 1  | 19 |     |     |    |            |          |
|     |    |    | 320 | 2   |    |            |          |
| 240 | 3  | Ne | 321 | 4   |    |            |          |
| 242 | 3  |    |     |     |    |            |          |
|     |    |    | 369 | 1   |    |            |          |
| 262 | 13 | 24 | 370 | 1   |    |            |          |
| 263 | 14 |    |     |     |    |            |          |
| 264 | 9  |    | 392 | 1   |    |            |          |

Fe<sub>3.7</sub>C

393

ph blank.  
 ph 4 x DW with ph just under carbide



|     |   |     |     |
|-----|---|-----|-----|
| 8   | 1 | 277 | 1   |
| 57  | 1 | 278 | 3   |
| 58  | 5 | 279 | 13  |
|     |   | 280 | 104 |
| 102 | 4 | 281 | 167 |
| 103 | 4 | 282 | 26  |
| 104 | 3 | 283 | 6   |
|     |   | 284 | 1   |
| 186 | 6 | 285 | 2   |
| 187 | 1 | 286 | 1   |
| 202 | 1 | 316 | 1   |
| 225 | 1 | 324 | 1   |
| 226 | 2 |     |     |
|     |   | 331 | 1   |
| 230 | 1 |     |     |
|     |   | 961 | 1   |
| 239 | 1 |     |     |
| 259 | 1 |     |     |
| 260 | 3 |     |     |
| 261 | 8 |     |     |
| 270 | 1 |     |     |
| 274 | 1 |     |     |
| 275 | 6 |     |     |
| 276 | 7 |     |     |

~~338~~  
 57



~ 300 ions - stopped detecting, ? end of carbonate

pk > where spectrum taken  
 axial spectrum pk > 9.97 keV

0.4

~~0.2~~

spectrum - rapid!

2nd spectrum

1000 ions

| pk  | count | pk  | count | pk   | count |
|-----|-------|-----|-------|------|-------|
| 56  | 13    | 272 | 6     | 56   | 19    |
| 57  | 21    | 273 | 9     | 57   | 44    |
| 58  | 21    | 274 | 120   | 58   | 21    |
|     |       | 275 | 405   | 59   | 2     |
| 130 | 5     | 276 | 657   | 130  | 7     |
| 131 | 15    | 277 | 106   | 131  | 2     |
|     |       | 278 | 25    |      |       |
| 171 | 2     | 279 | 5     | 170  | 2     |
|     |       | 280 | 1     |      |       |
| 182 | 4     | 281 | 2     | 182  | 2     |
| 183 | 1     | 282 | 1     |      |       |
| 184 | 1     |     |       |      |       |
| 196 | 1     | 309 | 1     | 196  | 2     |
| 197 | 2     | 311 | 1     | 197  | 2     |
|     |       |     |       |      |       |
| 221 | 1     | 389 | 1     |      |       |
| 222 | 4     |     |       | 2223 | 388 1 |
|     |       |     |       | 2222 | 390 1 |
| 233 | 2     |     |       | 2271 |       |
| 235 | 2     |     |       |      |       |
|     |       |     |       |      |       |
| 256 | 4     |     |       | 256  | 6     |
|     |       |     |       |      |       |
| 264 | 1     |     |       | 269  | 3     |
| 270 | 29    |     |       | 270  | 22    |
| 271 | 42    |     |       | 271  | 39    |

Matrix, adjacent to last spectra

q. 20 + 2 → 1.8 → 1.85  
225-550

ind mm, 100v lens, pulse

|    |    |    |    |    |     |
|----|----|----|----|----|-----|
| 56 | 24 | 56 | 27 | 56 | 35  |
| 57 | 51 | 57 | 67 | 57 | 100 |
| 58 | 22 | 58 | 44 | 58 | 51  |
| 59 | 1  | 59 | 1  |    |     |

|    |   |    |   |    |   |
|----|---|----|---|----|---|
| 79 | 1 | 78 | 2 | 78 | 1 |
|----|---|----|---|----|---|

|     |   |  |    |     |   |
|-----|---|--|----|-----|---|
| 182 | 2 |  | 12 | 182 | 2 |
|-----|---|--|----|-----|---|

|     |   |     |   |     |    |
|-----|---|-----|---|-----|----|
| 196 | 2 | 195 | 1 |     | 14 |
| 197 | 1 | 197 | 3 | 197 | 1  |

|     |   |     |   |  |    |
|-----|---|-----|---|--|----|
| 207 | 1 | 207 | 1 |  | 16 |
|-----|---|-----|---|--|----|

|     |   |     |   |    |     |   |
|-----|---|-----|---|----|-----|---|
| 224 | 1 | 225 | 1 | Ne | 224 | 4 |
|     |   | 227 | 1 |    |     |   |

|     |   |  |  |     |   |
|-----|---|--|--|-----|---|
| 269 | 1 |  |  | 269 | 1 |
|-----|---|--|--|-----|---|

|     |    |     |    |     |    |
|-----|----|-----|----|-----|----|
| 270 | 33 | 270 | 36 | 270 | 17 |
|-----|----|-----|----|-----|----|

|     |    |     |    |     |    |
|-----|----|-----|----|-----|----|
| 271 | 36 | 271 | 55 | 271 | 54 |
|-----|----|-----|----|-----|----|

|     |    |     |   |     |   |
|-----|----|-----|---|-----|---|
| 272 | 11 | 272 | 8 | 272 | 9 |
|-----|----|-----|---|-----|---|

|     |   |     |   |     |   |
|-----|---|-----|---|-----|---|
| 273 | 6 | 273 | 3 | 273 | 4 |
|-----|---|-----|---|-----|---|

|     |     |     |    |     |    |
|-----|-----|-----|----|-----|----|
| 274 | 118 | 274 | 66 | 274 | 44 |
|-----|-----|-----|----|-----|----|

|     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|
| 275 | 457 | 275 | 394 | 275 | 204 |
|-----|-----|-----|-----|-----|-----|

|     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|
| 276 | 611 | 276 | 619 | 276 | 626 |
|-----|-----|-----|-----|-----|-----|

|     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|
| 277 | 122 | 277 | 126 | 277 | 170 |
|-----|-----|-----|-----|-----|-----|

|     |    |     |    |     |    |
|-----|----|-----|----|-----|----|
| 278 | 17 | 278 | 33 | 278 | 36 |
|-----|----|-----|----|-----|----|

|     |   |     |    |     |    |
|-----|---|-----|----|-----|----|
| 279 | 1 | 279 | 10 | 279 | 10 |
|-----|---|-----|----|-----|----|

|     |   |     |   |     |   |
|-----|---|-----|---|-----|---|
| 280 | 4 | 280 | 2 | 280 | 2 |
|-----|---|-----|---|-----|---|

|     |   |     |   |     |   |
|-----|---|-----|---|-----|---|
| 281 | 3 | 281 | 3 | 281 | 1 |
|-----|---|-----|---|-----|---|

|     |   |  |  |     |   |
|-----|---|--|--|-----|---|
| 282 | 1 |  |  | 282 | 1 |
|-----|---|--|--|-----|---|

320 1

ph blank

ph x > where last spectrum took

ph x > 1 more ph diam's from boundary

9-21 + 2 2) 5/550

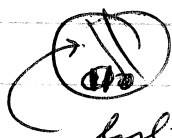
|     |     |    |     |               |     |
|-----|-----|----|-----|---------------|-----|
| 55  | 1   | 55 | 2   | 55            | 2   |
| 56  | 66  | 56 | 70  | 56            | 57  |
| 57  | 171 | 57 | 168 | 57            | 170 |
| 58  | 79  | 58 | 50  | 58            | 60  |
|     |     | 59 | 1   | <del>59</del> |     |
| 65  | 1   | 65 | 1   |               |     |
|     |     | 78 | 1   |               |     |
| 109 | 1   |    |     |               |     |

|     |     |            |        |     |     |
|-----|-----|------------|--------|-----|-----|
| 197 | 6   | 195        | 1      |     |     |
| 198 | 1   | 196        | 2      | 196 | 1   |
|     |     | 205        | 1      | 197 | 1   |
|     |     | <u>269</u> | 4      | 268 | 1   |
| 269 | 1   | 270        | 21     | 269 | 5   |
| 270 | 25  |            | 1 40   | 270 | 25  |
| 271 | 08  |            | 2 8    | 271 | 40  |
| 272 | 8   |            | 3 5    | 272 | 7   |
| 273 | 5   |            | 4 110  | 273 | 5   |
| 274 | 112 |            | 5 412  | 274 | 145 |
| 275 | 402 |            | 6 460  | 275 | 483 |
| 276 | 544 |            | 7 80   | 276 | 409 |
| 277 | 104 |            | 278 25 | 277 | 57  |
| 279 | 6   |            | 279 4  | 278 | 21  |
| 280 | 1   |            | 280 9  | 279 | 6   |
| 281 | 2   |            | 281 0  | 280 | 4   |
|     |     |            | 282 1  | 281 | 1   |
| 222 | 1   |            | 286 1  | 282 | 1   |
|     |     |            | 302 1  | 321 | 1   |
|     |     |            | 365 1  | 758 | 1   |

ph x 4 where spectra taken

IAP Div x 3

- blank



last spectrum here

Fe<sup>2+</sup> 60 sec

C<sup>2+</sup> | v little, ? niteline  
C<sup>2+</sup>

Fe<sup>2+</sup> 107 = 670 ← - 210 = 460

C<sup>++</sup> 52 ← 420 ← 210

14- ) 65 ← 525 ← 225

C<sub>12</sub> 67 510 201

- Si<sup>2+</sup> 65 60 sec

Si<sup>2+</sup> 4 "

C<sup>+</sup> 60 "

C<sup>+</sup> 4 "

IAP x 3

IAP mp/oh

IAP x 3

Fe<sup>2+</sup> dud

Fe<sup>2+</sup> 60s

Si

Si

C<sup>+</sup>

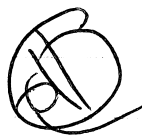
C<sup>+</sup>

C<sup>++</sup>

C<sup>++</sup>

IAP x 3

More slightly IAP x 3



axial 10

Fe<sup>2+</sup>  
Si<sup>2+</sup>  
Si<sup>2+</sup>  
C<sup>+</sup>  
C<sup>+</sup>  
? C<sup>+</sup>

IAP x >

Move to top IAP x >

Fe<sup>2+</sup>

all ~ 60 min

Si<sup>2+</sup>

Si<sup>2+</sup>

C<sup>+</sup>

C<sup>+</sup>

Fe<sup>2+</sup>

Si<sup>2+</sup>

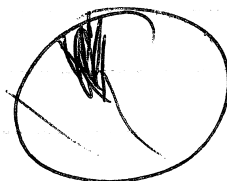
faster, 12 hrs

C<sup>+</sup>

12 hrs

C<sup>2+</sup> dnd

end of pln



IAP Mph

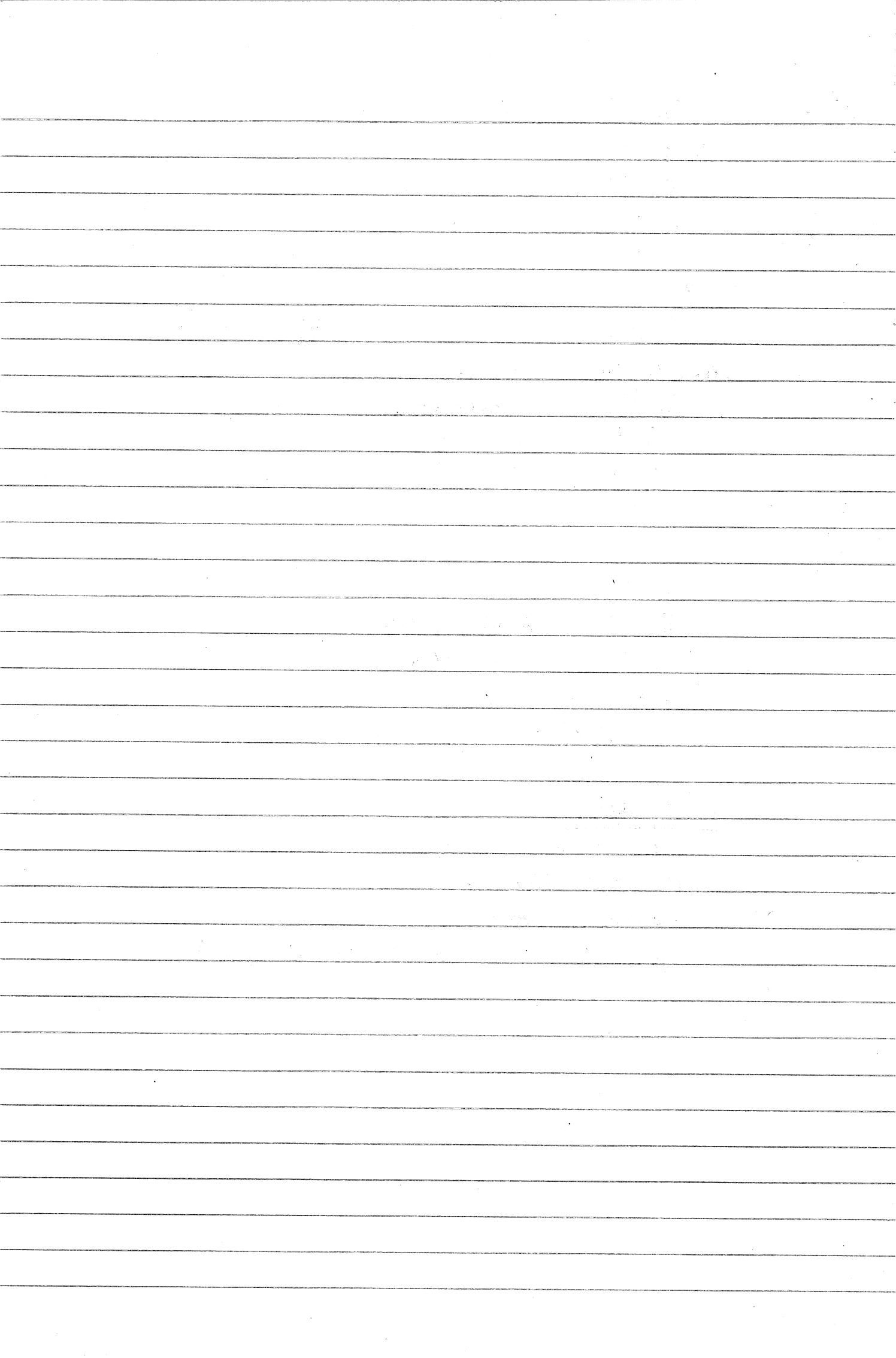
IAP x >

More left IAP x >

More down IAP x >

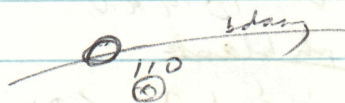
ph x >

(IAP area top right)



6/2/78

PSW steps same tip



T 389 off bdary to look @ carbon distribution

$10.67 + 1.6$       260/550       $6 \cdot 10^{-7}$  Ne / 60       $\sim 4000$  ions  
 all at same  $V_{tip}$

Previously spectrum with blue box ( $?V_p, V_c, V_n?$ ) New 6110

|    |    |     |   |
|----|----|-----|---|
| 11 | 1  | 267 | 4 |
| 54 | 12 | 268 | 4 |
| 55 | 23 | 269 | 1 |
| 56 | 12 |     |   |
| 57 | 1  | 240 | 1 |

188 2      451 1

190 2

224 1

225 5

226 10

227 7

228 1

229 1

258 10

259 32

260 27

261 8

262 10

263 267

264 240

265 260

266 28

7/2/78 Same tip

~~ph~~ DIV 10.9 KV  
ph blank

ph  $\frac{1}{2}$   $\frac{1}{2}$  1 2 CDW  
2  $\frac{1}{2}$   $\frac{1}{2}$  DIV

more slightly  $\frac{1}{2}$   $\frac{1}{2}$  1 DIV  
1  $\frac{1}{2}$   $\frac{1}{2}$  CDW



where spectrum yesterday (~72C)



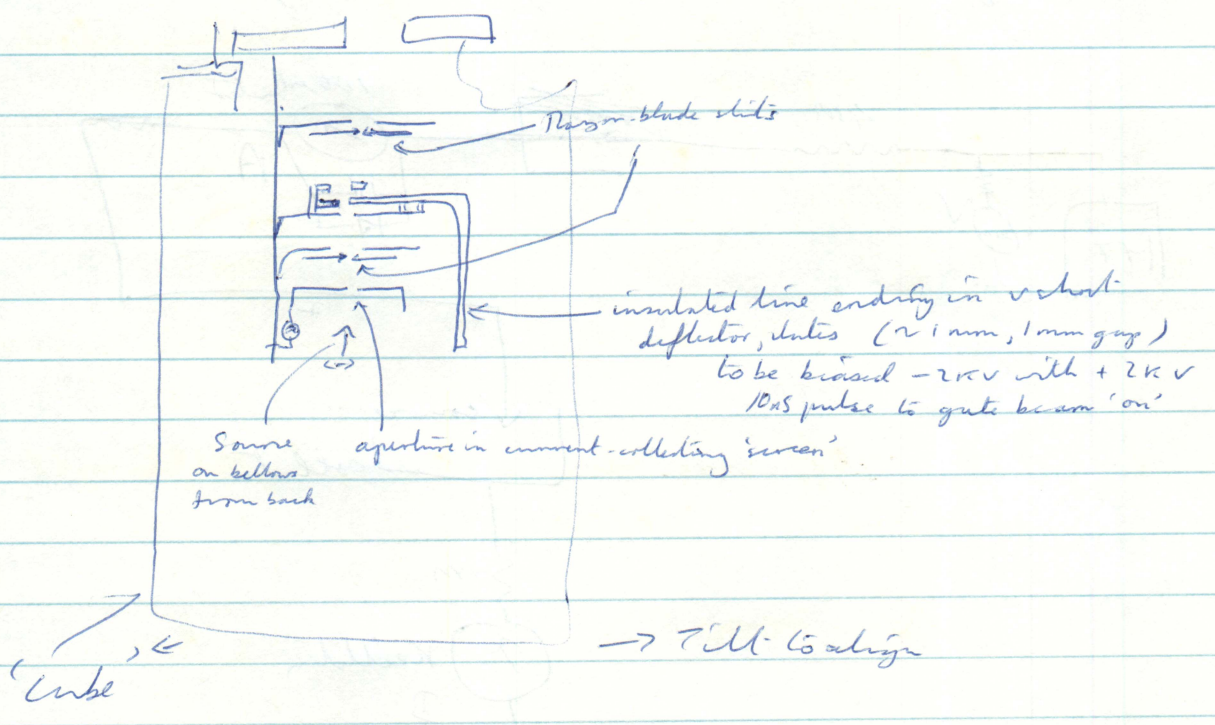
7  $\frac{290}{11 + 1.56}$  off same blank as 289, slightly to right  
260/550

~ 7000  $\Omega$

ph 4 x DIV 11.65 KV @ spectrum place ~~⊙~~  
ph blank



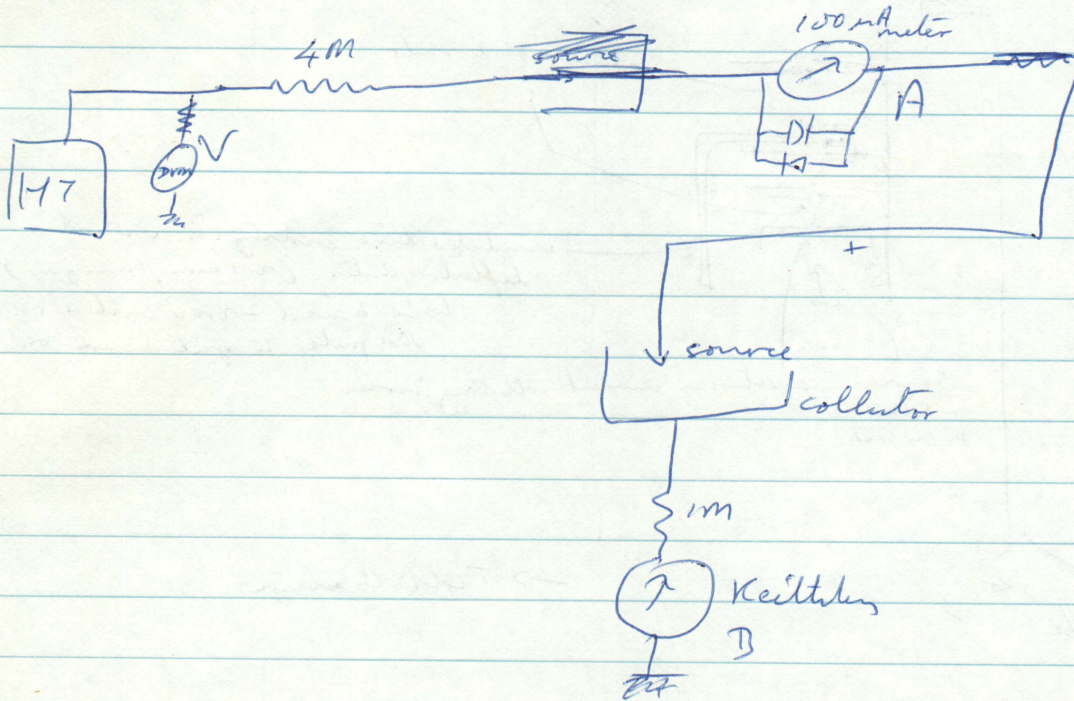
Designing bits of ICP Mass Spectrometer for Carbon Ion sources



& designing interface for KVM

12/3/79

Measuring V/A characteristics of Ga ion source from Kalthan

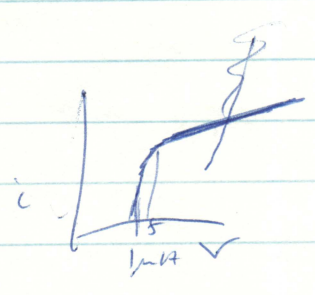


| V     | A         | D                   |
|-------|-----------|---------------------|
| 8.85  | 1         |                     |
| 9.05  | 2         |                     |
| 9.06  | 3         |                     |
| 9.07  | 4         |                     |
| 8.40  | 2 $\mu$ A | $4 \cdot 10^{-7}$ A |
| 8.88  | 5         | $7.9 \cdot 10^{-7}$ |
| 9.52  | 8         | $1.5 \cdot 10^{-6}$ |
| 9.90  | 10        | 7 $\mu$ - rising    |
| 10.54 | 10        | 8 "                 |
| 9.90  | 5         | 4 "                 |

Had to run up to ~ 12.5 KV to get to strike properly.

50  $\mu$ A meter in  
 HT lead to top  
 Keithley 65  
 collector via 1M $\Omega$

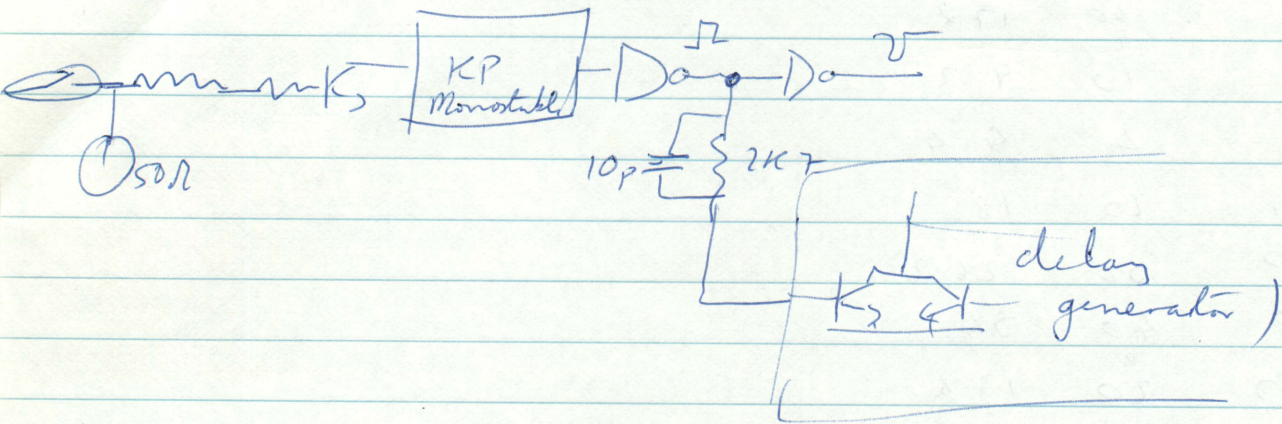
| KV   | $\mu$ A | $\mu$ A           |
|------|---------|-------------------|
| 6.60 | 19      | 17                |
| 5.51 | 10      | 9.2               |
| 6.64 | 20      | 17.8              |
| 7.97 | 25      | 22                |
| 7.16 | 20      | 17.8              |
| 8.75 | 20      | 26                |
| 7.20 | 20      | 17.8              |
| 6.01 | 10      | 9.2               |
| 5.51 | 4       | 4.4               |
| 7.09 | 20      | 18                |
| 8.80 | 20      | 26.2              |
| 9.50 | 40      | 24                |
| 7.27 | 20      | 17.8              |
| 9.50 | 25      |                   |
| 9.50 | 29      |                   |
| 10   | 48      | 25                |
| "    | 45      | 24                |
| "    | 47      | 28                |
| "    | 41      | 22                |
| "    | 45      |                   |
| 6.1  | 10      |                   |
| 6.09 | 10      | 9.2               |
| 5.66 | 5       | 4.7               |
| 5.84 | 5.5     | 5.4 after 10 mins |
| 5.45 |         | 3                 |
| 5.27 |         | 2                 |
| 5.22 |         | 1.5               |
| 5.32 |         | 1                 |



If approached slowly will run down to  $\approx$  1  $\mu$ A collector current

Pause for conference (1982) at Cavendish - papers + slides.

- fixed IAS electronics ( $\Rightarrow$  shorter delay, more stable)

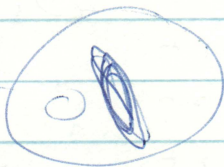


~ 3 April 79

IAP DW  $\times 3$  <sup>IAP blank</sup> 12-3 kV

12-3 + 2.6

top of spec



|                  |     |                     |
|------------------|-----|---------------------|
| Fe <sup>2+</sup> | 50s |                     |
| C <sup>2+</sup>  | 50s |                     |
| C <sup>2+</sup>  | 50s | 50-57               |
| C <sup>2+</sup>  | 60s | - slightly quenched |
| Fe <sup>2+</sup> | 50s | - 77-100            |

640 - 210 = 430      H = 81

C<sup>2+</sup> = 200 = 51

C<sup>+</sup> = 282 = 61

N<sup>+</sup>, Si<sup>2+</sup> = 204 = 62

C<sub>18</sub> = 345 = 70

C<sub>24</sub> = 398 = 75

C<sub>36</sub> = 488 = 106

PE<sub>21</sub> = 452 = 102

- ? IAP DIV

Fe<sup>2+</sup> 20

C<sup>2+</sup> 40

C<sup>+</sup> 40

N<sup>+</sup> 40

C<sub>18</sub> 40

C<sub>24</sub> - spotted (Fe<sup>2+</sup>)

C<sub>24</sub> 40

IAP  $\times 3$

1 IAP  $\times 3$  same carbide

Fe<sup>2+</sup>

C<sup>2+</sup>

C<sup>2+</sup>

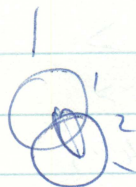
C<sup>2+</sup>

C<sup>+</sup>

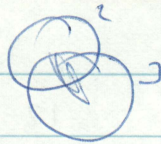
Fe<sup>2+</sup>

IAP  $\times 1$

IAP N after



IAP x 3



More IAP x 3

Fe<sup>2+</sup> 40s

C<sup>2+</sup>

C<sup>2+</sup>

C<sup>2+</sup>

Fe<sup>2+</sup> - HT set unstable again

IAP x 3

More IAP x 4 1 chunk

IAP blank

Fe<sup>2+</sup> ~ 30

C<sup>2+</sup>

C<sup>2+</sup>

C<sup>2+</sup>

Fe<sup>2+</sup> - ep spread

Fe<sup>2+</sup> rapid ~ 4-5 planes, 20s.

C<sup>2+</sup> 40

IAP x 3



IAP x 3

Fe<sup>2+</sup>

C<sup>2+</sup>

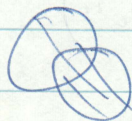
C<sup>2+</sup>

C<sup>2+</sup>

Fe<sup>2+</sup>

IAP x 2

IAP Mixture



IAP x 3

IAP x 3

Fe<sup>2+</sup> 40s

C<sup>2+</sup>

C<sup>2+</sup>

C<sup>2+</sup>

Fe<sup>2+</sup>

IAP x 3

Dark to carbides @ top of bedrock

IAP x)

Fe<sup>2+</sup> 40%

C<sup>2+</sup> "

C<sup>2+</sup> -

C<sup>2+</sup> "

Fe<sup>2+</sup> "

IAP x)

ph x ~ 1/2 dozen

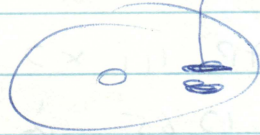
ph bluish.

IAP x 4

Fe<sup>2+</sup> rapidly

- flushed.

IAP bluish.



5

4 April 79

SAM NiAl spec.

Spec 9 - broke transmission to mic

Spec 5 as ground + outgassed 200 C

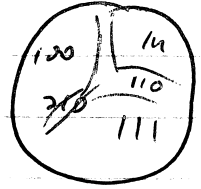
ph blank

ph x 3

ph Muffin

ph x 4

13.9 keV Ne DW



I think

IAP 111 x 3

2.5 + 12.65 in room.

IAP 111 x 3

Ni 6200 = 640 = 400

Al 60 = 510 = 300

H 80

Ni<sup>+</sup> 620 = 800 = 120

Ni<sup>2+</sup> 50

Al<sup>2+</sup> 50

Ni<sup>2+</sup> 40 grains

Al<sup>2+</sup> 40 ~

IAP Muffin

2

Ni<sup>2+</sup>

Al<sup>2+</sup>

14  
still

Al<sup>2+</sup>

H<sup>+</sup>

IAP x 3

ph x 4

200 IAP x 3 ordered region central.

Ni<sup>2+</sup> 60s empty rather cloudy.

Al<sup>2+</sup> ~

- flushed when tried to increase rate

IAP blank

ph blank

- fell off Ni tube when extracted.





New Specimen

orthorhombically dried N<sub>2</sub> AC

ph x 3 15-22 v coming in.

1 AP all around

~ central pole

1 AP x 3



~ 14 + 2.6

- 2 bit up channels

N<sub>2</sub><sup>2</sup>

AL<sup>2</sup>

N<sub>2</sub><sup>2</sup>

AL<sup>2</sup>

1 AP x 3

ph x 4 procther



not whole part

15.69 + 2.7.

pulse too small I think

$$57 = 470 - 210 = 260 = 32.$$

no delay line

N<sub>2</sub><sup>2+</sup>

~ 50

← AP of top of spec, ~ 420?

12.9 + 2.6

AL<sup>2+</sup>

~ 34

1 AP up th

?

N<sub>2</sub><sup>1</sup>

AL

N<sub>2</sub>

AL

1 AP x 3

1 AP x 3 a bit lower

N<sub>2</sub><sup>1</sup> 203

AL :

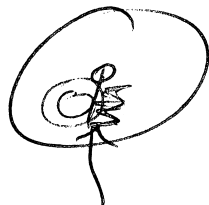
N<sub>2</sub> ~ faster

AL :

AL

1 AP x 3

ph x 4



? disordered region

LAP x 3

Ni

Al

Ni

Al

Al

LAP x 3

ph  $\frac{1}{4}$   $\frac{1}{2}$  1

LAP x 3

Ni

Al

Al

Ni

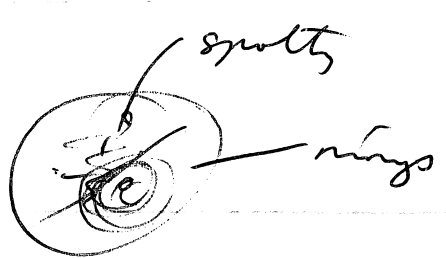
LAP x 2

LAP Mph 4

LAP x 3

ph x 3

ph x 3

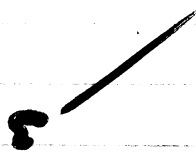


3200

Surface

19.5 + 2.84

Div 17.8



Spectrum off ragged bit of spec next to 111

17.65 + 2.8

420/561

110<sup>-6</sup> Ne / 60

Ni<sup>2+</sup> 325, Al<sup>2+</sup> 228

211 Al

574 Ni

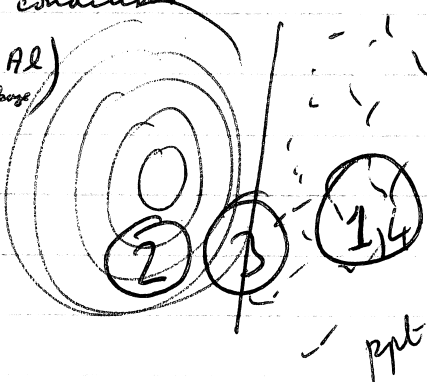
Ni<sub>2.57</sub> Al

Al 27.9 ± 1.9 %

88 Al

682 Ni

Al 11.4 ± 1.2 %



ppt

1 = 27.9 ± 1.9

2 = 11.4 ± 1.2

3 = 28.9 ± 2.1

4 = 27.9 ± 1.5

apparently loading up 5% of nickel box of H.

small region

Client Matrix

①

②

③

4

|     |     |     |     |     |
|-----|-----|-----|-----|-----|
| 40  | 3   | 12  | 7   | 17  |
| 44  | 86  | 81  | 85  | 110 |
| 45  | 127 | 106 | 208 | 208 |
| 46  | 10  | 6   | 17  | 10  |
|     |     |     | 47  | 1   |
| 67  | 1   | 60  | 1   | 76  |
|     |     |     |     | 99  |
|     |     |     |     | 100 |
|     |     |     |     | 101 |
|     |     |     |     | 120 |
|     |     |     |     | 122 |
| 145 | 4   | 144 | 4   | 134 |
| 146 | 40  | 18  | 42  | 139 |
| 147 | 101 | 35  | 82  | 145 |
| 148 | 67  | 30  | 64  | 146 |
| 149 | 4   | 2   | 3   | 147 |
|     |     |     |     | 150 |
|     |     |     |     | 148 |
|     |     |     |     | 149 |
|     |     |     |     | 150 |
|     |     |     |     | 151 |
|     |     |     |     | 154 |
|     |     |     |     | 170 |
|     |     |     |     | 177 |
|     |     |     |     | 174 |
|     |     |     |     | 180 |
|     |     |     |     | 186 |
|     |     |     |     | 194 |
|     |     |     |     | 195 |
|     |     |     |     | 210 |
| 211 | 19  | 20  | 17  | 29  |
| 212 | 100 | 106 | 71  | 140 |
| 213 | 160 | 200 | 166 | 258 |
| 214 | 82  | 87  | 79  | 110 |
| 215 | 21  | 28  | 22  | 29  |
| 216 | 52  | 74  | 27  | 89  |
| 217 | 62  | 67  | 50  | 79  |
| 218 | 14  | 14  | 8   | 6   |

①

②

③

④

|     |   |     |     |     |
|-----|---|-----|-----|-----|
| 219 | 8 | 8   | 6   | 14  |
| 220 | 8 | 16  | 8   | 12  |
| 221 | 5 | 5   | 2   | 4   |
|     |   | 222 | 2   | 1   |
| 223 | 2 | 1   |     | 2   |
| 224 | 1 | 2   | 4   | 4   |
|     |   |     | 225 | 1   |
|     |   |     | 227 | 1   |
|     |   |     | 296 | 1   |
|     |   |     | 298 | 4   |
|     |   |     | 298 | 2   |
|     |   |     | 4   | 10  |
|     |   |     | 2   | 4   |
|     |   |     | 200 | 1   |
|     |   |     | 4   | 2   |
|     |   |     | 200 | 1   |
|     |   |     | 201 | 1   |
|     |   |     | 202 | 1   |
|     |   |     | 204 | 1   |
|     |   |     | 2   | 206 |
|     |   |     | 1   | 207 |
|     |   |     | 1   | 208 |
|     |   |     | 674 | 1   |

$314 \text{ HR} = 27 \cdot 88 = 15$   
 $812 \text{ N:}$   
 $\frac{1126}{2232}$

$320$   
 $226$

$196 \text{ A:}$   
 $482 \text{ N:}$

$678$   
 $= 28 \cdot 97 = 2.1$

Churs.  
5/2/21

same tip  
ph bluish  
ph x 2  
ph x 2


IAP bottom left

Ni 80  
Al 60  
Ni 20 - 40 = ~~50~~ 20  
Al 20

? Al

24 = 60 280 24 = 270 = 40  
24 = Ne<sup>+</sup>

IAP x 4

IAP x 2  $\gamma'$  @ top 

Ni - puffed

< IAP DW

ph x 2 -  $\gamma'$  visible, pretty

ph bluish

ph x lots.

IAP x  $\gamma'$  22-4 kV

Ni

Al

Ni

Al - dnd

Al

Ni

Al - dnd ?

Al

IAP bluish 5

Ni

Al - puffed

~~Al~~

ph

28.5 + 3 !!!

IAP x 2?

NB  $\gamma'$  proud of surface, so Ni & Al from ppt, not from matrix, for first few pixels



ph @ DW }  
ph (DIV) :

ph @ after N's pulsing in NE .

→  $\gamma'$  ⇒ spotty after pulsing . 27.5 kV

ph blank

IAP blank

Extract specimen, still ok.

6 April M AC Sun 2 10 hrs, Laked.

15.6KV ph x > after 100 while turning up  
ph Mph

ph x >

ph x > < Div

IAP x > ~ axial 200

N<sub>1</sub>

AL

N<sub>1</sub>

AL

AL

~ 24 - v little

IAP x >

IAP

(11) IAP x 2

NL 60 sec rapid

AL

AL

IAP x >

IAP x > left-

IAP x >

N<sub>1</sub> 60 sec

AL

AL

N<sub>1</sub>

IAP x > 18.1 KV

~~RMS~~ ~~IAP x >~~ IAP Mph 2

~~RMS IAP x >~~ ph x >

IAP x > RMS, y' @ Ep of

N<sub>1</sub> 60

AL

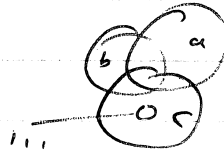
N<sub>2</sub> 40 further

AL

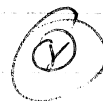
IAP x >



+ 2.5 pulse

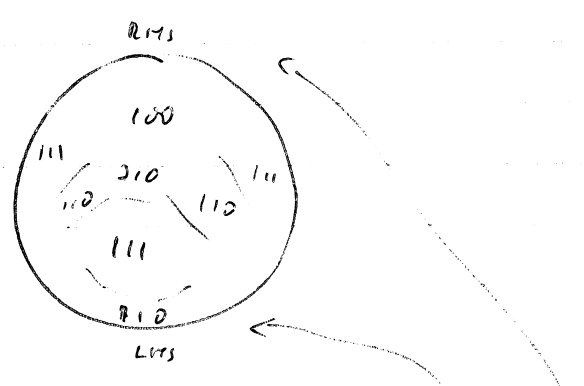
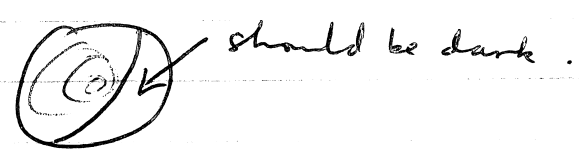


17.42 DMV



IAP x 2  
 N<sub>c</sub> 50s      3800 v applied 60 cps pulses  
 N<sub>c</sub> 50s      4000 v      -      '  
 N<sub>c</sub> 50s      3600 v      -      '  
 IAP x 2

This to test Walker's theory on noise of  $\epsilon_p$   
 of applying large pulse  
 - set up with mantle vignetting image

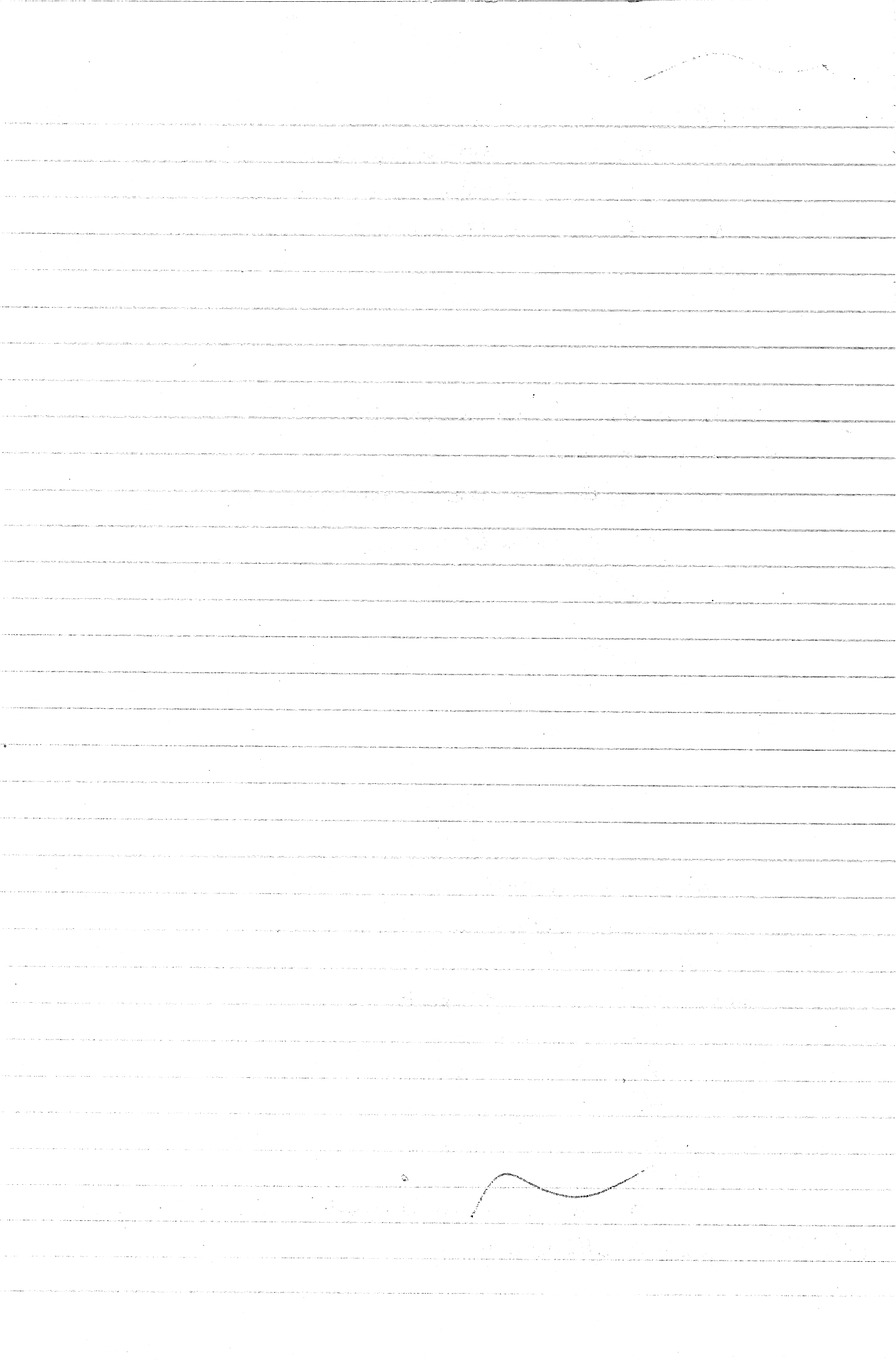


$\mu_h \times 2$  - axial  
 $\mu_h \times 2$  bottom  
 $\mu_h \times 2$  top

220 IAP x 4      ~ top 1770  
 N<sub>c</sub> 40s  
 AL  
 N<sub>c</sub>  
 AL

IAP x 2  
 $\mu_h \times 2$  after us increase - 'measles' - dark patches of  $\gamma^1$   
 $\mu_h \times 2$  after  $\gamma^1$  crop

18-20W





5

15/5/79 Ga ion source in TOF machine  
 $B_0 = 9.62 \text{ kV} \sim 5 \cdot 10^{-7}$

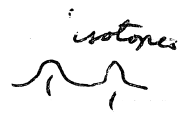
$i_{\text{collector}} = 10 \mu\text{A}$   $i_{\text{total}} \sim 50 \mu\text{A}$

Timebase  $1 \mu\text{s/cm}$

vert.  $.05/\text{cm} + \times 10 \text{ probe} = .5 \text{ cm}$

f4  $1, \frac{1}{2}$   $\frac{1}{4}$   $\frac{1}{8}$   $\frac{1}{16}$   $\frac{1}{32}$   $\frac{1}{64}$   $\frac{1}{128}$   $\frac{1}{256}$   
Mplm (TAE camera) 2

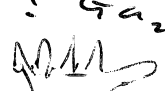
f4  $1, \frac{1}{2}, \frac{1}{4}, \frac{1}{8}, \frac{1}{16}$   
 f 18  $1, \frac{1}{2}, \frac{1}{4}, \frac{1}{8}, \frac{1}{16}$

f4  $\frac{1}{6}, \frac{1}{8}, \frac{1}{4}, \frac{1}{2}, 1, 2$  timebase delayed,  $50 \text{ ns/cm}$  

f4  $2, 1, \frac{1}{2}, \frac{1}{4}, \frac{1}{8}, \frac{1}{16}, \frac{1}{32}, \frac{1}{64}, \frac{1}{128}$  dimmer trace  
 timebase  $2 \text{ sec/cm}$

f4 current increased to  $55 \mu\text{A}$ ,  $110 \text{ u}$

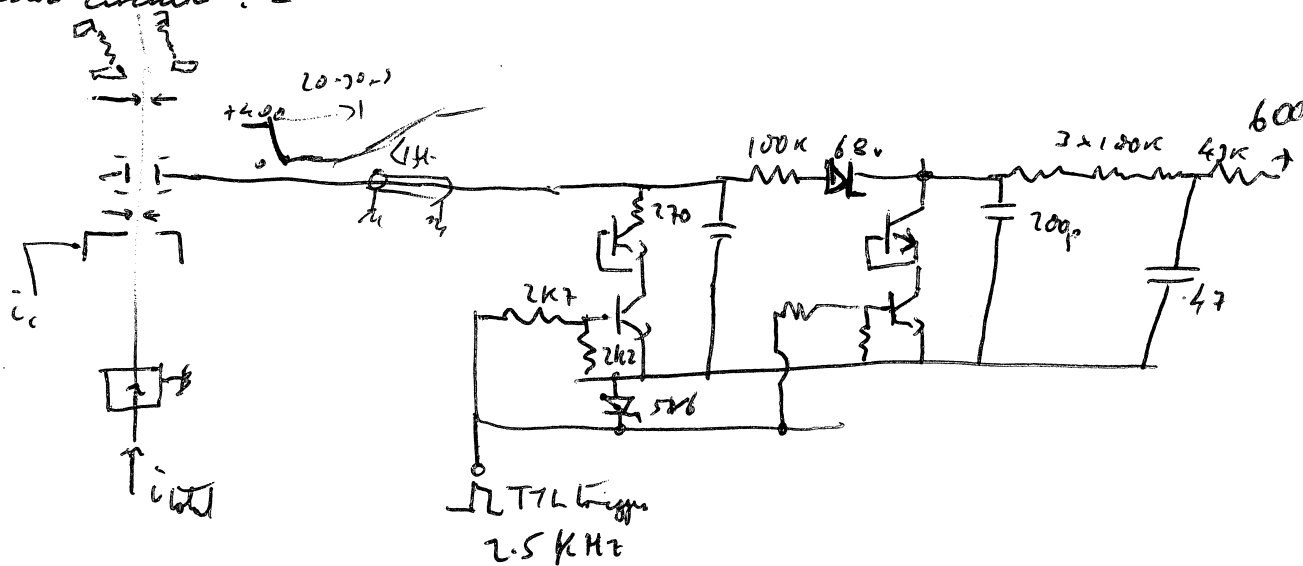
11.23 V

set of pics?  $\text{Ga}_2^+$   
 'blush' 

|     |     |
|-----|-----|
| 7.8 | 5.6 |
| 5.6 | 1.4 |
|     | 2.2 |
|     | 4   |
|     | 5.6 |
|     | 7.8 |

Will run down to  $7-8 \text{ kV}$  at present.

These pictures were taken (lens not fitted to spectrometer) with the beam tilted mechanically & chopped across the aperture with automatic transistor circuit :-



Solun chromati + acetic acid <sup>Göttingen</sup> (Cu 17e polsh)  
2

2

12/5/79 slit lens added to spectrometer. AM @ ~ 1-2 kHz

$I_c$  5  $\mu$ A  $I_T$  ~ 20  $\mu$ A 11.4 kV

$V_{\text{anode}}$  -2 kV  $V_{\text{lens}}$  + 2 kV

ph camera blank

2  $\mu$ s/cm 1 cm ft vert ~ .8 v/cm (line probe)  
1 cm "

ph output 3

$\frac{1}{2}$   $\frac{1}{4}$   $\frac{1}{8}$   $\frac{1}{16}$   $\frac{1}{32}$  2  $\mu$ s/cm

$\frac{1}{32}$   $\frac{1}{16}$   $\frac{1}{8}$   $\frac{1}{4}$   $\frac{1}{2}$  1 200 ns/cm delayed timebase

ph blank

lens 1.85 kV  $I_T$  10.95  $I_c$  5  $\mu$ A

2  $\mu$ s/cm, 100 ns/cm dual

~ max signal 1  $\frac{1}{4}$   $\frac{1}{16}$

less signal  $\frac{1}{16}$   $\frac{1}{4}$  1 better dynamic

2 1  $\frac{1}{2}$   $\frac{1}{4}$   $\frac{1}{8}$  etc with pulse voltage increased

slightly  $\Rightarrow$  no jitter, superb resolu

100 ns/cm - resolved isotops ~ x5-

2  $\mu$ s - overall view.

No sign of  $G_{a_2}^+$

3 x .5  $\mu$ s/cm.

3 x 1  $\mu$ s/cm.

300 ns

4.3  $\mu$ s

$$\frac{DM}{\mu} = \frac{2.01}{6} = \frac{.6}{4.3}$$

# μ Mplh 4

| kV    | $i_T$              |                        |                                      |               |   |
|-------|--------------------|------------------------|--------------------------------------|---------------|---|
| 11.57 | 20                 | $\frac{1}{2}$          | $\frac{1}{4}$                        | $\frac{1}{2}$ | 1 |
| 12.12 | 40                 | 1                      | →                                    |               |   |
| 15    | 100                | $\frac{1}{2}$          | → → $Gr_2^{2+}$                      |               |   |
| 11.47 |                    | →                      | → now has $Gr_2^+$ & sputtered wires |               |   |
| 12.06 | <u>blank</u> 1 sec |                        |                                      |               |   |
| 12.06 | $\sim 20 \mu A$    | $1 \times \frac{1}{2}$ | $\frac{1}{2}$                        | $\frac{1}{2}$ |   |

? few others

blank.

Now runs @ 8 kV (up to 45 kV used)

Dimers persists when volts reduced,  $i_c \sim 40 \mu A$ .

12.06  $40 \mu A i_c$  Max of 3 peaks  $\sim 11$

(end of film  
source runs down to 10.4 kV - seems to like getting hot.

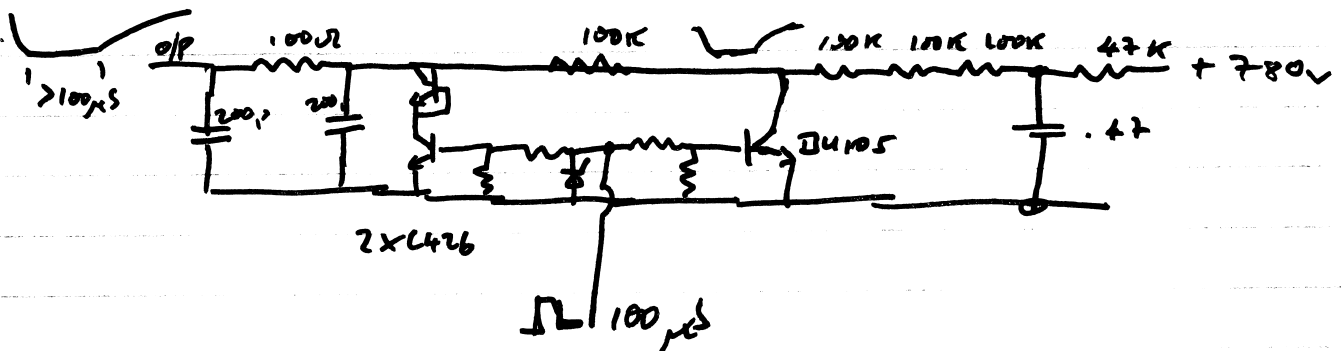
# μ Mplh 5

More peaks 2  $\mu s$ , 1  $\mu s$  / cm of source  
remains @  $i_c \sim 50 \mu A$ ,  $i_T \sim 200 \mu A$

$\Rightarrow Gr_2^+$  as well (v small peak)  $\sim 20 \mu A$

- last few peaks with reaction of pulser faster

->



Allegedly!

4

19/5/79 / Multisync Run

$2 \times 10^{-9} \sim 70^\circ$

He  $\rightarrow$  no image - ? wrong

Ne  $\rightarrow$  image, except @  $\sim$  Div  
- ragged surface

ph  $3 \times$  (Div 11.8  
 $3 \times$  Div 12.3

Tip was polished in  $\pm$  butoxyethanol, 25 v dc (ie just like Fe di)  
- etched @ boundaries if polished in Melonids KOH, or in NaOH,  
good & shiny in butoxy.

pop  $\rightarrow$  144 KV ph  $\times 4$

C = 3.6215 -04

13.35+2

320/561

2

$\begin{cases} 420 & 179 \Rightarrow 20 \\ 5020 & 235 \Rightarrow 20 \end{cases}$

267  $\approx$  48.8  $\mu\text{m}^2$

|       |         |        |       |
|-------|---------|--------|-------|
| 49 10 | 229 26  | 248 15 | 329 2 |
| 50 68 | 220 107 | 249 8  | 320 2 |
| 51 84 | 221 81  | 250 4  | 321 1 |
| 52 1  | 222 20  | 251 7  | 322 4 |
|       | 223 18  | 252 1  | 323 2 |
| 59 1  | 234 4   | 255 2  | 341 1 |
| 71 1  | 241 5   |        | 342 1 |
| 202 1 | 242 59  | 327 4  |       |
| 204 1 | 243 101 | 324 6  | 457 1 |
| 207 1 | 244 24  | 325 3  |       |
| 225 4 | 245 7   | 326 10 |       |
| 226 6 | 246 18  | 327 1  |       |
| 227 1 | 247 67  | 328 2  |       |

KV<sup>2</sup>

202 => 28

1.613 x t x t x v

5.029 - 04

320/561

3 x ph DIV 10:3 KV

320 / 561

13.1 + 2.23

Molto ripetuto =>

|         |       |         |         |                       |
|---------|-------|---------|---------|-----------------------|
| 171 6   | 328 1 | 0 3     | 245 19  | 459 1                 |
|         | 330 2 |         | 246 18  | 460 2                 |
| 225 6   | 331 3 | 49 22   | 247 107 | 463 1                 |
| 226 20  | 333 1 | 50 147  | 248 44  | 499 1                 |
| 227 39  | 334 2 | 51 150  | 249 13  |                       |
| 228 2   |       | 52 1    | 250 5   | 751 1                 |
| 299 6   |       |         | 251 17  |                       |
| 230 94  |       | 159 1   | 252 4   | 917 2                 |
| 231 270 |       | 203 1   | 253 1   |                       |
| 232 31  |       | 204 1   | 255 3   |                       |
| 233 12  |       |         | 256 3   |                       |
| 234 6   |       | 225 6   | 323 4   |                       |
| 235 9   |       | 226 26  | 324 9   | 225-236 1061          |
| 236 1   |       | 227 16  | 325 13  | 239-256 681           |
| 242 3   |       | 228 4   | 326 10  | 323-335 80            |
| 243 24  |       | 229 41  | 327 11  | 341-342 2             |
| 244 67  |       | 230 361 | 328 5   | 456-463 6             |
| 245 3   |       | 231 404 | 329 60  |                       |
| 247 7   |       | 232 94  | 330 6   | $\frac{a}{b} = 1.558$ |
| 248 9   |       | 233 51  | 331 2   |                       |
| 249 1   |       | 234 17  | 332 3   | 1800                  |
| 250 1   |       | 235 9   | 333 6   |                       |
| 252 1   |       | 236 1   | 334 1   |                       |
| 254 1   |       | 237 5   | 341 1   |                       |
| 255 2   |       | 241 1   | 342 1   |                       |
| 256 2   |       | 242 49  | 456 1   |                       |
| 257 2   |       | 243 272 | 457 1   |                       |
|         |       | 244 120 |         |                       |

4.824

220/561

Not Ru! - spec magnetic - spectrum probably Fe/Cu or Fe/Ni  
2<sup>nd</sup> spectrum off dark region (provided off line)

49 30

50 243

247 71

868 1

51 157

248 23

52 0

249 6

(3)

54 2

250 11

251 14

Ne 204-206

4

68 0

252 0

225-226

856<sup>527</sup><sub>a</sub>

69 1

253 1

240-254

656<sup>1020</sup><sub>b</sub>

254 4

219-330

88<sup>542</sup>

204 2

229-244

9<sup>14</sup>

205 1

219 1

455-462

7

206 1

222 0

225 16

220 6

$\frac{a}{b} = 1.005$

226 10

224 11

227 9

225 14

228 0

226 16

1620

229 129

227 4

230 421

228 6

24.4

231 122

229 11

232 74

230 2

233 21

231 7

234 14

232 5

235 5

233 2

236 1

234 1

240 1

240 0

241 14

241 2

242 205

245 1

244 197

247 2

244 29

455 1

245 7

456 2

246 60

459 2

460 1

462 1



Round Robin SS

6.45 + 1

ph blank ph x3 ~ 6.6 KV

155/561 6.46 + (1.16) - 1.25

| Row | Col 1 | Col 2 | Col 3 | Col 4 | Col 5 | Col 6 |
|-----|-------|-------|-------|-------|-------|-------|
| 0   | 1     | 299   | 1     | 241   | 150   | 699   |
| 13  | 2     | 300   | 1     | 242   | 51    |       |
| 67  | 4     | 24    | 311   | 1     | 243   | 15    |
| 68  | 38    |       | 312   | 1     | 244   | 14    |
| 69  | 112   |       |       |       | 245   | 9     |
| 70  | 12    | 24.9  | 316   | 7     | 246   | 27    |
| 71  | 3     |       | 317   | 31    | 247   | 57    |
|     |       |       | 318   | 10    | 248   | 11    |
| 158 | 5     |       | 319   | 2     | 249   | 8     |
| 159 | 2     |       | 320   | 3     | 250   | 1     |
| 160 | 1     | 25.7  | 321   | 8     | 251   | 4     |
|     |       |       | 322   | 243   | 25.15 | 253   |
| 222 | 2     |       | 323   | 562   | 254   | 2     |
|     |       |       | 324   | 287   |       |       |
| 238 | 12    | 14.16 | 325   | 62    | 25.8  | 257   |
| 239 | 46    |       | 326   | 66    | 258   | 7     |
| 240 | 10    |       | 327   | 40    | 259   | 1     |
| 242 | 1     |       | 328   | 46    |       |       |
| 244 | 1     | 27    | 329   | 161   | 26.3  | 265   |
| 247 | 1     |       | 330   | 90    |       |       |
| 251 | 1     |       | 331   | 24    | 48.6  | 441   |
| 252 | 2     | 15.8  | 332   | 20    |       |       |
| 271 | 2     | 18.3  | 333   | 35    | 50.6  | 460   |
| 283 | 1     | 20    | 334   | 706   |       | 464   |
| 284 | 0     | 28.06 | 335   | 1900  | 55.46 |       |
| 285 | 2     |       | 336   | 899   |       | 471   |
| 286 | 0     |       | 337   | 229   | 57.6  | 480   |
| 287 | 1     |       | 338   | 82    |       | 491   |
| 292 | 1     |       | 339   | 26    | 62    | 497   |
| 297 | 1     |       | 340   | 54    |       |       |

end, ph x1 7.25 KV

end of file

Ground home time (21.25)

20/5/79 Same specimen 160 / Ne  $110^{-9}$  @ stut, cold.

6.96 + 1.15 - 1.25  $\mu$ sec 7 391  
60K,  $10^{-7}$  Ne

170/561

$\Delta$  11,100 counts

all @ same analyser setting

22/5/79 Same spec 520<sup>-</sup> 20

5

7392 7 + 1.25 175/561 vacuum 78K

(tip turned up in vacuum, no Ne)

11K ions

7.3 + 1.45<sup>?</sup> 180/561 78 vac 20,496 ions 6

|     |      |     |    |     |      |     |      |       |     |   |
|-----|------|-----|----|-----|------|-----|------|-------|-----|---|
| 0   | 55   | 206 | 13 | 265 | 2    | 312 | 6044 | 3379  | 442 | 1 |
| 19  | 1    | 207 | 11 | 266 | 1    | 313 | 1677 |       | 445 | 1 |
| 29  | 2    | 208 | 1  | 273 | 2    | 314 | 383  | 3091  | 446 | 9 |
| 62  | 10   |     |    | 274 | 3    | 315 | 171  | 3401  | 447 | 2 |
| 63  | 205  | 214 | 2  | 278 | 1    | 316 | 121  | 345/1 | 448 | 2 |
| 64  | 1300 | 215 | 3  | 289 | 1    | 317 | 446  |       | 449 | 1 |
| 65  | 1042 |     |    | 293 | 1    | 318 | 320  | 3571  | 454 | 2 |
| 66  | 12   | 221 | 17 | 294 | 33   | 319 | 58   | 3601  | 456 | 1 |
| 67  | 4    | 222 | 76 | 295 | 85   | 320 | 28   | 3621  | 459 | 1 |
| 68  | 2    | 223 | 75 | 296 | 33   | 321 | 22   |       | 465 | 2 |
| 74  | 1    | 224 | 7  | 297 | 16   | 322 | 118  | 3701  | 466 | 1 |
| 78  | 1    | 225 | 1  | 298 | 16   | 323 | 175  | 3941  | 467 | 1 |
| 87  | 1    | 226 | 4  | 299 | 124  | 324 | 38   | 3952  | 469 | 1 |
| 88  | 3    | 227 | 1  | 300 | 842  | 325 | 10   | 4002  | 476 | 1 |
| 89  | 1    | 230 | 3  | 301 | 1839 | 326 | 12   | 4021  | 494 | 1 |
| 98  | 1    | 231 | 1  | 302 | 437  | 327 | 9    | 4042  | 500 | 2 |
| 121 | 2    | 232 | 2  | 303 | 201  | 328 | 30   | 4062  | 514 | 1 |
| 134 | 1    |     |    | 304 | 179  | 329 | 6    | 4251  | 574 | 1 |
| 139 | 2    | 245 | 1  | 305 | 100  | 330 | 3    | 4321  | 580 | 1 |
| 145 | 2    | 246 | 9  | 306 | 368  | 331 | 2    | 4341  | 598 | 2 |
| 147 | 1    | 251 | 1  | 307 | 351  | 332 | 2    | 4351  | 661 | 1 |
| 148 | 7    | 252 | 2  | 308 | 77   | 333 | 6    | 4372  | 687 | 1 |
| 153 | 1    | 255 | 1  | 309 | 60   | 334 | 2    | 4383  | 720 | 1 |
| 163 | 1    | 259 | 1  | 310 | 296  | 335 | 1    | 4392  | 723 | 1 |
| 192 | 3    | 264 | 1  | 311 | 2675 | 336 | 1    | 4411  | 781 | 1 |

~~524~~

772 | 795 | 819 | 829 | 955 | 1005 | 1006 |

20000  $\mu\text{s}$   $\approx$  2 hrs 225 Hz

$2 \text{ hrs} = 2 \times 3600 \times 10^3 = 10^{-1} \times 225 \text{ Hz} = 120 \text{ sec}$

Noise level  $\approx$  1 per, so expect  $\approx$  20 garbage bits.

ch0 = 55, so  $\approx$  2/sec noise on average.

α

Tues 22

ph <sup>mpk</sup> x 3

8.7 kV

60 / Me

7

7-21 + 2-2

200/580

nm

22,072 was all at same volts !!! in ~ 1 1/2 hrs.

0 54

|     |      |    |     |     |     |      |     |     |     |   |      |   |
|-----|------|----|-----|-----|-----|------|-----|-----|-----|---|------|---|
| 5   | 1    | ?? | 195 | 4   | 275 | 1    | 305 | 22  | 383 | 1 | 618  | 1 |
| 18  |      |    | 196 | 18  | 278 | 1    | 306 | 63  | 384 | 1 | 620  | 1 |
| 59  | 20   |    | 197 | 24  | 279 | 9    | 307 | 141 | 386 | 1 | 630  | 1 |
| 60  | 209  |    | 203 | 1   | 280 | 50   | 308 | 51  | 387 | 1 | 639  | 2 |
| 61  | 1723 |    | 205 | 2   | 281 | 102  | 309 | 20  | 388 | 1 | 642  | 1 |
| 62  | 1754 |    | 210 | 9   | 282 | 29   | 310 | 13  | 394 | 1 | 644  | 1 |
| 63  | 47   |    | 211 | 63  | 283 | 15   | 311 | 15  | 395 | 1 | 650  | 1 |
| 64  | 6    |    | 212 | 114 | 284 | 68   | 312 | 27  | 417 | 1 | 664  | 1 |
| 66  | 1    |    | 213 | 23  | 285 | 650  | 313 | 8   | 458 | 2 | 670  | 2 |
| 67  | 1    |    | 214 | 7   | 286 | 1794 | 314 | 5   | 424 | 1 | 681  | 1 |
| 72  | 1    |    | 215 | 1   | 287 | 943  | 315 | 1   | 425 | 2 | 715  | 1 |
| 74  | 1    |    | 216 | 3   | 288 | 322  | 316 | 1   | 426 | 1 | 734  | 1 |
| 83  | 1    |    | 219 | 6   | 289 | 255  | 317 | 9   | 427 | 1 | 785  | 2 |
| 84  | 2    |    | 220 | 2   | 290 | 148  | 318 | 2   | 431 | 1 | 795  | 1 |
| 85  | 2    |    | 226 | 1   | 291 | 372  | 319 | 7   | 436 | 1 | 804  | 1 |
| 90  | 1    |    | 232 | 2   | 292 | 332  | 320 | 2   | 438 | 2 | 820  | 1 |
| 118 | 1    |    | 238 | 1   | 293 | 111  | 322 | 1   | 439 | 1 | 875  | 1 |
| 120 | 1    |    | 239 | 3   | 294 | 143  | 327 | 1   | 443 | 1 | 903  | 3 |
| 133 | 1    |    | 240 | 1   | 295 | 881  | 336 | 1   | 445 | 1 | 919  | 2 |
| 140 | 5    |    | 244 | 2   | 296 | 2482 | 344 | 1   | 459 | 1 | 920  | 1 |
| 141 | 15   |    | 251 | 1   | 297 | 5080 | 353 | 1   | 466 | 1 | 960  | 1 |
| 142 | 4    |    | 252 | 3   | 298 | 1092 | 354 | 1   | 470 | 1 | 985  | 1 |
| 143 | 1    |    | 253 | 1   | 299 | 569  | 355 | 1   | 476 | 1 | 1007 | 2 |
| 164 | 1    |    | 254 | 1   | 300 | 212  | 356 | 1   | 477 | 1 | 1011 | 1 |
| 181 | 4    |    | 261 | 2   | 301 | 227  | 362 | 1   | 487 | 1 |      |   |
| 182 | 2    |    | 262 | 1   | 302 | 402  | 366 | 1   | 559 | 1 |      |   |
| 184 | 2    |    | 264 | 2   | 303 | 120  | 372 | 1   | 594 | 1 |      |   |
|     |      |    | 265 | 1   | 304 | 40   | 381 | 1   | 606 | 1 |      |   |

Turn down amp threshold to reduce noise ~1/20 sec.

1.49 7.00 +2.00 200 / 580 again 60 pax  
 3.55 -2.43 20000 odd

|     |      |     |     |     |      |        |     |      |   |
|-----|------|-----|-----|-----|------|--------|-----|------|---|
| 0   | 22   | 197 | 12  | 283 | 21   | 312/23 | 401 | 1    |   |
| 58  | 2    | 198 | 1   | 284 | 69   | 313    | 6   | 422  | 1 |
| 59  | 1    | 199 | 1   | 285 | 60   | 314    | 6   | 465  | 1 |
| 60  | 239  | 204 | 4   | 286 | 1916 | 315    | 6   | 467  | 1 |
| 61  | 1311 | 205 | 2   | 287 | 818  | 316    | 1   | 486  | 1 |
| 62  | 1627 | 210 | 13  | 288 | 293  | 317    | 3   | 501  | 1 |
| 63  | 28   | 211 | 43  | 289 | 225  | 319    | 1   | 512  | 2 |
| 64  | 2    | 212 | 100 | 290 | 144  | 320    | 2   | 584  | 1 |
| 65  | 2    | 213 | 22  | 291 | 375  | 323    | 1   | 617  | 1 |
| 72  | 1    | 214 | 5   | 292 | 268  | 328    | 1   | 660  | 1 |
| 73  | 2    | 215 | 4   | 293 | 103  | 335    | 2   | 673  | 1 |
| 81  | 2    | 216 | 1   | 294 | 83   | 336    | 1   | 685  | 1 |
| 84  | 2    | 218 | 1   | 295 | 793  | 370    | 2   | 768  | 1 |
| 85  | 3    | 219 | 3   | 296 | 3936 | 378    | 2   | 889  | 1 |
| 103 | 2    | 220 | 1   | 297 | 4387 | 380    | 1   | 907  | 1 |
| 106 | 2    | 221 | 2   | 298 | 1254 | 389    | 1   | 926  | 1 |
| 119 | 2    | 222 | 4   | 299 | 496  | 390    | 1   | 1002 | 1 |
| 120 | 1    | 224 | 2   | 300 | 160  | 394    | 1   |      |   |
| 123 | 1    | 251 | 1   | 301 | 250  | 402    | 1   |      |   |
| 140 | 4    | 260 | 2   | 302 | 330  | 404    | 1   |      |   |
| 141 | 14   | 262 | 1   | 303 | 147  | 410    | 1   |      |   |
| 142 | 5    | 263 | 1   | 304 | 51   | 417    | 2   |      |   |
| 147 | 2    | 275 | 2   | 305 | 30   | 418    | 1   |      |   |
| 168 | 1    | 276 | 2   | 306 | 86   | 423    | 2   |      |   |
| 175 | 1    | 277 | 1   | 307 | 140  | 424    | 2   |      |   |
| 183 | 4    | 279 | 9   | 308 | 53   | 425    | 4   |      |   |
| 184 | 2    | 280 | 52  | 309 | 23   | 426    | 1   |      |   |
| 193 | 1    | 281 | 105 | 310 | 9    | 428    | 1   |      |   |
| 196 | 6    | 282 | 22  | 311 | 17   | 430    | 1   |      |   |

8

$510^{-7} \text{Ne}/60$

7.55 + 2.47

200/580

-7.65 + 2.47

20000  $\mu\text{m}$

1hr 20mins (!)

9

|     |     |          |          |       |       |
|-----|-----|----------|----------|-------|-------|
| 0   | 1   | 235 1    | 296 4349 | 334 1 | 521 2 |
| 54  | 3   | 238 2    | 297 5761 | 335 1 | 525 1 |
| 60  | 72  | 239 4    | 298 771  | 336 2 |       |
| 61  | 336 | 243 2    | 299 211  | 337 2 |       |
| 62  | 345 | 244 2    | 300 109  |       |       |
| 63  | 5   | 251 4    | 301 282  | 344 1 |       |
| 64  | 1   | 252 11   | 302 533  | 364 1 |       |
| 65  | 1   | 253 1    | 303 98   | 366 1 |       |
| 66  | 1   | 255 3    | 304 44   | 378 1 |       |
| 65  | 1   | 261 2    | 305 19   | 380 1 |       |
| 65  | 2   | 273 1    | 306 98   | 386 1 |       |
| 69  | 2   | 275 9    | 307 181  | 387 1 |       |
| 70  | 2   | 276 5    | 308 25   | 388 1 |       |
| 74  | 12  | 279 27   | 309 17   | 390 1 |       |
| 77  | 1   | 280 76   | 310 7    |       |       |
| 82  | 1   | 281 122  | 311 19   | 405 1 |       |
| 83  | 3   | 282 16   | 312 25   | 406 1 |       |
| 95  | 3   | 283 12   | 313 9    | 407 1 |       |
| 196 | 13  | 284 40   | 314 2    | 409 1 |       |
| 197 | 20  | 285 679  | 315 4    | 418 1 |       |
| 198 | —   | 286 2718 | 316 3    | 419 1 |       |
| 205 | 5   | 287 670  | 317 9    | 423 1 |       |
| 210 | 11  | 288 198  | 318 5    | 425 3 |       |
| 211 | 30  | 289 256  | 319 2    | 426 2 |       |
| 212 | 87  | 290 127  | 320 1    | 430 1 |       |
| 213 | 7   | 291 474  | 321 3    | 432 1 |       |
| 215 | 1   | 292 296  | 322 2    | 435 2 |       |
| 216 | 3   | 293 72   | 323 1    | 442 2 |       |
| 218 | 5   | 294 76   | 324 3    | 443 1 |       |
| 219 | 3   | 295 920  |          | 451 1 |       |

Same trip, small print

60 /  $2 \times 10^7$  Ne

12.24 9.09 + 1.20 220 / 580 10375  $\infty$   
 14.20

|     |            |     |                   |     |      |     |   |
|-----|------------|-----|-------------------|-----|------|-----|---|
| 0   | 1          | 209 | 1                 | 276 | 130  | 308 | 1 |
| 57  | 3          | 210 | 2                 | 277 | 87   | 315 | 1 |
| 58  | 156        | 211 | 1                 | 278 | 156  | 320 | 1 |
| 59  | 714        | 212 | 1                 | 279 | 202  |     |   |
| 60  | 151        | 213 | 2                 | 280 | 56   | 361 | 1 |
| 61  | 2          | 216 | 2                 | 281 | 57   | 367 | 1 |
| 63  | 1          | 227 | 2                 | 282 | 497  | 375 | 1 |
| 65  | 2          | 229 | 1                 | 283 | 2039 | 392 | 1 |
| 80  | 1          |     |                   | 284 | 2470 | 396 | 1 |
|     |            | 238 | 1                 | 285 | 642  | 397 | 1 |
| 134 | 1          | 240 | $10^{20.4}$<br>Ne | 286 | 258  | 398 | 1 |
| 135 | 11         | 241 | 6                 | 287 | 144  | 399 | 1 |
| 136 | 1          | 242 | 13                | 288 | 166  |     |   |
|     |            | 247 | 10                | 289 | 194  | 406 | 1 |
| 174 | $5^{10.7}$ | 244 | 9                 | 290 | 62   | 407 | 2 |
| 175 | 2          | 249 | 5                 | 291 | 29   | 411 | 1 |
|     |            | 252 | 2                 | 292 | 23   | 414 | 1 |
| 187 | 1          | 255 | 1                 | 293 | 78   | 416 | 1 |
| 188 | $11^{C^+}$ |     |                   | 294 | 49   | 423 | 1 |
| 189 | 6          | 263 | 1                 | 295 | 20   | 424 | 1 |
|     |            | 264 | 4                 | 296 | 4    | 511 | 1 |
| 195 | 2          | 267 | 15                | 297 | 7    | 708 | 1 |
|     |            | 268 | 43                | 298 | 11   | 709 | 2 |
| 201 | 14         | 269 | 28                | 299 | 5    | 847 | 1 |
| 202 | 60         | 270 | 7                 | 300 | 2    |     |   |
| 203 | $54^{Si}$  | 271 | 6                 | 301 | 1    |     |   |
| 204 | 6          | 272 | 130               | 302 | 2    |     |   |
| 205 | 2          | 273 | 598               | 303 | 4    |     |   |
| 206 | 5          | 274 | 650               | 304 | 1    |     |   |
| 207 | 2          | 275 | 191               |     |      |     |   |



9.3 + 1.2

2 20/580

1100  $\mu$ m

9.14 + 1.2

$510^{-7}/60/16,500$

$510^{-7} Ne 160$

|       |         |         |          |          |       |
|-------|---------|---------|----------|----------|-------|
| 0 0   | 271 2   | 0 0     | 212 2    | 275 281  | 309 1 |
|       | 272 11  |         | 217 7    | 276 256  | 314 1 |
| 58 13 | 273 82  | 58 148  | 229 2    | 277 96   | 322 1 |
| 59 64 | 274 72  | 59 916  | 232 2    | 278 338  | 324 1 |
| 60 13 | 275 19  | 60 188  | 239 2    | 279 256  | 365 1 |
|       | 276 21  | 61 4    | 240 12   | 280 74   | 369 1 |
| 81 1  | 277 5   | 62 2    | 241 22   | 281 94   | 372 1 |
|       | 278 25  | 65 2    | 242 25   | 282 659  | 373 1 |
| 175 2 | 279 15  | 81 2    | 247 7    | 283 4441 | 374 1 |
|       | 280 5   | 104 5   | 244 10   | 284 3301 | 384 1 |
| 187 2 | 281 7   | 105 10  | 245 2    | 285 952  | 387 1 |
|       | 282 34  | 106 0   | 246 0    | 286 476  | 388 1 |
| 201 5 | 283 277 | 107 2   | 247 2    | 287 179  | 390 1 |
| 202 3 | 284 260 | 170 1   | 248 2    | 288 298  | 392 3 |
| 203 3 | 285 56  | 174 0   | 249 2    | 289 229  | 393 2 |
| 204 2 | 286 25  | 175 5   | 252 3    | 290 80   | 396 1 |
|       | 287 11  | 187 6   | 253 4    | 291 40   | 398 1 |
| 208 1 | 288 11  | 188 17  | 254 2    | 292 79   | 400 1 |
| 210 1 | 289 15  | 189 7   | 257 3    | 293 141  | 401 1 |
|       | 290 2   | 195 2   | 259 1    | 294 72   | 405 2 |
| 240 2 | 291 4   | 197 2   | 260 5    | 295 29   | 406 1 |
| 241 2 | 292 5   | 201 25  | 265 3    | 296 10   | 409 1 |
| 242 2 | 293 12  | 202 107 | 266 0    | 297 11   | 412 1 |
| 244 2 | 294 8   | 203 85  | 267 21   | 298 19   | 418 1 |
| 248 1 | 295 2   | 204 15  | 268 70   | 299 6    | 422 1 |
| 250 1 | 298 2   | 205 2   | 269 53   | 300 1    | 423 1 |
| 257 2 | 302 1   | 206 5   | 270 17   | 302 2    | 424 1 |
| 260 2 |         | 207 1   | 271 20   | 303 6    | 431 1 |
| 268 8 |         | 208 1   | 272 177  | 305 2    | 435 1 |
| 269 3 |         | 209 10  | 273 1133 | 306 2    | 828 1 |
|       |         | 210 6   | 274 889  | 308 3    |       |

Notes, step @ 500

increased

| 550 | 9.9 + 1.2 | var 160  | 270/580 | ↓ | 240/580 | 9.90 + 1.2 | var 160 |
|-----|-----------|----------|---------|---|---------|------------|---------|
| 0   | 2         | 265 11   | 315 1   |   | 0 0     | 263 95     |         |
| 56  | 5         | 266 124  | 327 1   |   | 54 1    | 264 63     | 5502100 |
| 57  | 21        | 267 441  | 334 1   |   | 55 10   | 265 46     |         |
| 58  | 107       | 268 166  | 336 1   |   | 56 94   | 266 124    |         |
| 59  | 5         | 269 78   | 356 1   |   | 57 188  | 267 101    | clean   |
| 101 | 0         | 270 25   | 360 1   |   | 58 14   | 268 26     |         |
| 102 | 8         | 271 55   | 361 1   |   | 129 7   | 269 20     |         |
| 107 | 1         | 272 115  | 362 1   |   | 130 4   | 270 360    |         |
| 170 | 2         | 273 46   | 383 1   |   | 167 4   | 271 1798   |         |
| 171 | 2         | 274 22   | 364 1   |   | 168 2   | 272 967    |         |
| 180 | 0         | 275 106  | 383 1   |   | 179 0   | 273 172    |         |
| 184 | 0         | 276 672  | 402 1   |   | 180 6   | 274 62     |         |
| 189 | 1         | 277 1440 | 410 1   |   | 181 1   | 275 57     |         |
| 191 | 0         | 278 419  | 427 1   |   | 186 2   | 276 120    |         |
| 196 | 0         | 279 159  | 447 1   |   | 193 20  | 277 38     |         |
| 197 | 21        | 280 62   | 457 1   |   | 194 50  | 278 16     |         |
| 198 | 40        | 281 69   | 487 1   |   | 195 9   | 279 6      |         |
| 199 | 6         | 282 81   | 514 1   |   | 197 1   | 280 26     |         |
| 201 | 0         | 283 25   | 600 1   |   | 198 1   | 281 42     |         |
| 202 | 1         | 284 16   | 616 1   |   | 200 1   | 282 2      |         |
| 204 | 2         | 285 10   | 660 1   |   | 200 2   | 283 2      |         |
| 205 | 2         | 286 44   | 661 1   |   | 201 1   | 284 0      |         |
| 206 | 0         | 287 20   | 828 1   |   | 252 2   | 285 12     |         |
| 223 | 2         | 288 8    | 868 1   |   | 253 2   | 286 6      |         |
| 224 | 1         | 289 7    | 870 1   |   | 256 4   | 289 1      |         |
| 227 | 1         | 290 4    | 901 1   |   | 257 20  | 292 2      |         |
| 233 | 1         | 291 5    |         |   | 258 6   | 308 1      |         |
| 260 | 1         | 295 2    |         |   | 259 2   | 350 1      |         |
| 261 | 5         | 296 2    |         |   | 260 61  | 387 1      |         |
| 262 | 22        | 298 2    |         |   | 261 304 | 396 1      |         |
| 263 | 6         | 300 1    |         |   | 262 511 | 401 1      |         |
| 264 | 2         | 306 1    |         |   |         |            |         |

rest day

415177

240 / 5000

9.80 + 1.2 hinned up in case  
10.09 + 1.0 20,000 all

510<sup>00</sup> cold

5

|     |     |          |          |       |
|-----|-----|----------|----------|-------|
| 0   | 29  | 148 6    | 266 448  | 345 1 |
| 55  | 58  | 199 5    | 267 351  | 246 1 |
| 56  | 287 | 200 1    | 268 118  | 350 1 |
| 57  | 705 | 202 1    | 269 211  | 256 1 |
| 58  | 02  | 203 0    | 270 1914 | 260 2 |
| 60  | 2   | 204 2    | 271 6801 | 376 1 |
| 64  | 1   | 205 3    | 272 2960 | 378 1 |
| 68  | 1   | 220 2    | 273 818  | 279 1 |
| 77  | 1   | 222 1    | 274 427  | 280 2 |
| 93  | 2   | 223 2    | 275 201  | 287 2 |
| 127 | 2   | 224 1    | 276 249  | 406 1 |
| 128 | 7   | 230 4    | 277 145  | 422 2 |
| 129 | 21  | 231 6    | 278 60   | 465 1 |
| 130 | 9   | 232 1    | 279 71   | 486 2 |
| 152 | 1   | 239 2    | 280 133  | 702 1 |
| 166 | 0   | 241 2    | 281 119  | 721 2 |
| 167 | 6   | 251 2    | 282 37   | 742 1 |
| 168 | 5   | 252 7    | 283 18   | 745 2 |
| 178 | 2   | 253 1    | 284 14   | 758 1 |
| 179 | 9   | 254 1    | 285 26   | 901 1 |
| 180 | 21  | 255 16   | 286 8    | 910 1 |
| 181 | 4   | 256 68   | 287 4    | 928 1 |
| 182 | 1   | 257 97   | 288 5    | 930 2 |
| 189 | 1   | 258 25   | 289 5    | 943 1 |
| 191 | 2   | 259 08   | 290 5    | 956 1 |
| 192 | 23  | 260 264  | 291 2    | 993 1 |
| 193 | 95  | 261 1789 | 294 1    |       |
| 194 | 165 | 262 1711 | 298 1    |       |
| 195 | 21  | 263 401  | 304 1    |       |
| 196 | 7   | 264 273  | 307 1    |       |
| 197 | 10  | 265 224  | 308 2    |       |

N

M

| 3.46<br>4.23 |     | 10-2 + 1-3 var 78 rapido 250/500 20000 all @ 1v. |      |     |     |     |     |     |      |      |      |     |     |   |
|--------------|-----|--------------------------------------------------|------|-----|-----|-----|-----|-----|------|------|------|-----|-----|---|
| 0            | 4   | 1982                                             | 271  | 272 | 381 | 1   | 194 | 4   | 266  | 5610 | 274  | 2   |     |   |
| 44           | 1   | 199                                              | 2    | 272 | 52  | 391 | 1   | 196 | 10   | 267  | 1171 | 288 | 1   |   |
| 50           | 2   | 200                                              | 4    | 272 | 19  | 477 | 1   | 197 | 2    | 268  | 268  | 292 | 1   |   |
| 54           | 24  | 214                                              | 2    | 274 | 60  | 588 | 1   | 199 | 2    | 269  | 178  | 293 | 1   |   |
| 55           | 208 | 215                                              | 2    | 275 | 187 | 882 | 2   | 200 | 1    | 270  | 406  | 295 | 2   |   |
| 56           | 540 | 225                                              | 2    | 276 | 56  | 0   | -   | 4   | 214  | 5    | 271  | 265 | 296 | 1 |
| 57           | 17  | 226                                              | 4    | 277 | 14  | 50  | 1   | 215 | 2    | 272  | 57   | 297 | 1   |   |
| 76           | 1   | 234                                              | 3    | 278 | 6   | 54  | 52  | 218 | 2    | 273  | 20   | 298 | 1   |   |
| 125          | 2   | 235                                              | 1    | 279 | 14  | 55  | 440 | 224 | 1    | 274  | 68   |     |     |   |
| 126          | 4   | 248                                              | 1    | 280 | 25  | 56  | 629 | 226 | 2    | 275  | 101  |     |     |   |
| 127          | 26  | 250                                              | 10   | 281 | 2   | 57  | 28  | 227 | 2    | 276  | 52   |     |     |   |
| 128          | 1   | 251                                              | 71   | 282 | 1   | 76  | 2   | 228 | 2    | 277  | 11   |     |     |   |
| 132          | 2   | 252                                              | 74   | 283 | 2   | 77  | 5   | 229 | 2    | 278  | 6    |     |     |   |
| 156          | 1   | 253                                              | 27   | 284 | 5   | 76  | 14  | 247 | 1    | 279  | 14   |     |     |   |
| 160          | 1   | 254                                              | 19   | 285 | 1   | 127 | 13  | 248 | 2    | 280  | 11   |     |     |   |
| 164          | 4   | 255                                              | 217  | 286 | 1   | 128 | 7   | 250 | 17   | 281  | 4    |     |     |   |
| 175          | 1   | 256                                              | 1724 | 297 | 1   | 136 | 1   | 251 | 121  | 282  | 2    |     |     |   |
| 176          | 16  | 257                                              | 1614 | 300 | 1   | 160 | 4   | 252 | 107  | 283  | 4    |     |     |   |
| 177          | 11  | 258                                              | 252  | 302 | 1   | 164 | 4   | 253 | 26   | 284  | 2    |     |     |   |
| 178          | 1   | 259                                              | 228  | 303 | 1   | 165 | 2   | 254 | 21   | 286  | 1    |     |     |   |
| 180          | 2   | 260                                              | 152  | 307 | 1   | 167 | 2   | 255 | 280  | 285  | 1    |     |     |   |
| 188          | 4   | 261                                              | 554  | 309 | 1   | 175 | 1   | 256 | 2380 | 286  | 1    |     |     |   |
| 189          | 57  | 262                                              | 201  | 309 | 1   | 176 | 15  | 257 | 1547 | 287  | 2    |     |     |   |
| 190          | 180 | 262                                              | 64   | 314 | 1   | 177 | 10  | 258 | 240  | 288  | 1    |     |     |   |
| 191          | 28  | 264                                              | 271  | 315 | 1   | 178 | 2   | 259 | 244  | 289  | 1    |     |     |   |
| 192          | 2   | 265                                              | 2765 | 317 | 1   | 186 | 2   | 260 | 202  | 289  | 1    |     |     |   |
| 193          | 8   | 266                                              | 7369 | 318 | 1   | 189 | 71  | 261 | 564  | 290  | 1    |     |     |   |
| 194          | 2   | 267                                              | 1540 | 322 | 1   | 190 | 187 | 262 | 220  | 291  | 1    |     |     |   |
| 195          | 2   | 268                                              | 220  | 323 | 1   | 191 | 41  | 263 | 107  | 292  | 1    |     |     |   |
| 196          | 4   | 269                                              | 124  | 324 | 2   | 192 | 5   | 264 | 281  | 293  | 1    |     |     |   |
| 197          | 2   | 270                                              | 262  | 328 | 1   | 193 | 6   | 265 | 3378 | 294  | 1    |     |     |   |

4-33-457 21 mins/20K @ 250/500  
 9.2 + 2.2 molto rapido! var 78

| 4.53 - 21 mins per 20k ions. | 9.00 + 2.0 | vue 78  | 22000                                                            |
|------------------------------|------------|---------|------------------------------------------------------------------|
| 5.08 - 6.29 1hr 30 per 22k   | 250/580    |         | √ Discovered noisy furnace in Mand Room → interference on reads. |
| 0 2                          | 195 4      | 268 132 | 379 2                                                            |
| 52 2                         | 196 1      | 269 87  | 380 4                                                            |
| 53 4                         | 197 4      | 270 367 | 386 1                                                            |
| 54 135                       | 199 1      | 271 353 | 387 1                                                            |
| 55 1828                      | 215 2      | 272 37  | 388 1                                                            |
| 56 2467                      | 218 1      | 273 19  | 392 1                                                            |
| 57 112                       | 226 7      | 274 55  | 395 2                                                            |
| 58 1                         | 227 1      | 275 160 | 586 1                                                            |
| 59 2                         | 233 1      | 276 44  | 900 1                                                            |
| 61 1                         | 234 4      | 277 8   |                                                                  |
| 65 1                         | 237 1      | 278 5   |                                                                  |
| 75 1                         | 246 3      | 279 17  |                                                                  |
| 76 6                         | 247 5      | 280 20  |                                                                  |
| 99 1                         | 250 9      | 281 1   |                                                                  |
| 125 2                        | 251 83     | 282 1   |                                                                  |
| 126 19                       | 252 75     | 283 5   |                                                                  |
| 127 18                       | 253 21     | 284 5   |                                                                  |
| 184 8                        | 254 7      | 285 5   |                                                                  |
| 175 2                        | 255 190    | 286 3   |                                                                  |
| 176 22                       | 256 1756   | 289 1   |                                                                  |
| 177 12                       | 257 1481   | 308 1   |                                                                  |
| 178 1                        | 258 165    | 317 1   |                                                                  |
| 182 2                        | 259 203    | 344 1   |                                                                  |
| 183 3                        | 260 120    | 350 1   |                                                                  |
| 184 7                        | 261 510    | 360 1   |                                                                  |
| 189 48                       | 262 242    | 361 1   |                                                                  |
| 190 149                      | 263 58     | 364 1   |                                                                  |
| 191 27                       | 264 220    | 367 1   |                                                                  |
| 192 1                        | 265 2608   | 369 1   |                                                                  |
| 193 6                        | 266 6563   | 373 1   |                                                                  |
| 194 2                        | 267 1122   | 374 2   |                                                                  |

hi Cr?

Next day Fri 25/5/79 knowledge in view 4 10<sup>10</sup> cold for 4 pers see.

| 1257 |     | 9.01 + 2.3 |     | Vdc 78 |     | 250/580 |      |             |      |      |                      |
|------|-----|------------|-----|--------|-----|---------|------|-------------|------|------|----------------------|
| 1st  | 2nd | 3rd        | 4th | 5th    | 6th | 7th     | 8th  | 9th         | 10th | 11th | 12th                 |
| 0    | 0   | 1          |     | 3      | 225 |         |      |             |      |      |                      |
| 0    | 0   | 1          |     | 3      | 226 | 1       |      |             | 275  | 41   | 44 39 44             |
| 52   | 1   |            |     |        | 233 | 2       |      |             | 276  | 11   | 19 14 11             |
| 53   | 9   |            |     |        |     |         |      |             | 277  | 1    | 2 4 2                |
| 54   | 94  | 56         | 28  | 39     | 241 | 2       |      |             | 8    | 4    | 3 3                  |
| 55   | 400 | 565        | 576 | 644    | 249 | 1       |      | 246 1       | 279  | 7    | 5 3 8                |
| 56   | 578 | 937        | 971 | 1010   | 250 | 9       | 2    | 1           | 280  | 6    | 4 1 6                |
| 57   | 20  | 50         | 53  | 42     | 251 | 27      | 17   | 21 13       | 2    | 1    | 1 2 <sup>281</sup> 1 |
| 59   | 1   |            |     |        | 252 | 14      | 34   | 17 21       | 2    |      |                      |
|      |     |            |     |        | 253 | 2       | 7    | 3 3         | 283  | 5    | 2 2 1                |
| 76   | 3   |            | 1   | 2      | 254 | 12      | 7    | 2 1         | 284  | 2    | 1 2 2                |
| 92   |     | 1          |     |        | 255 | 126     | 74   | 38 31       | 2    | 5    |                      |
| 126  | 4   | 6          | 3   | 1      | 256 | 420     | 414  | 323 332     | 286  | 1    | 1                    |
| 127  | 6   | 6          | 3   | 10     | 257 | 304     | 407  | 392 343     |      |      |                      |
| 1    |     |            |     |        | 258 | 47      | 54   | 56 54       |      |      |                      |
| 64   | 4   |            |     | 2      | 259 | 52      | 68   | 41 38       |      |      |                      |
| 175  |     | 1          |     |        | 260 | 42      | 27   | 27 23       | 316  |      | 1 2                  |
| 176  | 4   | 6          | 4   | 4      | 261 | 113     | 112  | 104 121     | 317  |      | 2 1                  |
| 177  | 3   | 5          | 2   | 4      | 262 | 55      | 73   | 70 57       | 318  | 1    | 1                    |
| 178  | 1   |            |     |        | 263 | 31      | 14   | 16 11       | 319  |      | 1                    |
| 182  |     | 2          |     |        | 264 | 184     | 51   | 26 37       | 347  |      | 261 368 1            |
| 184  |     |            |     |        | 265 | 873     | 682  | 440 506     | 368  |      | 369 1                |
| 189  | 13  | 18         | 6   | 10     | 266 | 1407    | 1780 | 1493 1444   | 379  |      | 375 1                |
| 190  | 27  | 55         | 36  | 23     | 267 | 248     | 367  | 360 333 380 | 378  |      | 2                    |
| 191  | 17  | 8          | 9   | 4      | 268 | 38      | 67   | 40 38 381   | 385  |      | 1 2                  |
| 193  | 2   | 2          | 1   |        | 269 | 32      | 24   | 23 21 397   | 397  |      | 1 1                  |
| 196  |     | 2          |     |        | 270 | 95      | 96   | 72 71       |      |      | 408 1                |
| 197  | 1   |            | 1   | 3      | 271 | 71      | 98   | 83 82 415   |      |      |                      |
| 200  | 1   | 1          |     |        | 272 | 8       | 13   | 6 11        |      |      | 607 2                |
| 214  | 4   |            | 2   |        | 273 | 3       | 7    | 3 3         |      |      |                      |
|      |     |            |     |        | 274 | 3       | 11   | 10 7        |      |      |                      |

G

← latched into false, near beginning.  
 ph x) < 0.1V

x) DW \* ~ 10.5KV

x) DW after emptying in Me - gully, 78 K.

F

410<sup>-5</sup> 5000 Take out specimen & outgas @ 250°C - replace  
 Ne 110<sup>-7</sup> background, 78, 8.8 + 2.0 250/580 78 10,500

|     |     |          |         | Gas out 110 <sup>-9</sup> 9.25 + 2.0 250/580 |          |       |  |
|-----|-----|----------|---------|----------------------------------------------|----------|-------|--|
| 0   | 1   | 257 213  | 345     |                                              |          |       |  |
| 52  | 41  | 258 461  | 373 1   | 184 1                                        | 262 56   | 378 1 |  |
| 55  | 223 | 259 40   | 375 1   | 188 2                                        | 264 155  | 380 2 |  |
| 56  | 613 | 260 48   | 379 1   | 189 20                                       | 265 1807 | 381 2 |  |
| 57  | 60  | 261 45   | 381 1   | 190 60                                       | 266 2712 | 387 1 |  |
| 62  | 2   | 262 103  | 382 2   | 191 18                                       | 267 629  | 394 1 |  |
| 67  | 1   | 263 101  | 389 1   | 192 4                                        | 268 276  |       |  |
| 126 | 4   | 264 12   | 397 1   | 193 5                                        | 269 129  |       |  |
| 127 | 1   | 265 62   | 404 2   | 196 4                                        | 270 186  |       |  |
| 176 | 2   | 266 529  |         | 200 2                                        | 271 158  |       |  |
| 177 | 5   | 267 1524 | 0 0     | 210 2                                        | 272 25   |       |  |
| 178 | 3   | 268 674  | 53 1    | 215 2                                        | 273 17   |       |  |
| 189 | 2   | 269 40   | 54 49   | 226 1                                        | 274 45   |       |  |
| 190 | 12  | 270 42   | 55 759  | 246 1                                        | 275 90   |       |  |
| 199 | 22  | 271 68   | 56 1109 | 247 5                                        | 276 19   |       |  |
| 192 | 1   | 272 95   | 57 28   | 256 3                                        | 277 10   |       |  |
| 194 | 2   | 273 14   | 76 2    | 251 27                                       | 278 3    |       |  |
| 203 | 1   | 274 4    | 78 1    | 252 29                                       | 279 12   |       |  |
| 226 | 2   | 275 11   | 126 7   | 253 20                                       | 280 9    |       |  |
| 227 | 2   | 276 31   | 127 6   | 254 16                                       | 283 1    |       |  |
| 228 | 1   | 277 25   | 128 2   | 255 162                                      | 284 5    |       |  |
| 228 | 1   | 279 2    | 132 1   | 256 953                                      | 285 3    |       |  |
| 251 | 1   | 280 4    | 162 2   | 257 596                                      | 286 2    |       |  |
| 252 | 16  | 281 3    | 164 3   | 258 181                                      | 309 1    |       |  |
| 253 | 26  | 283 3    | 176 4   | 259 106                                      | 263 1    |       |  |
| 254 | 3   | 318 2    | 777 1   | 260 79                                       | 264 1    |       |  |
| 255 | 9   | 319 2    | 178 3   | 261 254                                      | 274 1    |       |  |
| 256 | 58  |          | 183 3   | 262 86                                       | 276 1    |       |  |

Mon 29/may

flint

9.1 - 9.22 + 2.0 78/Vac  $110^{-9}$  (no ne locking) 250/580

2, 2.10, 2.28, 2.59, 3.22, 3.49, 4.16, 4.44, 5.13, 5.43, 6.15 slip @ 6.30

11 x 10000 + 5000

H gated out @  $\sim 100000$  - inadvertently let delay time into spectrum  
 $\sim 5$  sec worth 22-75 range (total)

|     |                                         |        |         |          |                          |        |        |
|-----|-----------------------------------------|--------|---------|----------|--------------------------|--------|--------|
| 0   | 8 (!)                                   | 71 2   | 176 87  | 212 4    | 258 1167                 | 282 7  | 342 2  |
| 16  | 1                                       | 72 1   | 177 64  | 214 8    | 259 920                  | 283 16 | 343 1  |
| 17  | 9                                       | 73 1   | 178 4   | 215 10   | 260 863                  | 284 25 | 344 1  |
| 18  | 29                                      | 74 1   | 179 1   | 217 1    | 261 2294                 | 285 3  | 345 4  |
| 19  | 2                                       | 75 8   | 180 12  | 224 1    | 262 820                  | 286 4  | 346 4  |
| 20  | 1                                       | 76 43  | 184 3   | 225 6    | 263 403                  | 287 2  | 347 2  |
| 21  | 1                                       | 77 12  | 187 3   | 226 11   | 264 2928                 | 289 2  | 348 3  |
| etc | 48 12<br>49 17<br>50 2<br>51 4<br>52 11 | 84 2   | 188 43  | 230 1    | 265 7050                 |        | 349 3  |
| 53  | 53                                      | 92 2   | 189 263 | 233 5    | 266 5678                 | 292 1  | 350 1  |
| 54  | 2186                                    | 97 1   | 190 686 | 234 6    | 267 4459                 | 293 2  | 352 1  |
| 55  | 2184                                    |        | 191 100 | 237 1    | 268 1190                 | 296 2  | 353 1  |
| 56  | 7494                                    | 125 14 | 192 22  | 245 3    | 269 678                  | 297 3  | 361 1  |
| 57  | 676                                     | 126 55 | 193 40  | 246 11   | 270 <sup>1833</sup> 1833 | 298    | 362 1  |
| 58  | 14                                      | 127 54 | 194 7   | 247 19   | 271 1141                 | 303 1  | 363 1  |
| 59  | 90                                      | 128 4  | 195 2   | 248 4    | 272 216                  | 305 2  | 364 2  |
| 60  | 49                                      | 131 1  | 196 10  | 249 9    | 273 143                  | 306 2  | 365 1  |
| 61  | 73                                      | 132 2  | 197 26  | 250 93   | 274 368                  | 315 6  | 366 4  |
| 62  | 53                                      | 156 1  | 198 1   | 251 413  | 275 699                  | 316 9  | 367 3  |
| 63  | 50                                      | 162 2  | 199 49  | 252 330  | 276 150                  | 317 26 | 368 4  |
| 64  | 14                                      | 163 6  | 200 4   | 253 49   | 277 49                   | 318 2  | 369 2  |
| 65  | 11                                      | 164 15 | 202 4   | 254 160  | 278 41                   | 319 1  | 370 7  |
| 66  | 5                                       | 165 2  | 208 1   | 255 2139 | 279 107                  |        | 371 2  |
| 67  | 1                                       | 174 3  | 210 3   | 256 8280 | 280 47                   | 338 3  | 372 10 |
|     |                                         | 175 14 | 211 1   | 257 5044 | 281 9                    | 339 2  | 373 21 |



374 22

375 5

376 2

377 2

378 6

379 22

380 42

381 12

382 2

383 2

384 2

385 9

386 21

387 14

388 2

390 2

392 2

393 2

395 2

396 2

~~399~~ 401 1

402 1

403 1

405 2

493 1

645 1

703 1

905 1

990 1

W, Th, & assembly Kim, exasperated, etc.

Fri

Discovered timer ch2 possibly not accessed by the box during previous runs, as set to hold. ? Effect on accuracy.

So 9.7-9.25 + 2.0 78 5<sup>-10</sup> vac (none). 250/580

20K wds in 16 hrs.

|     |      |     |    |     |      |     |    |     |   |
|-----|------|-----|----|-----|------|-----|----|-----|---|
| 0   | 3    | 183 | 0  | 254 | 110  | 282 | 5  | 280 | 7 |
| 53  | 4    | 184 | 1  | 255 | 307  | 283 | 8  | 281 | 3 |
| 54  | 373  | 186 | 3  | 256 | 1263 | 284 | 2  | 282 | 1 |
| 55  | 2303 | 187 | 0  | 257 | 557  | 285 | 2  | 283 | 1 |
| 56  | 4222 | 188 | 10 | 258 | 210  |     |    | 284 | 2 |
| 57  | 67   | 189 | 29 | 259 | 168  | 295 | 1  | 286 | 2 |
| 58  | 2    | 190 | 63 | 260 | 177  | 301 | 1  | 298 | 1 |
| 59  | 1    | 191 | 8  | 261 | 402  | 307 | 1  | 400 | 1 |
| 60  | 5    | 192 | 1  | 262 | 208  | 313 | 1  | 402 | 1 |
| 62  | 2    | 194 | 4  | 263 | 437  | 314 | 1  | 403 | 1 |
| 72  | 1    | 196 | 4  | 264 | 852  | 315 | 2  | 476 | 1 |
| 73  | 1    | 197 | 2  | 265 | 3060 | 316 | 1  | 479 | 1 |
| 75  | 2    | 199 | 2  | 266 | 3694 | 317 | 3  |     |   |
| 76  | 8    | 201 | 1  | 267 | 561  | 327 | 1  |     |   |
| 77  | 2    | 210 | 2  | 268 | 280  | 340 | 2  |     |   |
| 78  | 3    | 211 | 2  | 269 | 162  | 343 | 1  |     |   |
| 126 | 7    | 214 | 1  | 270 | 352  | 347 | 2  |     |   |
| 127 | 7    | 226 | 1  | 271 | 135  | 365 | 2  |     |   |
| 128 | 1    | 233 | 1  | 272 | 66   | 367 | 1  |     |   |
| 130 | 1    | 245 | 1  | 273 | 51   | 371 | 3  |     |   |
| 164 | 2    | 247 | 2  | 274 | 90   | 372 | 4  |     |   |
| 174 | 1    | 248 | 1  | 275 | 102  | 373 | 10 |     |   |
| 175 | 4    | 249 | 3  | 276 | 177  | 374 | 4  |     |   |
| 176 | 10   | 250 | 14 | 277 | 15   | 376 | 3  |     |   |
| 177 | 5    | 251 | 59 | 278 | 14   | 377 | 2  |     |   |
| 178 | 1    | 252 | 30 | 279 | 16   | 378 | 4  |     |   |
| 182 | 1    | 253 | 23 | 280 | 4    | 379 | 10 |     |   |

D

total 100

20K @ 1 1/2 hrs.

Gate out H speed up rate slightly

9.6 + 2.3 250/580 var 78

20K  
all @ 9.8 hrs  
+ 2.3

quicks

9.8 + 2.3 250/580 var 78

|     |     |     |      |     |     |      |      |     |     |     |      |     |     |     |    |
|-----|-----|-----|------|-----|-----|------|------|-----|-----|-----|------|-----|-----|-----|----|
| 0   | 2   | 213 | 1    | 270 | 578 | 3453 | 617  | 1   | 215 | 1   | 275  | 128 | 366 | 2   |    |
| 68  | 2   | 215 | 1    | 271 | 167 | 348  | 2812 | 1   | 215 | 1   | 275  | 128 | 366 | 2   |    |
| 76  | 7   | 218 | 1    | 272 | 92  | 349  | 2    | 0   | 4   | 226 | 2    | 276 | 37  | 368 | 1  |
| 77  | 1   | 225 | 1    | 273 | 55  | 360  | 1    | 75  | 1   | 234 | 1    | 277 | 28  | 369 | 1  |
| 125 | 3   | 226 | 1    | 274 | 171 | 362  | 1    | 76  | 6   | 246 | 3    | 278 | 19  | 370 | 1  |
| 126 | 10  | 222 | 1    | 275 | 145 | 364  | 1    | 725 | 2   | 248 | 1    | 279 | 19  | 371 | 5  |
| 127 | 7   | 233 | 1    | 276 | 43  | 365  | 1    | 126 | 8   | 249 | 2    | 280 | 15  | 372 | 8  |
| 128 | 1   | 239 | 1    | 277 | 18  | 367  | 2    | 127 | 8   | 250 | 22   | 281 | 7   | 373 | 11 |
| 163 | 1   | 245 | 1    | 278 | 15  | 369  | 1    | 128 | 1   | 251 | 97   | 282 | 2   | 374 | 3  |
| 164 | 2   | 247 | 4    | 279 | 25  | 371  | 3    | 144 | 1   | 252 | 49   | 283 | 6   | 376 | 2  |
| 165 | 1   | 248 | 2    | 280 | 15  | 372  | 3    | 163 | 3   | 253 | 21   | 284 | 7   | 377 | 3  |
| 174 | 1   | 249 | 3    | 281 | 2   | 373  | 7    | 164 | 6   | 254 | 70   | 285 | 3   | 378 | 4  |
| 175 | 5   | 250 | 24   | 282 | 2   | 374  | 6    | 174 | 1   | 255 | 620  | 288 | 1   | 379 | 5  |
| 176 | 14  | 251 | 92   | 283 | 9   | 375  | 4    | 175 | 1   | 256 | 1863 | 303 | 1   | 380 | 8  |
| 177 | 6   | 252 | 49   | 284 | 6   | 376  | 15   | 176 | 9   | 257 | 717  | 304 | 1   | 381 | 1  |
| 178 | 2   | 253 | 21   | 285 | 4   | 377  | 3    | 177 | 4   | 258 | 299  | 308 | 1   | 382 | 1  |
| 183 | 2   | 254 | 71   | 286 | 1   | 378  | 8    | 178 | 1   | 259 | 189  | 314 | 1   | 384 | 1  |
| 184 | 1   | 255 | 594  | 287 | 1   | 379  | 6    | 183 | 1   | 260 | 301  | 315 | 1   | 387 | 1  |
| 187 | 1   | 256 | 1883 | 288 | 1   | 380  | 7    | 187 | 1   | 261 | 530  | 316 | 1   | 393 | 1  |
| 188 | 4   | 257 | 628  | 289 | 1   | 381  | 1    | 188 | 6   | 262 | 323  | 317 | 1   | 394 | 1  |
| 189 | 51  | 258 | 361  | 305 | 1   | 382  | 1    | 189 | 53  | 263 | 243  | 339 | 2   | 402 | 1  |
| 190 | 101 | 259 | 192  | 306 | 1   | 385  | 4    | 190 | 112 | 264 | 1111 | 340 | 1   | 596 | 1  |
| 191 | 22  | 260 | 269  | 314 | 1   | 386  | 7    | 191 | 9   | 265 | 5389 | 342 | 1   | 894 | 1  |
| 192 | 5   | 261 | 526  | 315 | 1   | 387  | 1    | 192 | 7   | 266 | 5209 | 344 | 2   |     |    |
| 193 | 7   | 262 | 317  | 316 | 2   | 388  | 1    | 193 | 3   | 267 | 1063 | 346 | 1   |     |    |
| 194 | 6   | 263 | 245  | 317 | 4   | 396  | 1    | 194 | 8   | 268 | 313  | 348 | 1   |     |    |
| 195 | 1   | 264 | 1099 | 318 | 2   | 397  | 1    | 196 | 7   | 269 | 258  | 349 | 3   |     |    |
| 196 | 4   | 265 | 5601 | 328 | 2   | 399  | 1    | 197 | 4   | 270 | 583  | 351 | 1   |     |    |
| 198 | 2   | 266 | 5037 | 339 | 2   | 402  | 1    | 198 | 2   | 271 | 178  | 356 | 1   |     |    |
| 199 | 2   | 267 | 996  | 341 | 1   | 411  | 1    | 199 | 2   | 272 | 97   | 359 | 1   |     |    |
| 200 | 1   | 268 | 482  | 343 | 3   | 491  | 1    | 200 | 1   | 273 | 64   | 362 | 1   |     |    |
| 202 | 2   | 269 | 262  | 344 | 2   | 550  | 1    | 214 | 1   | 274 | 160  | 364 | 2   |     |    |

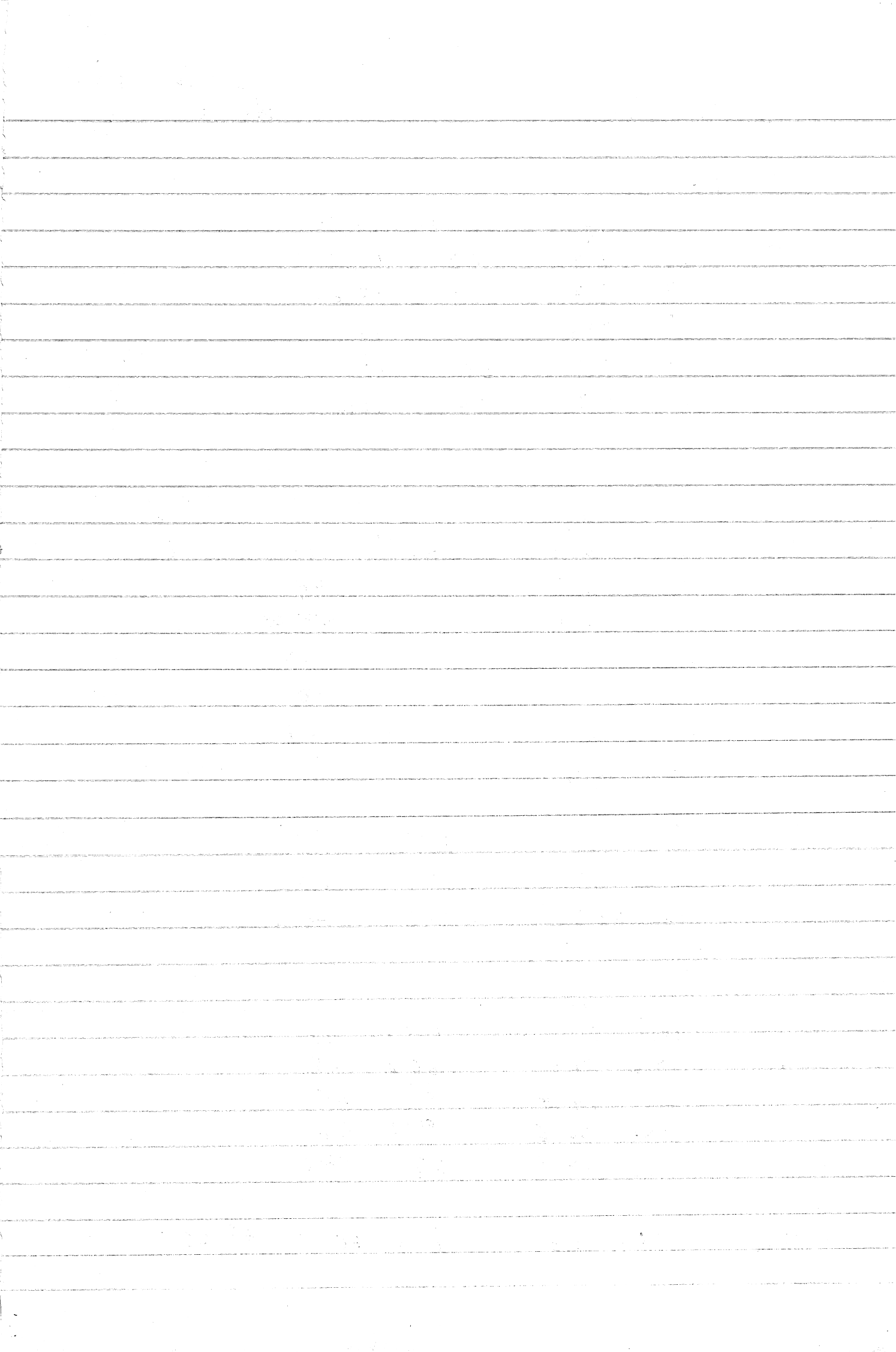
B

4.10 - 570  
10.2 + 2.7 650/580  
~ 7-10/sec

A

10.7 + 2.7 250/580  
5.20 rapido - flushed, ~ 10-20/sec

|         |          |         |       |         |         |
|---------|----------|---------|-------|---------|---------|
| 0 2     | 224 1    | 273 72  | 343 1 | 0 1     | 266 569 |
| 74 1    | 225 1    | 274 163 | 344 1 | 117 1   | 267 5   |
| 125 2   | 226 4    | 275 164 | 345 1 | 126 2   | 268 42  |
| 126 9   | 234 3    | 276 23  | 348 1 | 127 1   | 269 18  |
| 127 7   | 237 1    | 277 4   | 353 1 | 131 1   | 270 64  |
| 128 2   | 238 1    | 278 22  | 362 1 | 177 1   | 271 22  |
| 131 1   | 243 1    | 279 41  | 365 1 | 187 1   | 272 8   |
| 132 1   | 245 1    | 280 7   | 368 4 | 188 1   | 273 6   |
| 163 3   | 247 1    | 281 7   | 369 1 | 189 8   | 274 11  |
| 164 6   | 250 22   | 282 3   | 370 1 | 190 3   | 275 19  |
| 174 2   | 251 87   | 283 4   | 372 4 | 196 2   | 276 4   |
| 175 6   | 252 45   | 284 8   | 373 2 | 213 1   | 277 3   |
| 176 4   | 253 11   | 285 3   | 375 1 | 215 1   | 278 2   |
| 177 3   | 254 33   | 286 3   | 377 4 | 225 1   | 279 6   |
| 182 1   | 255 573  | 287 3   | 378 4 | 234 1   | 280 14  |
| 184 1   | 256 2105 | 288 3   | 379 3 | 247 1   | 282 1   |
| 188 9   | 257 64   | 289 2   | 380 6 | 250 2   | 283 2   |
| 189 55  | 258 216  | 296 1   | 381 1 | 251 16  | 287 1   |
| 190 103 | 259 192  | 298 1   | 382 1 | 252 2   | 289 1   |
| 191 1   | 260 257  | 302 1   | 383 1 | 253 1   | 293 1   |
| 192 1   | 261 625  | 305 1   | 384 1 | 254 1   | 306 1   |
| 193 6   | 262 306  | 306 1   | 385 1 | 255 61  | 308 1   |
| 194 4   | 263 301  | 307 1   | 386 3 | 256 218 | 353 1   |
| 195 3   | 264 1179 | 308 1   | 389 1 | 257 62  | 379 1   |
| 196 6   | 265 4957 | 309 1   | 392 1 | 258 32  | 386 1   |
| 197 2   | 266 5922 | 315 3   | 393 1 | 259 12  |         |
| 198 1   | 267 423  | 316 2   | 394 2 | 260 39  |         |
| 199 1   | 268 199  | 317 1   | 395 2 | 261 54  |         |
| 210 1   | 269 189  | 320 1   | 402 1 | 262 30  |         |
| 214 2   | 270 617  | 324 1   | 549 1 | 263 28  |         |
| 215 3   | 271 199  | 326 1   |       | 264 149 |         |
| 216 1   | 272 65   | 342 2   |       | 265 533 |         |



C 12, 1%0

Ne<sup>+</sup> 92% 8%  
20 22

O 16

| $\tau_i$ | $\tau_i^+$ | %    | $\tau_i^{++}$ | $\tau_i^{2+}$ |
|----------|------------|------|---------------|---------------|
|          | 46         | 7.9  | 23            | 15.3          |
|          | 47         | 7.7  | 23.5          | 15.6          |
|          | 48         | 73.5 | 24            | 16            |
|          | 49         | 5.5  | 24.5          | 16.3          |
|          | 50         | 5.3  | 25            | 16.6          |

| $Ru$ |     | %    | $Ru^{2+}$          | $Ru^{2+}$ |
|------|-----|------|--------------------|-----------|
|      | 96  | 5.7  | 48                 | 32        |
|      | 98  | 2.2  | 49                 |           |
|      | 99  | 12.8 | <del>50</del> 49.5 |           |
|      | 100 | 12.7 | 50                 |           |
|      | 101 | 16.9 | 50.5               |           |
|      | 102 | 21.3 | 51                 |           |
|      | 104 | 18.3 | 52                 | 34.6      |

| $Ir$ | $Ir^+$ | %    | $Ir^{2+}$ | $Ir^{2+}$ |
|------|--------|------|-----------|-----------|
|      | 191    | 38.5 | 95.5      | 63.6      |
|      | 193    | 61.5 | 96.5      | 64.3      |

| $W$ |     | %    |      |       |
|-----|-----|------|------|-------|
|     | 180 | 0.1  | (60) | (45)  |
|     | 182 | 26.4 | 60.6 | 45.5  |
|     | 183 | 14.4 | 61   | 45.75 |
|     | 184 | 30.6 | 61.3 | 46    |
|     | 186 | 28.4 | 62   | 46.5  |

Ta 191 100 90.5 60.3 45.25



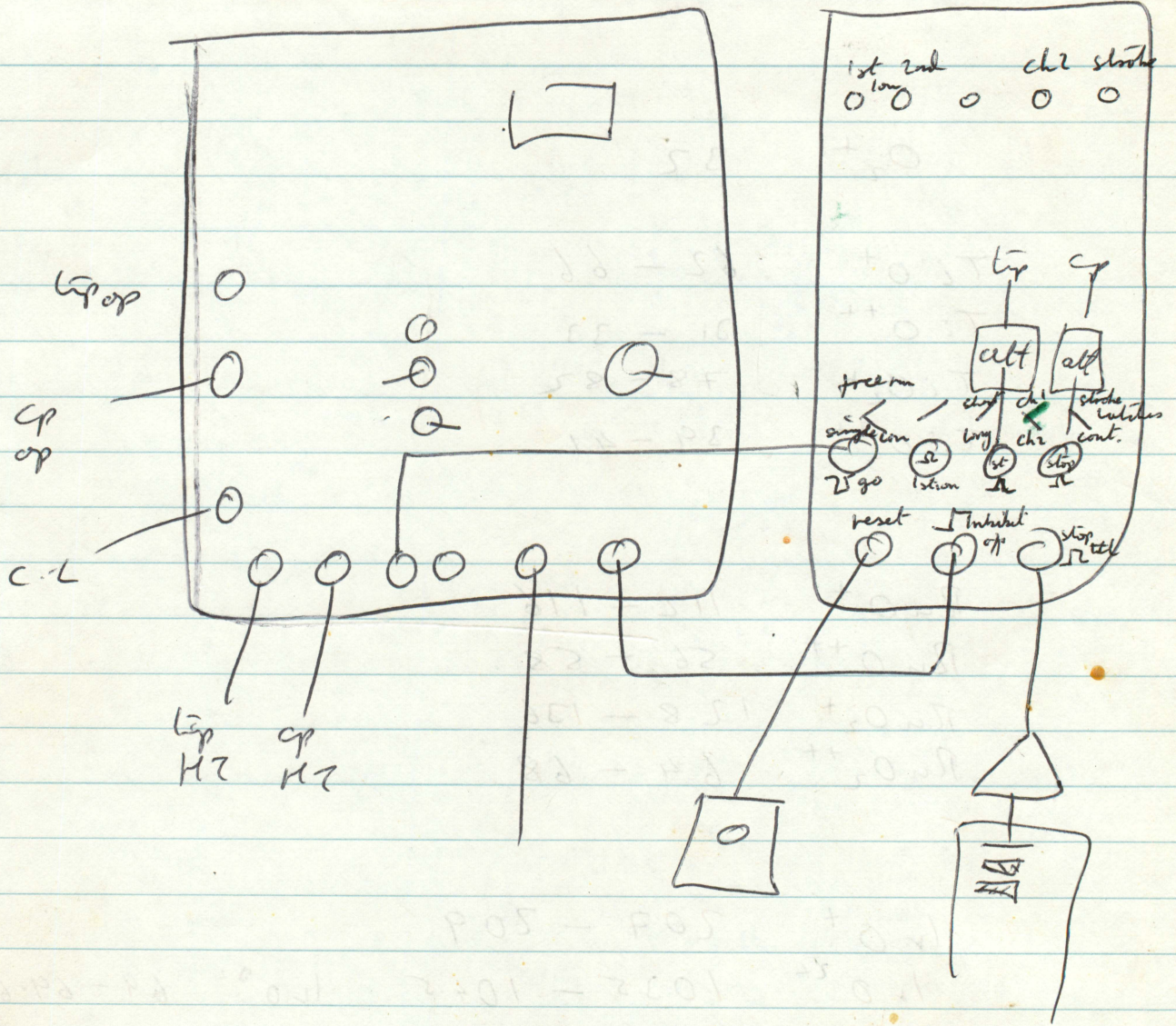
1-613 V E<sup>2</sup>

|              |         |
|--------------|---------|
| $O_2^+$      | 32      |
| $TiO^+$      | 62 - 66 |
| $TiO^{++}$   | 31 - 33 |
| $TiO_2^+$    | 78 - 82 |
| $TiO_2^{2+}$ | 39 - 41 |

|              |           |
|--------------|-----------|
| $RuO^+$      | 112 - 116 |
| $RuO^{++}$   | 56 - 58   |
| $RuO_2^+$    | 128 - 136 |
| $RuO_2^{++}$ | 64 - 68   |

|              |               |                        |
|--------------|---------------|------------------------|
| $IrO^+$      | 207 - 209     |                        |
| $IrO^{2+}$   | 103.5 - 104.5 | $IrO^{3+}$ 69 - 69.6   |
| $IrO_2^+$    | 223 - 225     |                        |
| $IrO_2^{++}$ | 111.5 - 112.5 | $IrO_2^{3+}$ 74.5 - 75 |

|             |                          |
|-------------|--------------------------|
| $WO_2^+$    | <del>198</del> 198 - 200 |
| $WO^{2+}$   | 96 - 101                 |
| $WO_2^+$    | 217 - 218                |
| $WO_2^{2+}$ | 107 - 109                |



x 12.5 mm  
 16 middle  
 x 19.5  
 approx limits  
 (conservative)

