FactSage Practical MSE302

Practical 4. Equilib Module

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Outline

- 1. <u>Some Important Thermodynamic Terms</u>
- 2. Equilib Module: Basics
- 3. <u>H₂O Equilibrium</u>
- 4. Gasification of Coal
- 5. <u>Recovery of Tin from Tin Cans</u>
- 6. Oxidation of Fe
- 7. <u>Mixing Properties</u>
- 8. Equilib Module: General Tips

Some Important Thermodynamic Terms

| Heat Capacity C_P The amount of heat required to raise the temperature of the system by 1 K during an isobaric process.Enthalpy HTotal energy of the system. The change in Enthalpy refers to the amount of heat that is exchanged with the surroundings during an isobaric process.Entropy SA thermodynamic function that is used to determine the process spontaneity. The entropy for an isolated system always increases for spontaneous processes.Gibbs Energy GA thermodynamic function that is used to determine the process spontaneity. The Gibbs energy of a closed system always decreases for spontaneous processes with constant temperature and pressure.Fugacity (Gas Species)A thermodynamic function that describes the deviation from the ideal gas behavior. It is sometimes named as effective partial pressure of gas species. For ideal gases, fugacity is numerically equal to partial pressure.Activity (Solution Species)A thermodynamic function that describes the deviation from the ideal solution behavior. It represents effective concentration of components in a solution. For ideal solutions, activity is numerically equal to mole fraction. | Term | Physical Meaning |
|---|--------------------------------|---|
| Enthalpy HTotal energy of the system. The change in Enthalpy refers to the amount of heat that is exchanged with the surroundings during an isobaric process.Entropy SA thermodynamic function that is used to determine the process spontaneity. The entropy for an isolated system always increases for spontaneous processes.Gibbs Energy GA thermodynamic function that is used to determine the process spontaneous processes.Fugacity (Gas Species)A thermodynamic function that describes the deviation from the ideal gas behavior. It is sometimes named as effective partial pressure of gas species. For ideal gases, fugacity is numerically equal to partial pressure.Activity behavior. It represents effective concentration of components in a solution. For ideal solutions, activity is numerically equal to mole fraction. | Heat Capacity \mathcal{C}_P | The amount of heat required to raise the temperature of the system by 1 K during an isobaric process. |
| Entropy SA thermodynamic function that is used to determine the process spontaneous processes.Gibbs Energy GA thermodynamic function that is used to determine the process spontaneous processes.Gibbs Energy GA thermodynamic function that is used to determine the process spontaneous processes with constant temperature and pressure.Fugacity (Gas Species)A thermodynamic function that describes the deviation from the ideal gas behavior. It is sometimes named as effective partial pressure of gas species.Activity (Solution Species)A thermodynamic function that describes the deviation from the ideal solution. For ideal gases, fugacity is numerically equal to partial pressure. | Enthalpy <i>H</i> | Total energy of the system. The change in Enthalpy refers to the amount of heat that is exchanged with the surroundings during an isobaric process. |
| Gibbs Energy GA thermodynamic function that is used to determine the process spontaneous processes with constant temperature and pressure.Fugacity (Gas Species)A thermodynamic function that describes the deviation from the ideal gas | Entropy S | A thermodynamic function that is used to determine the process spontaneity. The entropy for an isolated system always increases for spontaneous processes. |
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| Activity (Solution Species) A thermodynamic function that describes the deviation from the ideal solution behavior. It represents effective concentration of components in a solution. For ideal solutions, activity is numerically equal to mole fraction. | Fugacity (Gas Species) | A thermodynamic function that describes the deviation from the ideal gas behavior. It is sometimes named as effective partial pressure of gas species. For ideal gases, fugacity is numerically equal to partial pressure. |
| | Activity (Solution Species) | A thermodynamic function that describes the deviation from the ideal solution behavior. It represents effective concentration of components in a solution. For ideal solutions, activity is numerically equal to mole fraction. |

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Equilib Module: Some Important Terms

| Term | Physical Meaning |
|---------------------------------|--|
| | Theses terms are considered as "phase activity". When their |
| Fugacity_Total (Gas Phase) | value is 1, the phase is stable; otherwise, the phase is not stable. |
| Activity_Total (Solution Phase) | When their value is close to 1, this indicates that if the |
| Activity (Compound) | temperature and pressure change slightly, the phase might |
| | become stable. |

The Equilib Module is the **most powerful module** of FactSage.

- The module calculates the equilibrium for multiphase, multicomponent equilibria, with a wide variety of tabular and graphical output modes, under a large range of constraints (for example, given temperature, pressure, composition, etc.).
- ✓ The module uses the "Gibbs energy minimization" principle to find the phases that exist at equilibrium and their respective compositions & amounts.
- $\checkmark~$ The module accesses both Compound and Solution databases.

Different from the Reaction Module, the Equilib Module does not require a welldefined reaction equation. The user only needs to tell the Equilib Module the input elements and the equilibrium conditions, and then the Equilib Module will calculate the products at equilibrium from the list of the **possible** phases the user has selected.

Equilib Module: Basics

Equilib Module in the home page.



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Equilib Module: Basics

After you run the Equilib Module, you will see the following screen:

| 存 Equilib - Menu: Simple gas r | eaction | | | _ | | × |
|---|----------------|------------------------------------|------------------|--|------------------------------------|-----------------|
| File Units Parameters Help | | | | | | |
| | T(C) F | P(atm) Energy(J) Quantity(m | iol) Vol(litre) | [| in 🗗 C | • |
| reactants [2] | [| 2 H2 + O2 (25C,g,#1) (25C,g,#1) | | | | |
| Products | | | | | | |
| Compound species | Solution phase | s Base-Phase Ful | l Name | Custom Solution 0 fixed activit 0 ideal solution | nis lies Deta ons | s |
| o pure liquids | Menu V | Vindow 🖛 | | - Pseudonyms- | Edit . | . [] |
| pure solids 0 | incina v | | | ✓ Volume data assume mol solids and liv | ar volumes quids = 0 | of |
| species: 9 | | Reactants | Window | and physics | ar volume a I properties | ata data |
| Target | Legend | 🔽 Show 🗺 | | Virtual species: | an « Ginin j | 10 |
| Estimate T(K): 1000 Quantity(mol): 0 | | specie: solutions. | List Wind | OW plutions (r | nax 5000) max 200) max 1500) | 9 0 |
| | | | | <u>i otal Phases (m</u> | | |
| - Final Conditions | T(C) | P(stm) V Dalt | Results V | Window | mal + tran | sitions |
| | 1000 | | | transitions only | niai + tran | 0100110 |
| 10 steps 🗖 Table | 11000 | л• , | 1 calculation | open | Calculate | >> |
| actSage 7.3 | | | | | | |

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Equilib Module: Basics



A Note on "Initial Conditions"

The equilibrium that is calculated under given conditions is independent of the input species and only depends on the amounts of the various **elements** added (element matrix). For example, consider the following two scenarios:

(a) we add 1.0 mole of chalcopyrite (CuFeS₂) and 1.0 mole of oxygen (O₂) into the smelter; or,

(b) we add 0.5 mole of Cu_2O , 1.0 mole of hematite (Fe₂O₃), 1.0 mole of sulfur gas (S₂), and 0.25 mole of oxygen (O₂) into the smelter.

Note in both scenarios, the number of moles of elements added:

Cu: 1.0, Fe: 2.0, S: 2.0, and O: 2.0.

If the temperature and pressure in the smelter are maintained at the same level, the final products when the system reaches equilibrium must be same for the above two scenarios, although the heat of reaction will be different.

We will start with a simple example: H_2O .

Say we have 1 mole of H_2O . We would like to know when the system reaches equilibrium at 25 °C and 1 atm, what phase(s) are present and what are their compositions.



Before we use the Equilib Module, let us perform some manual calculations so we can better understand how FactSage works based on **the Gibbs energy minimization** principle.

[Problem] Find the equilibrium state for 1 mole of H_2O at 25 °C and 1 atm.

[Step 1] First, the system at equilibrium must meet the requirement of **mass conservation**, that is, **2 mole of hydrogen** and **1 mole of oxygen**. Clearly, there are an **infinite** number of ways (or, system configuration) so that this requirement can be met. **A few of them** are listed below:

- (1) 1 mole of $H_2O(s)$, i.e., ice
- (2) 1 mole of $H_2O(l)$, i.e., liquid water
- (3) 1 mole of $H_2O(g)$, i.e., water vapor
- (4) 1 mole of $H_2(g) + 0.5$ mole of $O_2(g)$ etc.

[Step 2] We can use the FactPS database to calculate the Gibbs energy for the above system configurations at 25 °C and 1 atm (**next page**).

(1) -306.09 kJ (2) -306.69 kJ (3) -298.10 kJ (4) -71.86 kJ

[Step 3] The system at equilibrium should possess the minimum Gibbs energy. Therefore, the equilibrium state should be configuration (2).

A Note: the Gibbs energy minimizer in FactSage employs an efficient algorithm (Lagrange's Multipliers, FactSage-Teach) that can find the system configuration with the minimum Gibbs energy under the constraints of mass balance.

Compound Module: FactPS



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Reactants Window: Define Reactants

| 4 | Equilib - Reactants | _ | | \times |
|------|--|-------------|-----------|------------|
| File | Edit Table Units Data Search Data Evaluation Help | | | |
| D | T(C) P(atm) Energy(J) Quantity(mol) Vol(litre) | 11 | 1 🕠 | N W |
| L | Don't forget the Directory. | | | |
| | Quantity(mol) Species Phase T(C) P(total |)** Strea | m# Data | a |
| | H ₂ O molecule is introd | uced. | | |
| | Do not check "Initial Conditions" because | | | |
| | we are NOT interested in the change in | | | |
| | the the second second in the change in | | | |
| | the thermodynamic properties. | 🔲 Initial C | onditions | |
| | Next >> | | | |
| Fact | Sage 7.3 Compound: 1/14 databases Solution: 0/15 databases | | | 11. |

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Reactants Window: Database(s)

| Q | Equilib - <mark>R</mark> | eactants |] | | | | _ | | \times | |
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| Ē | F | actPS | FScopp | | solutions only | EXAM | | | | |
| | | T salt | FSIead FSIead | | no database | 1 | | | | |
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| | | TOxCN | | Other | | - | | | | |
| | | Tfrtz | | | Add/Remove Data | | | | | |
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| | - Info | " H ₂ | $0 \cos^2 \theta$ | sists of i | H and O. ' | These tw | o elem | ents | can | only form gaseous species |
| L | | n | d nuro | solide | | and nure | liquid | ί۵σ | 1473 | ter) Therefore only |
| | | an | u purc | Sonus | (c.g., icc) | and pure | , iiquiu | (C.g. | , wa | ter j. Therefore, only |
| | | Fa | ctPS is | require | ed. | | | | | |
| | 0-1 | | L (| -• | | | | | | |
| | - upa | ons - sea | arch ror produ ⊢ Incl | ude compounds - | | Limits | | | | |
| FactS | | Default | | gaseous ions (pla | ismas) C | Organic species CxHy. | , X(max) = 2 | | 11. | |
| | | | | limited data comp | oounds (25C) | Minimum solution comp | oonents: O 1 💿 | 2 cpts | | |
| | | Care | al | | Summary | | | ĸ | | |
| | | Call | | | Junnary | | | | | |

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Reactants Window: Choose Units and Input the Quantity of Species

| Equilib - Reactants | | _ | | × |
|--|--------------|--------------|----------|----|
| File Edit Table Units Data Search Data Evaluation Help | | | | |
| T(C) P(atm) Energy(J) Quantity(mol) Vol(litre) | | 111 | - | 漸 |
| Choos | se the u | nits. |] | |
| Quantity(mol) Species Phase T(C. H20 We will consider 1 mole of H ₂ O. |) P(total)** | Stream# | Data | |
| Specifying the quantity requires we choose | the uni | ts fir: | st. | |
| | | Initial Cond | litions | |
| Next >> | | | | |
| FactSage 7.3 Compound: 1/14 databases Solution: 0/15 databases | | | | // |

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Menu Window: Selection of Products (Compounds and Solution Phases)

| 存 Equilib - Menu: | $ \square$ \times |
|--|--|
| File Units Parameters H | Help |
| D 🖻 🖬 | T(C) P(atm) Energy(J) Quantity(mol) Vol(litre) |
| Reactants (1) | H2D Choose the units. |
| Products Compound species + gas • ideal • real aqueous + pure liquids + pure solids species: Target | 9 9 0 2 1 12 Solution phases Custom Solutions 0 fixed activities 0 deal solutions 12 12 12 12 12 12 12 12 12 12 12 12 12 12 12 13 14 15 16 17 18 19 10 10 10 |
| rone - Estimate T(K): 1000 Quantity(mol): 0 Final Conditions | Choose all the Compound species. Normally, when only one compound database (FactPS) is selected, there is no need to screen the phases from the list. For the gas phase, we choose the ideal gas model because the gas species in the real gas model are quite limited and the assumption of ideal gas model is valid at low pressures. |

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Menu Window: Set up the Final Conditions



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Results: ChemSage Format

| 存 Equilib - Results 25 C | | | | - | | × | |
|----------------------------|---|-----------------------|----------------------|--------------|-----------|-----------------------|--|
| Output Edit Show Pages Fir | Dutput Edit Show Pages Final Conditions | | | | | | |
| Save or Print | > | T(C) P(atm) Energy(J) | Quantity(mol) Vol(li | itre) | 111 🖳 🕞 | 汉 | |
| Plot | > | | | | | | |
| Equilib Results file | > - | | | | | | |
| Stream File | > | | | | | | |
| Format | > | FACT Format | | | | | |
| Fact-XMI | , ~ | ChemSage Format | | | | | |
| | | FACT + ChemSage | | | | | |
| Fact-Optimal | > | ChemSage + FACT | | FUGACITY | | | |
| Fact-Function-Builder | > | Append list of inpu | It is recor | nmended to | use the (| ChemSage format (just | |
| Refresh | | 0.0000E+00 | | | | 8 8 | |
| Swap loops | | 0.0000E+00 | personal | preference). | | | |
| ноо | | 0.0000E+00 1 | .8813E-43 | 5.8982E-45 | | | |
| н | | 0.0000E+00 1 | .2228E-48 | 3.8337E-50 | | | |
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| 03 | | 0.0000E+00 1 | .1577E-69 | 3.6296E-71 | | | |
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| | | mol | | ACTIVITY | | | |
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| H20_ICe(s) | 1 | 0.00002+00 | | 2 24202-25 | | | |
| *********************** | ***** | ************** | ****** | 3.34206-35 | | | |
| Ср Н | | S | G | v | | | |
| J.K-1 J | | J.K-1 | J | dm3 | | | |
| ***** | ***** | ***** | ****** | ***** | | | |
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Results: ChemSage Format

| 🗘 Equilib - Results 25 C | $ \Box$ \times | |
|--|---|-----|
| Output Edit Show Pages A | inal Conditions | |
| | These are the conditions under which the system reaches equilibrium. In mo | ost |
| | cases, the volume data for condensed phases are not considered, and only th | ıe |
| T = 25 C P = 1 atm | volume of gas phase will be shown. | |
| V = 0 dm3 STREAM CONSTITUENTS H2O | AMOUNT/mol 1.0000E+00 This is the input material and its amount. | |
| PHASE: gas ideal H20 H2 O2 OH HOOH HOO H O3 TOTAL: H20 liquid(liq) | EQUIL AMOUNT MOLE FRACTION mol 0.0000E+00 1.0000E+00 3.1352E-02 0.0000E+00 7.9733E-27 2.4998E-28 0.0000E+00 3.9867E-27 1.2499E-28 0.0000E+00 5.5710E-33 1.7466E-34 0.0000E+00 5.5710E-33 1.7466E-34 0.0000E+00 1.8813E-43 5.8982E-45 0.0000E+00 1.8813E-43 5.8982E-45 3.6837E-50 2.8019E-55 3.6296E-71 3.1352E-02 mol mol Mol ACTIVITY 1.0000E+00 1.000E+00 1.000E+00 Mol | |
| H20_Ice(s) HOOH_liquid(liq) | T 0.0000E+00 7.8723E-01 0.0000E+00 3.3420E-35 When activity of a phase is 1, this means that the phase is stable. T(C) P(atri 7 Product H(J) 1 calculation | |
| "T" mark mear | ns the thermodynamic data are no longer within the effective | |
| temperature r | ange. | 21 |

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Results: ChemSage Format



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Menu Window: Set up the Final Conditions

| 存 Equilib - Menu: last system | | - 🗆 X |
|--|--|--|
| File Units Parameters Help | T(C) P(atm) Energy(J) Quantity(mol) Vol(litre) | 🕅 🗗 🖅 |
| Products (1) Products pressure | e, let us calculate the equilibre is 0.031352 atm. | rium if the |
| Compound species + gas • ideal O real 9 aqueous 0 + pure liquids 2 + pure solids 1 species: 12 Target - none - Estimale T(K): 1000 Quantity(mol): 0 | Image: solution phases Full Name Image: solution phases Full Name Image: solution phase phase Full Name Image: solution phase phase phase Full Name Image: solution phase phas | Custom Solutions Details 0 fixed activities Details 0 ideal solutions Pseudonyms apply Edit Volume data assume molar volumes of solids and liquids = 0 • include molar volume data and physical properties data • paraequilibrium & Gmin edit Virtual species: 0 • Total Species (max 5000) 12 • Total Phases (max 1500) 4 |
| Final Conditions <a> 10 steps Table | T(C) P(atm) ▼ Product H(J) ▼ 25 0.031352 | Equilibrium normal normal + transitions transitions only open Calculate >> |

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Results: ChemSage Format

| 存 Equilib - Results 25 C | | - 🗆 × |
|--|--|--|
| Output Edit Show Pages Final | I Conditions T(C) P(atm) Energy(J) Quantity(mol) Vol(litre) | III 🖳 🕞 🔀 |
| T = 25 C P = 3.1352E-02 atm V = 780.25 dm3 | This time, we changed the pressur the system certainly contains gas. | re. Because the volume is not zero, this time |
| STREAM CONSTITUENTS H2O H2 O2 OH H0OH H0O H 0 O2 | AMOUNT/mol 1.0000E+00 EQUIL AMOUNT MOLE FRACTION FUGACITY mol atm 1.0000E+00 1.0000E+00 3.1352E-02 7.9733E-27 7.9733E-27 2.4998E-28 0E-33 5.5710E-33 1.7466E-34 1.2298-28 0E-33 5.5710E-33 1.7466E-34 1.7E-36 2.0017E-36 9.4110E-28 3E-43 1.8013E-43 5.8982E-45 1.2228E-48 1.2228E-48 3.8326E-50 8.9366E-54 8.9368E-54 2.8019E-55 1.1577E-69 1.1577E-69 3.6296E-71 | Total fugacity is 1 atm. This means the gas phase is stable. |
| TOTAL: System component O H H20 liquid(liq) H20_Ice(s) T H00H_liquid(liq) Cp H J.K-1 J 3.25886E+01 -2.41834E+05 | 1.0000E+00 1.0000E+00 1.0000E+00 Amount/mol Amount/gram Mole fraction 1.0000 15.999 0.32323 0.88810 2.0000 2.0159 0.66667 0.11190 mol ACTIVITY 0.0000E+00 9.99999E-01 0.0000E+00 7.8722E-01 0.0000E+00 3.3420E-25 S G V J.K-1 J dm3 2.17513E+02 -3.06686E+05 7.80351E+02 1.00351E+02 | very close to 1. This means that liquid H_2O is very close to be a stable phase. |
| This is expecte | ed because when we reduce the pres | ssure, gas tends to be stable. |

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The second example we will be looking at is the gasification of coal by steam. Say we inject the hot steam into a coal bed. The temperature of the coal bed is maintained at 1000 K, and the pressure at 10 atm. We would like to know what species are obtained at equilibrium as well as their respective amounts.



Reactants Window: Define Reactants



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Reactants Window: Database(s)

| 😝 Equilib - Reactants | – 🗆 X |
|--|---|
| File Edit Table Units Data Search Data Evaluation Help | |
| Data Search | × |
| Databases - 1/14 compound databases, 0/15 solution databases Cact GactSage" SGTE Compounds only Solutions Solutions | abases |
| FThall FT0xCN FTfrtz FTfrtz FThelg ELEM SGnobl FTpulp FTdemo SpMCBN RefreshDatabases TDmeph FTlite FTnucl TDnucl | |
| There is no condensed solutions. Only p are considered. Therefore, only FactPS is | oure solids (carbon) and gas mixture is required. |
| FactS Options - search for product species Include compounds Limits Include compounds Organic species CxHy, X(max) Include compounds (25C) Minimum solution components: C |]= 2 D 1 ⊙ 2 cpts |
| Cancel Summary | OK |

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Reactants Window: Choose Units and Input the Quantity of Species

| C Equilib - Reactants | _ | | \times | | |
|---|------------|----------|----------|--|--|
| File Edit Table Units Data Search Data Evaluation Help | | | | | |
| T(K) P(atm) Energy(J) Quantity(mol) Vol(litre) | <u>111</u> | 9 | * | | |
| ¹⁻² Choose the u | nits. | | | | |
| Quantity(mol) Species Phase T(K) P(total)** 2 C | Stream | n# Data | | | |
| | 1 | | | | |
| | | | -11 | | |
| We will consider a very simple case: 2 mole of | C re | acts | | | |
| with 1 mole of steam | | | | | |
| | | | | | |
| | | | | | |
| Specifying the quantity requires we choose the units first. | | | | | |
| | | | | | |
| | Initial Co | nditions | | | |
| Next >> | | | | | |
| FactSage 7.3 Compound: 1/14 databases Solution: 0/15 databases | | | //. | | |

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Menu Window: Selection of Products (Compounds and Solution Phases)

| 存 Equilib - Menu: last system | | – 🗆 X |
|---|--|--|
| File Units Parameters Help | | |
| D 😂 日 | T(K) P(atm) Energy(J) Quantity(mol) Vol(litre) | 🚻 📑 💽 📧 |
| Reactants (2) | 2 C + H20 Choose th | e units. |
| Products | | |
| Compound species + gas • ideal O real 41 aqueous 0 + pure liquids 9 + pure solids 3 | Solution phases | Custom Solutions O fixed activities O ideal solutions Oseudonyms apply Edit Colume data |
| species: 53 | Choose all the Compound sp | Decies. |
| Target - none - Estimate T(K): 1000 Quantity(mol): 0 | Legend ✓ Show ● all ○ selected Virt species: 0 Select Iol solutions: 0 Select Iol Iol | paraequilibrium & Gmn <u>edit</u> ual species: 10 tal <u>Species (max 5000)</u> 53 tal <u>Solutions (max 200)</u> 0 tal Phases (max 1500) 13 |
| Final Conditions | Equil | ibrium |
| <a> | T(K) P(atm) | mal C normal + transitions |
| | 1000 1 C trar | nsitions only |
| 10 steps I Table | 1 calculation | en Calculate >> |
| FactSage 7.3 | | |

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Menu Window: Set up the Final Conditions

| 存 Equilib - Menu: last system | | - 🗆 X |
|---|--|---|
| File Units Parameters Help | | |
| D 🚔 🖬 | T(K) P(atm) Energy(J) Quantity(mol) Vol(litre) | |
| Reactants (2) | 2 C + H20 | |
| Products | | |
| Compound species | Solution phases | Custom Solutions |
| + gas ● ideal ○ real 41 aqueous 0 | ▼ + Base-Phase Full Name | 0 fixed activities Details 0 ideal solutions |
| F pure liquids 9 | These are the equilibri | um conditions under which |
| species: 53 | We want to calculate. | Image: Second Control of |
| | | Total Phases (max 1500) 13 |
| Final Conditions | T(c) | Equilibrium |
| | Product H(J) ▼ Product H(J) ▼ | C hormal C hormal + transitions |
| 10 steps Table | 1 calculatio | Only 1 calculation will be performed |
| | | under the given conditions. |
| FactSage 7.3 | | |

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Save the Equilib settings: ".dat" file

In the Equilib Module, we can save the settings for a calculation as a ".dat" file.

| 存 Equilib - Menu: last system | | | Save File in w:\MSE302\Exercise\Equi*.dat X | | | |
|---|--------------------|--------|--|--|--|--|
| File Units Parameters Help | | | Enter the file number | | | |
| | New C | | (1 - 9999) | | | |
| | Open | Ctrl+O | or enter the file name, for example | | | |
| | Directories Ctrl+D | | Mu veru favorite calculation | | | |
| | Save | Ctrl+S | | | | |
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| | FSReactor File | > | Save File w:\MSE302\Exercise\EquiCoal_gasification.DAT X | | | |
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| | | | - to add additional notes, terminate the line of comments with the character + | | | |
| | | | FactPS dayanase, 1000 K and 10 atm | | | |

Open the ".dat" file

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| | | T(K) P(atm) Energy(J) Quantity(mol) Vol(litre) | ľ | 11 🖳 🕻 | • | |
| | Directory Equilib (My Files) | le w:\MSE302\Exercise\EquiCoal_gasification.DAT | — | × | | |
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| | File Date Desc Coal gasification 22/u/22 Eact | ription PS davanase 1000 K and 10 atm / 2 C + H20 | | | | |
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| | | directory. | | | | |
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Results: ChemSage Format



Pelton, Phase Diagrams and Thermodynamic Modeling of Solutions, 2019 (Chapter 5.12)

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Save the Results: Spreadsheet Format



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The third example is to recover tin from tin cans by chlorination, represented by the following reaction:

 $Sn + 2Cl_2 = SnCl_4$

Tin cans are made of tin-coated steel. Progressive chlorination of tin results in the exposure of iron. To avoid the chlorination of iron which would lower the grade of SnCl_4 , oxygen is introduced to form Fe_2O_3 . This means that we need to study the thermodynamics of the Fe-Sn-Cl-O system for this chlorination process if the steel is considered to consist of pure iron. Under the controlled conditions, the desired solid products should be SnCl_4 and Fe_2O_3 .

To help you better understand the underlying thermodynamic principle on which the above process is based, the predominance diagram of the Fe-Sn-Cl-O system was calculated.

Equilib Module: Recovery of Tin from Tin Cans

Predominance Diagram of the Fe-Sn-Cl-O System at 700 °C.

| Predom | — | × |
|---|---|---|
| File Units Data Search Help | Massímoli | 🕼 Data Search |
| Elements • 2-Metal Example • 2-Metal Example Metals: Fe Snon-metals: Clear Optional Next >> Metal Mole Fracti System components 2-Metal Diag R = Sn/(Fe + Sn) 0.0000 < R < 1.0000 | Parameters Pressure Isobar: P(atm): Constants Temperature Z: T(C): 700 Y-axis log10[2): Y-axis log10[Y) Y: P(Cl2) max: 0 min: -12 step: 1 Labels and Display color chemical 12 number color none color Calculate invariant point Calculate >> invariant point | ■ Databases - 1/14 compound databases, 0/15 solution database Image: Compound Stress Image: Compound Stress |

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Predominance Diagram of the Fe-Sn-Cl-O System at 700 °C.



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Part I.

Let us start with a simple calculation. Say we are recovering 1.0 mol of Sn, and the exposed iron is **assumed** to be 0.2 mol. Clearly, the minimum number of moles of Cl_2 is 2.0 mol when all Sn is recovered as $SnCl_4$; and the minimum number of moles of O_2 when all the exposed iron is oxidized to Fe_2O_3 is 0.15 mol.

 $1.0 \text{ mol Sn} + 2.0 \text{ Cl}_2 = 1.0 \text{ mol SnCl}_4$

 $0.2 \text{ mol Fe} + 0.15 \text{ O}_2 = 1.0 \text{ mol Fe}_2 \text{ O}_3$

Of course, if O_2 is supplied from air (21 vol. % O_2 + 79 vol. % N_2), then the number of moles of N_2 is 3.76 × 0.15 mol = 0.564 mol.

Also, we assume all the reactants are introduced into the reactor at room temperature.

Reactants Window: Define Reactants (Species)

| 👍 Equilib | - Reacta | nts | | | | | | | | - | | \times |
|--------------|----------|----------|------------|----------|------------|----------------------|----------|------|------------|---------------|-------------|----------|
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| 1.5 | | | | | | | | | | | | |
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| | Quant | ity(mol) | | Specie | es | Phase | | T(C) | P(total)** | Stream# | Data | |
| 1 | | | Sn | | | | - | | | 1 | | |
| + 1 | | | Fe | | | | - | | | 1 | | |
| + 1 | | | | 2 | — Г | | - | | | 1 | | |
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| | | | | | | Next >> | | | | | | |
| FactSage 7.3 | Co | mpound: | : 1/14 da | tabases | Solution: | 0/15 databases | | | | | | |

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Reactants Window: Select Database(s)

| Q | Equilib - Reactants | $ \Box$ \times |
|------|--|---|
| File | Edit Table Units Data Search Data Evaluation Help | |
| | 😰 🕂 🥅 T(C) P(atm) Energy(J) Quantity(n | nol) Vol(litre) |
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| | -Datahases - 1/14 compound datahases_0/15 solution datahas | \$ 6 \$ |
| | FactPS FScopp BINS Solutions only Solutions on Solution | Private Databases |
| | Floxid FSlead SGPS FTsalt FSstel SGTE FTmisc FSupsi SGsold ETball Clear All | Select FactPS only. |
| I | FT0xCN Other Add/Remove Data FTfrtz Add/Remove Data FThelg ELEM SGnobl | In this example, the major species we are interested in include $SnCl_2$, $SnCl_4$, SnO_2 , $FeCl_2$, $FeCl_3$, Fe_2O_3 , Cl_2 , O_2 , N_2 , |
| l | FTpulp FTdemo SpMCBN RefreshDatabases TDmeph TDmucl TDnucl | etc. Since all these species are either pure solids/liquid or |
| | -Information - | gases, there is no need to choose any solution database. |
| l | | |
| | -Options - search for product species | |
| Fac | Default Include compounds Incl | anic species $CxHy, X(max) = 2$ inimum solution components: $\bigcirc 1 \odot 2$ cpts |
| | Cancel Summary | |

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Reactants Window: Choose Units and Input the Quantity of Species

| 存 Equilib - Reactants | | | | _ | | |
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| File Edit Table Units | Data Search Data Eva T(C) P(| luation Help atm)Energy(J)Quantity(n | nol) Vol(litre) | | |] |
| 1-5 | | | Choose | the un | its. | |
| Quantity(mol) 1 + 0.2 + 2 + 0.15 + 0.564 | Species Sn Fe Cl2 02 N2 After choo quantity o | Phase | T(C) P(to | stream 1 1 1 1 1 1 1 1 | m# Data | |
| | | | | 🔲 Initial Co | onditions | |
| | | Next >> | | | | |
| FactSage 7.3 Compound: | 1/14 databases | Solution: 0/15 databas | es | | | / |

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Reactants Window: Choose "Initial Conditions"

| Q | 🗘 Equilib - Reactants | | | | | | Once "In | nitial (| Cone | ditions" is checked, we need to |
|----------------------------------|--|----------------|-----------------------------------|----------------------------|----------------------------|------------|---------------|-------------------|-------------------|--|
| File | Ed | it Table Units | Data Search Data Eval T(C) P(a | uation Help m)Energy(J) |) Quantity(mol) Vol(lit | irej | specify | the ph | nase | (i.e., structure) of species (see |
| | 1.5 | | | | | | next pag | ges for | r mo | ore information). |
| | | | | | | | | | | |
| | | Quantity(mol) | Species | | Phase | T(C | ;) P(total)** | Stream# | Data | |
| | | 1 | Sn | solid-1 | Solid(wh) 👤 | 25 | 1.0 | 1 | | |
| | + | 0.2 | Fe | solid-1 | bcc 💌 | 25 | 1.0 | 1 | | |
| | + | 2 | C12 | gas | – | 25 | 1.0 | 2 | | |
| | + | 0.15 | 02 | gas | – | 25 | 1.0 | 3 | | |
| | + | 0.564 | N2 | gas | • | 25 | 1.0 | 3 | | |
| L | | | | | Also, w | ze w | vant to a | ssign | Str | eam# to the reactants (Sn and Fe |
| | | | | | aro in | 1 st C | Stroom | Cl in | 7 nd | Stroom and air in 2rd Stroom) Vou |
| | | | | | | 1 J | | ¹² III | Δ | Stream, and an in 5 th Streamj. Tou |
| For a gaseous stream this is the | | | | | | click "Sti | ream# | f" to | see more details. | |
| l | partial pressures of the species in that stream. | | | | | | | | | |
| | | | | Nex | • > > | | | | | |
| Fact | Sage | 7.3 Compound: | 1/14 databases S | olution: 0/1 | 5 databases | | | | | |
| | | | | | | | | | | 42 |

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View Data Module: Structure of Sn and Fe at 25 °C, 1 atm

| View Data |
|---|
| View compounds - enter a list of elements or a compound or ALL |
| Examples: AI Ca 0 - compounds of AI, Ca and/or 0 Si02 - compound Fe2(S04)3 - compound Cu[++] - cation 0H[·] - anion ALL - all compounds ALL Fe - all compounds of Fe ALL S04 - all compounds with S04 ALL Fe S 0 - all compounds with Fe, S and 0 |
| Pressure Energy Image: Compound Image: Compound I |
| Compound Databases (14) |
| Summary Add Remove FactPS 💌 |
| C:\FactSage\FACTDATA\FS53base.cdb |
| FactPS - FACT pure substances database (2019) |
| Elements or Compound or ALL: |
| Exit Assessments Information OK |
| View Data Sn Units: T(K) P(atm) Energy(J) Quantity(mol) |
| File Edit Sort Compounds Summary Databases Units Atom |
| 8 compounds, 14 phases FactPS - FACT pure substances of |
| Compounds ordered by alphabet (see 'Sort |
| Fe FactPS S1 S2 L G |
| Fe[+] FactPS G |
| Fe[2+] FactPS Aq |
| Fe[3+1 FactPS Aq |
| Sn FactPS S1 S2 L G |
| Sn[2+] FactPS Aq |
| |

| File Edit Sort Compounds Summary Databases Units Atomic Wts. Table Graph Help << Back | <th>存 View Data 🛛 Fe 🛛 Uni</th> <th>ts: T(K) P(atm) Ene</th> <th>rgy(J) Quantity(m</th> <th>ol)</th> <th></th> <th>— 🗆</th> <th>×</th> | 存 View Data 🛛 Fe 🛛 Uni | ts: T(K) P(atm) Ene | rgy(J) Quantity(m | ol) | | — 🗆 | × |
|--|---|------------------------|---------------------|----------------------|-------------|-------------|---------|---|
| FactPS - FACT pure substances database (2019) Phases Cp(T) H(T) G(T) File (Trans. Mol Wt.% Name: Iron Standard ref At 25 °C, S1 which is bcc is stable. Transition T(K) T(C) Delta H Delta S Delta Cp J/mol J/mol J/mol-K J/mol-K Standard ref Standard ref At 25 °C, S1 which is bcc is stable. Transition T(K) T(C) Delta Cp J/mol J/mol-K J/mol-K S1 1667.47 1394.32 825.8 0.4455 2.183 S1 1667.47 1394.32 825.8 0.4455 2.183 S1 Difter FACT pure substances database (2019) File Edit Sort Compounds Summary Databases Dilter Fefs <th< td=""><td>File Edit Sort Compo</td><td>ounds Summary</td><td>Databases Unit</td><td>ts Atomic Wts.</td><td>Table Graph</td><td>Help << Bac</td><td>k</td></th<> | File Edit Sort Compo | ounds Summary | Databases Unit | ts Atomic Wts. | Table Graph | Help << Bac | k | |
| Phases Cp(T) H(T) G(T) S(T) Volume Magnetic Refs. Trans. Mol Wt.Z Name: Iron Standard of At 25 °C, S1 which is bcc is stable. Transition T(K) T(C) Delta H Delta S Delta Cp J/mol J/mol J/mol J/mol-K J/mol-K S1 -> S2 1184.81 911.66 1012.9 0.855 -7.681 S2 -> S1 1667.47 1394.32 825.8 0.495 2.183 S1 -> L1 1810.95 1537.80 13806.9 7.624 4.653 L1 -> G1 (1 atm) 3131.33 2858.78 349631.2 111.635 -18.938 View Data Sn Units: T(K) P(atm) Energy(J) Quantity(mol) - × × FactPS -FACT pure substances database [2019] Phases Cp(T) H(T) G(T) S(T) Volume Magnetic Refs. Trans. Mol Wt.2 Name: Tin At 225 °C , S1 which is solid(wh) is stable Transition T(K) T(C) | 4 Phases | Fac | tPS - FACT pure sub | bstances database (2 | 2019) | | | |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | | | | Value VMare | | - N. | | |
| Name: Iron Standard in Standard in At 25 °C, S1 which is bcc is stable. Transition T(K) Delta H Delta Cp J/mol J/mol-K J/mol-K STANDARD Delta Cp J/mol J/mol-K J/mol-K J/mol J/mol-K J/mol-K STANDARD Delta Cp J/mol J/mol-K J/mol-K J/mol J/mol-K J/mol-K STATURE STATUS STATURE STATUS STATURE STATUS STATURE STATUS STATURE STATUS FACT pure Status Mol WL 2 FACT pure substances database (2019) Phases Cp(T) Mol WL 2 FACT pure substances database (2019) Mol WL 2 Name: Tin Mol WL 2 Name: Tin At 25 ° | Fnases Cp[1] | הנון מנו |] [] []] | volume magn | euc ners. | Trans. Mor | ₩1.4 | |
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| $\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$ | | Standa | at 2 | 5 °C, S1 | which i | s bcc is | stable. | |
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| $\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$ | Transition | T(K) | T(C) | Delta H | Delta S | Delta Cp | I | |
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| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | S1> S2 | 1184.81 | 911.66 | 1012.9 | 0.855 | -7.681 | | |
| S1> L1 1810.95 1537.80 13806.9 7.624 4.653 L1> G1 (1 atm) 3131.93 2858.78 349631.2 111.635 .18.938 View Data Sn Units: T(K) P(atm) Energy(J) Quantity(mol) - - × File Edit Sort Compounds Summary Databases Units: Atomic Wts. Table Graph Help << Back Phases Cp(T) H(T) G(T) S(T) Volume Magnetic Refs. Trans. Mol Wt.% Name: Tin At 255 °C, S1 which is solid(wh) is stable J/mol-K J/mol-K J/mol-K L1 -> S2 55.06 -218.09 93955.4 180.808 -421.031 S2 -> S1 296.56 23.41 2090.1 7.048 1.187 S1 -> L1 505.06 231.91 7029.1 13.917 -1.039 | S2> S1 | 1667.47 | 1394.32 | 825.8 | 0.495 | 2.183 | | |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | S1> L1 | 1810.95 | 1537.80 | 13806.9 | 7.624 | 4.653 | | |
| View Data Sn Units: T(K) P(atm) Energy(J) Quantity(mol) - - × File Edit Sort Compounds Summary Databases Units: Atomic Wts. Table Graph Help << Back | L1> G1 (1 atm) | 3131.93 | 2858.78 | 349631.2 | 111.635 | -18.938 | | |
| Name: Tin At 25 °C, S1 which is solid(wh) is stable Transition T(K) T(C) Delta H Delta S Delta Cp Image: | View Data Sn Units: T(K) P(atm) Energy(J) Quantity(mol) File Edit Sort Compounds Summary Databases Units Atomic Wts. Table Graph Help << Back 4 Phases FactPS - FACT pure substances database (2019) Phases Cp(T) H(T) G(T) Volume Magnetic Refs. Trans. | | | | | | | |
| Transition T(K) T(C) Delta H Delta S Delta Cp Image: I | At 25 °C, S1 which is solid(wh) is stable. | | | | | | | |
| Image: Second | Transition | T(K) | T(C) | Delta H | Delta S | Delta Cn | T | |
| L1 -> S2 55.06 -218.09 9955.4 180.808 -421.031 S2 -> S1 296.56 23.41 2090.1 7.048 1.187 S1 -> L1 505.06 231.91 7029.1 13.917 -1.039 | | , | | J/mol | J/mol-K | J/mol-K | 1 | |
| S2 -> S1 296.56 23.41 2090.1 7.048 1.187 S1 -> L1 505.06 231.91 7029.1 13.917 -1.039 | L1> S2 | 55.06 | -218.09 | 9955.4 | 180.808 | -421.031 | 1 | |
| S1 -> L1 505.06 231.91 7029.1 13.917 -1.039 | S2> S1 | 296.56 | 23.41 | 2090.1 | 7.048 | 1.187 | | |
| | S1> L1 | 505.06 | 231.91 | 7029.1 | 13.917 | -1.039 | | |
| L1> G1 (1 atm] 2872.94 2599.79 295769.0 102.950 -2.033 | L1> G1 (1 atm) | 2872.94 | 2599.79 | 295769.0 | 102.950 | -2.033 | | |

43

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Menu Window: Select the Products

| 😝 Equilib - Menu: last system | — | | \times |
|--|--|--|---|
| File Units Parameters Help | | | |
| T(C) P(atm) Energy(J) Quantity(mol) Vol(litre) | 111 | 9 | |
| Sn + 0.2 Fe + 2 Cl2 + 0.15 0.2 + 0.564 N2 (25C,s1,#1) (25C,s1,#1) (25C,g,#2) (25C,g,#3) (25C,g,#3) | | | |
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| | activities solutions yms cies. hysical p quilibrium cies: cies (max tions (max | Edit Edit me so me da roperties & Gmin _ 5000) x 200) | s of ata data edit 10 73 0 33 |
| Final Conditions Equilibrium <a> T(C) P(atm) Delta H(J) | C norm | nal + trans | itions |
| 1000 1 C transitions 10 steps Table 1 calculation | only Ca | lculate : | >> |
| FactSage 7.3 | | | |

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Menu Window: Set the Final Conditions

| 🗘 Equilib - Menu: last system | - 🗆 × |
|---|---|
| File Units Parameters Help | |
| T(C) P(atm) Energy(J) Quantity(mol) Vol(litre) | 📊 🔜 💽 🐨 |
| Sn + 0.2 Fe + 2 Cl2 + 0.15 02 + 0.564 N2 (25C,s1,#1) (25C,s1,#1) (25C,g,#2) (25C,g,#3) (25C,g,#3) | |
| Products Compound species + gas • ideal • real 41 aqueous 0 - pure liquids | stom Solutions fixed activities Details ideal solutions eudonyms |
| Set the temperature ran species: 73 Set the temperature ran and the total pressure in calculations at different | nge from 500 to 800 °C at 100 °C intervals, is 1 atm. This allows us to perform 4 t temperatures. |
| - none - Estimate T(K): 1000 Quantity(mol): 0 | I <u>Species (max 5000)</u> 73 I <u>Solutions (max 200)</u> 0 I <u>Phases (max 1500)</u> 33 |
| Final Conditions Equilibrit <a> T(C) P(atm) Delta H(J) | rium al O normal + transitions itions only Calculate >> |
| FactSage 7.3 | |

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Results: (Here, we again use the ChemSage format)

| 🕞 Equilib - Results 500 C (page 1/4) | | | | | | - 🗆 X |
|---|--------------|----------------------|--------------------------|------------|---------------------------------------|--|
| Output Edit Show Pages Final Con | ditions | | | | | |
| | unions | T(C) D(-ha) Energy() |) |) | | |
| | | T(U) P(atm) Energy(J | j Quantity(molj Vol(litr | rej | _ | 🛄 💷 🕞 🧏 |
| - 500 C - 600 C 700 C 800 C | | | _ | | | |
| | Equi | lihrium | Conditi | ons | | |
| T = 500 C | Lyun | indituini | conun | 0115. | e 7.3 | ^ |
| P = 1 atm | | | | | - | |
| V = 99.138 dm3 | | | | | | |
| | | | | | | |
| STREAM CONSTITUENTS | AMOUNT/mol | TEMPERATURE/C | PRESSURE/atm | STREAM | | Thermodynamic properties of the system at 1 |
| Sn_Solid(wh) | 1.0000E+00 | 25.00 | 1.0000E+00 | 1 | · · · · · · · · · · · · · · · · · · · | Thermoughanne properties of the System at |
| Cl2/gas_ideal/ | 2.0000E+00 | 25.00 | 1.0000E+00 | 2 | | |
| 02/gas ideal/ | 1.5000E-01 | 25.00 | 1.0000E+00 | 3 | | the initial state. |
| N2/gas_ideal/ | 5.6400E-01 | 25.00 | 1.0000E+00 | 3 | | |
| ***** | ***** | ***** | ***** | | | |
| Cp_INI H_INI | S_INI | G_INI | V_INI | | | |
| *************************************** | ************ | U ************ | ****** | | | |
| 1.20694E+02 -6.31482E-03 | 6.44404E+02 | -1.92129E+05 | 6.63995E+01 | | | Gas phase the total fugacity is 1 which means |
| | | | | | _ | dus phase, the total tagaenty is I which means |
| | EQUIL AMOUNT | MOLE FRACTION | FUGACITY | | | the second case is stable. The main second |
| PHASE: gas_ideal | mol | C 215 CE 01 | atm | | | the gas phase is stable. The major gaseous |
| N2 | 5 6400E-01 | 3 60938-01 | 3 60938-01 | | | |
| FeC13 | 5.8786E-03 | 3.7620E-03 | 3.7620E-03 | | | spacios aro SnCl and N This means Sn is |
| (FeC13)2 | 5.7030E-03 | 3.6496E-03 | 3.6496E-03 | | | species are shere and N_2 . This means shifts |
| TOTAL: | 1.5626E+00 | 1.0000E+00 | 1.0000E+00 | | | |
| System component | Amount/mol | Amount/gram | Mole fraction | Mass fract | tion | I chlorinated and removed very efficiently |
| Sn Fo | 1 72457-02 | 0 96964 | 2 02068-02 | 0.42489 | -02 | emormated and removed very emoteneity. |
| C1 | 3.9997 | 141.80 | 0.65228 | 0.51429 | 03 | |
| 0 | 1.4589E-11 | 2.3341E-10 | 2.3791E-12 | 8.4654E | -13 | |
| N | 1,1280 | 15,800 | 0.18395 | 5.7302E | -02 | |
| | mol | | ACTIVITY | | | Pure solids: Fe_2U_3 , SnU_2 , and FeU_1_2 are |
| Fe203_hematite(s) | 9.1264E-02 | | 1.00008+00 | | | |
| FeCl2 solid(s) | 1.2611E-04 | | 1.0000E+00 | | | stable Other compound species have an |
| FeCl2 liquid(liq) | 0.0000E+00 | | 3.0049E-01 | | | stable. Other compound species have an |
| SnO2_L1(liq) | 0.0000E+00 | | 1.7599E-01 | | | |
| FeCl3_liquid(liq) | 0.0000E+00 | | 2.7558E-02 | | | l activity less than 1 which are not stable Also |
| SnCl4_liquid(liq) T | 0.0000E+00 | | 1.6389E-02 | | | |
| Fe304_Magnetite(s) | 0.00002+00 | | 1.43688-02 | | | |
| FeCl3 Molysite(s) | 0 Final Cond | tions | 2.01000 00 | | | $ Fe_2 U_2 $ is the major species. |
| FeOC1_solid(s) | 0 <a> | | T(C) | P(atm) | Delta H(J) | |
| FeO_Wustite(s) | 0 | | 500 800 100 | 1 | | |
| ********************** | **** | , | -, , | | | |
| < | | | | | | |

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Results: let us plot the data (this time we use Output\Plot)



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Results: let us plot the data (this time we use Output\Plot)

| Equilib - Results 500 C (page 1/4) | – 🗆 × | | |
|--|--|------------------------------|---------------------|
| Output Edit Show Pages Final Conditions | Bassiles Des servers un MSE 202) Europia | -\ [:0 | ~ |
| Save or Print > T(C) P(atm) Energy(J) Quantity(mol) Vol(litre) | File Heln | e/Equivires | ^ |
| Plot > Plot Results | Sn + 0.2 Fe + 2 | Cl2 + 0.15 O2 + | • |
| Equilib Results file > Repeat Plot | Axes Variables | Minimum | Maximum |
| | activity | 0 | 1 |
| Stream File > + 0.15 02 + | mole | 0 | 4 |
| (25,1,g,#2) (25,1,g,#3) | mole fract. soln. species | 0 | 0.652276 |
| Pomat / | gram | 0 | 275.73 |
| | weight % soln. species | 0 | 93.248 |
| Fact-XML | Alpha | 0 | 0 |
| Pal | T(C) | 500 | 800 |
| Fact-Optimal > 1, 99.138 litre, 2.7812E-03 gram.cm-3) | P(atm) | 1 | 1 |
| a=1,0000) | Delta Cp(J/K) | 25.765 | 115.19 |
| Fact-Function-Builder > SrG14 | Delta G(J) | -9.6921E+05 | -7.7538E+05 |
| | Vol(litre) | 99.138 | 141.34 |
| Perfect E.C.1.2 | Delta H(J) | -4.8986E+05 | -4.3610E+05 |
| renesh | Delta V(litre) | 32.738 | 74.936 |
| Swap loops (ieclis) 2) | Delta S(J/K) | -26.607 | 31.403 |
| | · page · | 1 | 4 |
| + 9 1264E-02 mol Fe2O3 hemavite | Axes Species | - Graph | |
| Feel free to use Fact-XML. However, | 0 selected Select | Labels Disp size: 9 no: 4 | color 🔽 full screen |
| come functions in the "Dlot" can not be | | 💽 💿 chemical 🛛 🗖 | C Viewer |
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| + 1.26112-04 mol FeC12 S011d | FactSage 7.3 wr\MSF302\Evercise\Eg | uil res | 26Jul22 A sets |
| (1.5984E-02 gram, 1.2611E-04 mol) | Tactodge 1.0 | 40.705 | 2000122 4 0010 |
| - (508 Cm ²) 511 00000 | | | |
| + 0 (A> (B> T(C) P(atm) Delta H(J) | 4 calculations × | | |
| 500 800 100 1 | Calculate >> | | |
| < | > | | |

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Results: let us plot the data (this time we use Output\Plot)



Choose "Sn_Gas" under the option of "ELEMENTS" (NOT the option of "Gas"). This is all the Sn contained in the gas phase. From the option of "Gas", you would see Sn exists as Sn, Sn₂, SnO, SnO₂, O_2Sn_2 , O_3Sn_3 , O_4Sn_4 , SnCl, SnCl₂, and **SnCl₄** (major species of Sn carrier).



Results: let us plot the data (this time we use Output\Plot)



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Results: let us plot the data (this time we use Output\Plot)



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Part II.

For Part II, we will be looking at what happens if the amount of oxygen supplied is not sufficient to oxidize the exposed iron.

Assume the amount of the exposed iron is a variable: for 1 mol of Sn, the amount of the exposed iron varies from 0.2 to 0.6 mol. The temperature is fixed at 600 °C.

Back to the Reactants Window:

| 🕼 Equilib - Reactants | - 🗆 × |
|--|---|
| File Edit Table Units Data Search Data Evaluation Help | |
| 🗅 🚄 🕂 🥅 T(C) P(atm) Energy(J) Qu | iantity(mo <mark>), Vol(litre) 🗰 📖 👞 😽 🔤</mark> |
| | 🔷 Quantity — 🗆 X |
| 1.5 | |
| | Enterthe encount of the encoderst Encounters 10, 14207, 1 0245, 4 |
| Quantity(mol) Species Pl | hase For example, the formation of water: |
| 1 Sn solid-1 Sol | id(wh) 1 H2 + 0.5 O2 |
| + <a> Fe solid-1 box | C A composition veriable "A" (alpha) may be specified in the form (aA+b) or (a+bA) where a and b are |
| + 2 Cl2 gas | constants, A is calculated or specified later. |
| + 015 02 0as | Examples: <a> <-1+2A> <3.7A+6>. For example, a binary mixture between conner and nickel: |
| | A> Cu |
| * 0.5 <mark>64 N2 gas</mark> | + <1-A> Ni |
| | A composition variable "B" (beta) may be specified in the form <aa+bb+cab+d> where a, b, c and d are constants. A and B are specified later in the Menu Window. Whereas you can specify or calculate a range [First Last, Step] of <a>, for example [0.0 1.0 0.1], only one constant value of can be specified. For example the oxidation of various quantities of hydrogen by oxygen diluted in nitrogen. Say you want to have 1 mole total of input gases you might enter: <a> H2 + <1-A-B> O2 + N2 If the fixed quantity of N2 is 0.1 mole, then in the [Menu Window] you would specify = 0.1 and give a range for alpha, say <a> = [0.0 0.9 0.1].</aa+bb+cab+d> |
| Next >> | |
| FactSage 7.3 Compound: 1/14 databases Solution: 0/15 d | latabases // |
| | 53 |

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Menu Window

| 存 Equilib - Menu: comments | 🛊 Final Conditions – 🗆 🗙 |
|---|---|
| File Units Parameters Help | |
| D 🗃 🖬 🛛 🖓 | |
| Reactants (5) | In most cases you specify values of T and P (and <a> and if necessary). For example T = 1000 and P = 1. |
| Compound species | A range is indicated by [FIRST LAST (STEP, optional)]] For example '[500 1000]' in the T column means T = 500 and 1000; '[500 1050 100]' means T = 500, 600, 700 1000 and finally 1050. |
| u ga <mark>s t⊙ ideal C real 41 u u u u u u u u u u u u u u u u u u </mark> | Leave the column blank if it is not specified. |
| acueous 0 + pure liquids 10 + pure solids 22 | When the reactant initial conditions have been specified ("Initial Conditions" box in [Reactants Window] is 'checked') a column for extensive variables (Delta H, Delta V, etc) is activated. Now you have the option specifying only one of T or P together with one of the extensive variables. |
| species: 73 | If you only specify one variable, say P =1, then you can perform a Target Phase calculation i.e. that temperature is calculated when the Target Phase becomes stable. You must specify which compound or solution is the target phase. In the case of solutions, the target may be a Formation Target Phase (unit activity) or Precipitate Target Phase (unit activity, 100% moles). Click on the Target Phase frame with the mouse-right-button for details. |
| Final Conditions | Equilibrium |
| | Platmj _ Delta H[J] _ O normal O normal + transitions |
| 10 steps Table | 5 calculations C open Calculate >> |
| | Temperature |
| FactSage 7.3 w:\MSE302\Exercise\ | Equil |

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Results: plot the amounts of major species

Plot Species Selection - Equilib Results: mole vs Alpha P

| File | Sho | w Select | | | | | | | |
|------|--------------------------------------|----------------|------------|---------------------|----------------|----------------|----------------|----------------|------------------|
| + | \checkmark | gas phase | | Mole (max) | Fraction (min) | Fraction (max) | Activity (min) | Activity (max) | A |
| | | aqueous specie | | | | | | | |
| | _ | aqueous specie | | 6.7206E-26 | 4.2895E-26 | 4.5121E-26 | 4.2895E-26 | 4.5121E-26 | |
| | \sim | pure liquids | | 0.564 | 0.359984 | 0.398307 | 0.359984 | 0.398307 | |
| | \checkmark | pure solids | | 4.2531E-29 | 2.5807E-29 | 3.0036E-29 | 2.5807E-29 | 3.0036E-29 | |
| | 1 | | | 5.5443E-17 | 2.8856E-21 | 3.5387E-17 | 2.8856E-21 | 3.5387E-17 | |
| | * | 3010110143 | | 5.4456E-10 | 2.3112E-18 | 3.4758E-10 | 2.3112E-18 | 3.4758E-10 | |
| | | ELEMENTS | | 7.2709E-27 | 2.5163E-39 | 4.6408E-27 | 2.5163E-39 | 4.6408E-27 | |
| | | | | 3.1263E-10 | 1.7116E-14 | 1.9954E-10 | 1.7116E-14 | 1.9954E-10 | |
| | | A.II. | | 1.6598E-14 | 9.5586E-19 | 1.0594E-14 | 9.5586E-19 | 1.0594E-14 | |
| | | All | | 1.8696E-15 | 8.3464E-24 | 1.1933E-15 | 8.3464E-24 | 1.1933E-15 | |
| | | Clear | | 3 9870E-27 | 1 4514E-39 | 2 5448E-27 | 1 4514E-39 | 2.5448E-27 | |
| | 11 | It is sug | acted th | at ELEN | IENTS not | ho chown | Mo E-42 | 2.7852E-30 | |
| | It is suggested that ELEMEN IS not t | | De Shown. | vve _{E-52} | 3.8960E-36 | | | | |
| | 13 | want to | nlot the | snecies i | not elemen | te | E-64 | 5.3442E-44 | |
| | 14 | want to | plot the | species | | | E-09 | 7.2154E-07 | |
| | 15 | CI2 | 2.4340E-08 | 4.1771E-04 | 1.7189E-08 | 2.6661E-04 | 1.7189E-08 | 2.6661E-04 | |
| | 16 | CIO | 1.1542E-18 | 1.9504E-12 | 8.1510E-19 | 1.2449E-12 | 8.1510E-19 | 1.2449E-12 | |
| | 17 | CI02 | 1 7585E-31 | 3 6443E-21 | 1 2419E-31 | 2 3260E-21 | 1 2419E-31 | 2 3260E-21 | • |
| | | | | Dis | play Mass | Order | Select T | op 15 🔺 1 | species selected |

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Х

Results: plot the amounts of major species

| Plot Species Selection - Equilib Results: mole vs Alpha Doubl | | | | | Double left c | lick to sor | rt the speci | es. × | |
|--|---|---|------------|------------|----------------|----------------|----------------|----------------|---------|
| File | File Show Select | | | | | | | | |
| + | # | Species | Mole (min) | Mole (max) | Fraction (min) | Fraction (max) | Activity (min) | Activity (max) | |
| | 77 | CI_GAS | 2.8044 | 4 | 0.58613 | 0.651791 | 0 | 0 | |
| | 74 | GAS | 1.416 | 1.5667 | 0 | 0 | 1 | 1 | |
| | 79 | N_GAS | 1.128 | 1.128 | 0.183805 | 0.235757 | 0 | 0 | |
| | 75 | Sn_GAS | 0.85 | 0.973187 | 0.157411 | 0.177654 | 0 | 0 | |
| + | 41 | SnCl4 | 0.549816 | 0.973153 | 0.38829 | 0.621135 | 0.38829 | 0.621135 | |
| + | 66 | FeCl2 | 0 | 0.597804 | 0 | 0 | 0.434254 | 1 | |
| | 2 | N2 | 0.564 | 0.564 | 0.359984 | 0.398307 | 0.359984 | 0.398307 | |
| + | 40 | SnCl2 | 3.4256E-05 | 0.300184 | 2.1864E-05 | 0.211996 | 2.1864E-05 | 0.211996 | |
| + | 72 | SnO2 | 2.6813E-02 | 0.15 | 0 | 0 | 1 | 1 | |
| | 59 | Fe203 | 0 | 8.2125E-02 | 0 | 0 | 6.9173E-04 | 1 | |
| | 76 | Fe_GAS | 2.1963E-03 | 3.5750E-02 | 4.5903E-04 | 5.8254E-03 | 0 | 0 | |
| | 29 | FeCl3 | 3.6469E-04 | 2.1823E-02 | 2.5755E-04 | 1.3929E-02 | 2.5755E-04 | 1.3929E-02 | |
| | 31 | (FeCl3)2 | 2.0331E-06 | 6.5795E-03 | 1.4358E-06 | 4.1995E-03 | 1.4358E-06 | 4.1995E-03 | |
| | 28 | FeCli | C | . 1 | .1 | | | | |
| | 15 | 15 C12 These four species have the most significant amounts (we are | | | | | | | |
| | 30 | FR not | aonaidan | ing "N " | Chasse | thogo four a | nadiaa | | |
| | 14 C not considering N ₂ J. Choose these four species. | | | | | | | | |
| | 39 | I SnCl | | | | | | | • |
| Clear Display Mass Order Select Top 15 • 4 species selected Click on the '+' column to add or remove species. name G radii G radii <t< th=""></t<> | | | | | | | | | |

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Results: plot the amounts of major species



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Results: plot the amounts of major species



- As seen from the graph, there is a complex chemistry occurring as more exposed iron is available for reaction **without adequate oxygen** to convert it to Fe_2O_3 .
 - (i) Some Sn forms solid SnO_2 and this would represent a Sn loss since SnO_2 is not volatile and will remain with the solid waste stream.
 - (ii) Some Cl₂ is wasted by reaction with iron to form solid FeCl₂.
 - (iii) The Sn volatilization does remain "respectable" because of the formation of stannous chloride $SnCl_2$ in the gas phase.

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Part III (Process Control)

The above calculations can be used to guide the production. If significant quantities of $FeCl_2$ are detected in the outlet product stream, then this is a sign that we need to add more O_2 (i.e., air) to oxidize the metallic iron to Fe_2O_3 . The **secret** in operating this tin recovery process efficiently is to maintain the oxygen flow to keep the iron as Fe_2O_3 , but not to over-oxidize the metals, either.

Bearing this in mind, let us simulate the process in FactSage.

Note: in the actual tin recovery process, the amount of the exposed iron is unknown, and the assumption of 0.2 mol of the exposed iron for 1 mol of Sn in Part I calculation is not universally valid.

Back to the Reactants Window

| 🧔 Ec | quilib - Reactants | | | | | _ | □ × | |
|--------|--------------------|----------------------------|---------------------------|----------|---------------------|--------------|---------|----------------------------------|
| File | Edit Table Units | Data Search Data Evaluatio | n Help | | | | | |
| | i + 📰 | T(C) P(atm) E | nergy(J) Quantity(mol) Vo | l(litre) | | 111 | 🗐 🕒 🔻 | e |
| | | | | | | | | |
| 1- | 5 | | | | | | | |
| | | | | | | | | |
| | Quantity(mol) | Species | Phase | T(C) | P(total)** | Stream# | Data | |
| | 1 | Sn | solid-1 Solid(wh) | 25 | 1 | 1 | | |
| + | <a> | Fe | solid-1 bcc 🔹 | · 25 | 1 | 1 | | |
| • | 2 | CI2 | gas 🔹 | 25 | 1 | 2 | | |
| • | <0.75A> | 02 | gas 🗸 | 25 | 1 | 3 | | |
| • | | N2 | gas 🔻 | 25 | 1 | 3 | | |
| | | | |]]== | 1. | 1. | | |
| | L | For every | mol of Fe, 0.7 | 75 mo | $1 \text{ of } 0_2$ | is re | auirea | 1 to form 0.5 mol of Fe_2O_3 . |
| | | J | , | | <u>L</u> | | 1 | |
| | | | | | | | | |
| | | East arrange mail | of 0 276 m | | 'N iai | n two o | lugad | 7 |
| | | For every mor | $010_2, 3.761$ | 101 01 | N_2 IS I | ntroc | iucea. | |
| | | | | | V | Initial Cond | litions | |
| - | | | | | | | | |
| | | | Next >> | | | | | |
| FactSa | ge 7.3 Compound: | 1/14 databases Solutio | n: 0/15 databases | | | | | 1. |

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Menu Window

| 🗘 Equilib - Menu: comments | - 🗆 × | |
|-----------------------------|---|--------------|
| File Units Parameters Help | | |
| | T(C) P(atm) Energy(J) Quantity(mol) Vol(litre) | |
| Reactants (5) | | |
| Sn (25C,s1,#1 | + <a> Fe + 2 Cl2 + <0.75A> O2 + <2.82A> N2 #1) (25C,s1,#1) (25C,g,#2) (25C,g,#3) (25C,g,#3) | |
| Pro ducto | | |
| - Compound encodes | - Solution phonon | |
| Compound species | Solution prosess | <u>ide</u> . |
| 🗌 🗔 gas 🖉 ideal O real – 41 | C ideal solutions | |
| | - Pseudonums | |
| pure liquids 10 | applu Edit | |
| pure solids 22 | Volume data | |
| | assume molar volumes of | |
| | solids and liquids = 0 | |
| species: 73 | C include molar volume data | |
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| - Target | paraequilibrium & Gmin edit | |
| - none - | Legend Show 👁 all 🔿 selected Virtual species: 0 | |
| Estimate T(K): 1000 | Total Species (max 5000) 73 | |
| | species: U Select <u>Total Solutions (max 200)</u> 0 | |
| Quantity(mol): JU | Total Phases (max 1500) 33 | |
| | | |
| | | |
| <a> | Platmj V Delta H(J) V normal C normal + transitions | |
| 0.2 0.6 0.1 | 600 1 C transitions only | |
| 10 steps 🗖 Table | 5 calculations O open Calculate >> | |
| | | |
| FactSage 7.3 w:\MSE3 | 1302\Exercise\EquiTin_Recovery.DAT | |

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Save the Graph and Equilib settings: ".dat" file

Save the Graph with the name "Tin_Chlor_Part III". Also, go back to the Menu Window, save the Equilib settings as a ".dat" file.

| Save File in w:\MSE302\Exercise\Equi*.dat | × |
|---|--------|
| Enter the file number (1 - 9999) | ОК |
| or enter the file name, for example | Cancel |
| My very favorite calculation | |
| - avoid the special characters $??"^1\!\!\sim\!\!\!\infty\&:\!\!\wedge$ | |
| Tin_Recovery_Variable Fe | |

A Note on the Real-world Production

In the actual production, with the majority of Sn being recovered as $SnCl_4$ to the gas phase, Fe_2O_3 that forms on the exposed iron will become a "protective" layer. Consequently, the amount of O_2 required will be difficult to predict ahead of time, and we will need to monitor the process for free Cl_2 and $FeCl_2$ to ensure that we:

- (a) add enough chlorine we will need to keep the free Cl_2 at around 2% in the gas phase; and,
- (b) add enough air to prevent iron chlorination.

For the commercial-scale production, an effective operating strategy that has been proven successful is to monitor the **oxygen** level in the off-gas and to control the feed rates of **chlorine** and **oxygen** (in air) to match the amounts of iron and tin that are actually reacting.

The following exercise focuses on the tin chlorination process with variable **oxygen** and **chlorine**.

Exercise 1. A Small Excess of Both Chlorine and Oxygen

In the first exercise, we will supply **excess chlorine** and **oxygen** to the reactor. In doing so, we will have some oxygen that can be measured in the product stream and some excess chlorine (that we can absorb and reuse). By having a (small) excess of both the reacting gases, we ensure that there will always be a driving force for the reactions we want.

For simplicity, we shall assume chlorine and oxygen that are supplied have the same excess ratio.

Exercise 1. A Small Excess of Both Chlorine and Oxygen

| 存 Equilib - Reactants | $ \square$ \times |
|---|--|
| File Edit Table Units | We are again calculating the tin recovery based on 1 mol of Sn. |
| 1.5 | |
| | The number of moles of the exposed iron are variable. |
| Quantity(mol) | Species Phase T(C) P(total)** Stream# Data Sn solid-1 Solid(wh) Image: Solid Solid(wh) Image: Solid So |
| + <a> + <2B> + <0.75AB> + <2.821AB> | Fe To recover 1 mol of Sn as $SnCl_4$, 2 mol of Cl_2 are required. By multiplying a factor greater than 1, we are providing excess Cl_2, and the excess ratio is calculated as $(B - 1) \times 100\%$. If you need help regarding B (beta), right click to open "Help". |
| | |
| | To oxidize <a> mol of Fe to Fe_2O_3, at least <0.75A> mol of O_2 are required. If |
| | we use the same excess ratio as Cl_2 , then the number of moles of O_2 that are |
| | supplied are <0.75AB>. |
| | ✓ Initial Conditions |
| | For every mole of O_2 introduced, 3.76 mol of N_2 is introduced. |
| FactSage 7.3 Compound: | 1/14 databases Solution: 0/15 databases |
| ractoage r.o compound. | 68 |

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Exercise 1. A Small Excess of Both Chlorine and Oxygen

| 存 Equilib - Menu: comments | - 🗆 X |
|--|---|
| File Units Parameters Help | |
| T(C) P(atm) Energy(J) Quantity(mol) Vol(litre) | 🕂 🖳 🔁 🐨 |
| Reactants (5) | |
| Sn + <a> Fe + <2B> Cl2 + <0.75AB> O2 + (25C,s1,#1) (25C,s1,#1) (25C,g,#2) (25C,g,#3) | <2.821AB> N2 (25C,g,#3) |
| Products | |
| Compound species Figas I ideal C real 41 | Custom Solutions O fixed activities Details Details Details Details Details Details |
| pure liquids 10 | apply Edit |
| + pure solids 22 | Volume data |
| | 🧐 antida and liquida – O |
| We are considering the effect of | the amount of the iron that is reacting. |
| | J_ paraequilibrium & Limin _edit |
| Estimate T(K): 1000 A small excess ratio (~10% | %) is used for both the input chlorine and oxygen. |
| Quantity(mol): 0 solutions: 0 | <u>Total Phases (max 1500)</u> 33 |
| Final Conditions | Equilibrium |
| | • normal • normal + transitions |
| 10 steps Table 5 calculations | |
| | |
| FactSage 7.3 w:\MSE302\Exercise\EquiTin R We are conside | ring the process at 500 °C. |
| | |

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Exercise 1. A Small Excess of Both Chlorine and Oxygen

After the calculation, plot the total amount of Sn in the gas phase. For varying amounts of iron reacting, is the recovery of Sn efficient? What are the levels of oxygen and chlorine in the off-gas?

Exercise 2. Adding Too Much Air

In the second exercise, we will consider the situation if the process is out of control and too much air is introduced to the reactor.

We will consider the fixed amount of the exposed iron: for 1 mol of Sn, 0.2 mol of the exposed iron. For the input chlorine, the excess ratio is set as 10%.

Let us vary the amount of oxygen supplied.

Exercise 2. Adding Too Much Air

| 存 Equilib - Reactants | - 🗆 X |
|------------------------------|--|
| File Edit Table Units | We are again calculating the tin recovery based on 1 mol of Sn. |
| 1.5 | The number of moles of the exposed iron are 0.2. |
| Quantity(mol) 1 + 0.2 + (20) | Species Phase T(C) P(total)** Stream# Data Sn solid-1 Solid-1 Solid-1 I I Fe solid-1 bcc 25 I I |
| + <0.15A> + <0.564A | Excess Cl_2 is supplied, will be set as 1.1 (Menu Window) to give 10% excess ratio. |
| | To oxidize 0.2 mol of Fe to Fe_2O_3 , at least 0.15 mol of O_2 are required. If excess O_2 are supplied, a factor, <a>, greater than 1, is multiplied. The excess ratio of O_2 is then $(A - 1) \times 100\%$. |
| | For every mole of O_2 introduced, 3.76 mol of N_2 is introduced. |
| FactSage 7.3 Compound | Next >> 1/14 databases 0/15 databases 72 |

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Exercise 2. Adding Too Much Air

| 存 Equilib - Menu: comments | – 🗆 X |
|--|--|
| File Units Parameters Help | |
| T(C) P(atm) Energy(J) Quantity(mol) Vol(litre) | 111 💷 🔁 |
| Sn + 0.2 Fe + <28> Cl2 + <0.15A> 0.2 + <0.564/ | A> N2 g.#3) |
| Products Compound species + gas • ideal • real 41 aqueous 0 + pure liquids 10 | Custom Solutions 0 fixed activities Details 0 ideal solutions Pseudonyms apply Edit |
| The excess ratio of O ₂ is between 0 to from 1 to 2. | o 100%, which means <a> varies |
| Target - none - none <th>paraequilibrium & Gmin edit S used for the input chlorine. Total Phases (max 1500) 33</th> | paraequilibrium & Gmin edit S used for the input chlorine. Total Phases (max 1500) 33 |
| Final Chaditions Equilibrium <a> T(C) P(atm) Delta H(J) • n | arilibrium Inormal - transitions Inormal - t |
| FactSage 7.3 We are considering | the process at 500 °C. |

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Exercise 2. Adding Too Much Air

After the calculation, plot the number of moles of $SnCl_4(g)$, $Cl_2(g)$, $Fe_2O_3(s)$ and $SnO_2(s)$ against <A>. With increasing the excess oxygen supplied, is Sn efficiently recovered to the gas stream? Why?

Also, plot the mole fraction of oxygen in the off-gas against <A>. If the oxygen level in the off-gas is measured and it reaches ~150 ppm, you would know to cut back on the air feed to the reactor. This means that it would be possible, at least in principle, to use an oxygen analyzer to drive an air flow control valve.

Note that the partial pressure of oxygen does not rise very steeply with excess air, because it is "buffered" by the formation of SnO_2 . The formation of SnO_2 means that less chlorine is used for chlorination of Sn so that chlorine will rise in tandem with oxygen, and the chlorine is present at much higher concentrations (please plot the mole fraction of chlorine in the off-gas against <A>).

Exercise 2. Adding Too Much Air

In an actual process, the excess Cl_2 supplied to the reactor would result in the presence of free Cl_2 in the off-gas. It would be necessary to keep the free Cl_2 in the off-gas in a range of 11~20 vol.%, or even higher, to provide the driving force for the chlorination process. This requires a careful control of the addition rate of chlorine. The free Cl_2 in the off-gas can be recovered and recycled.

Exercise 3. Changing the Amounts of Both Chlorine and Iron to the Reactor In the third exercise, we will be looking at the effects of the varying amounts of both Cl_2 and the exposed iron that reacts on the chlorination process. This can be done by setting the amounts of Cl_2 and iron as variables (next page). Note: when is used, the calculations are repeated for each value.

Exercise 3. Changing the Amounts of Both Chlorine and Iron to the Reactor

| 存 Equilib - Reactants | - 🗆 X |
|------------------------------------|---|
| File Edit Table Units | We are again calculating the tin recovery based on 1 mol of Sn. |
| 1.5 | The number of moles of the exposed iron are variable . |
| Quantity(mol) | Species Phase T(C) P(total)** Stream# Data Sn solid-1 Solid(wh) 25 1 1 Fe solid-1 bcc 25 1 1 |
| + <2A> + <0.825B> + <3.102B> | Different levels of input Cl_2 are tested by changing $\langle A \rangle$: $A = 1$ means stoichiometric addition of Cl_2 . |
| | To oxidize $\langle B \rangle$ mol of Fe to Fe ₂ O ₃ , at least $\langle 0.75B \rangle$ mol of O ₂ are required. If we assume the excess rate of O ₂ is 10%, then $\langle 0.825B \rangle$ mol of O ₂ are added. |
| Ļ | For every mole of O_2 introduced, 3.76 mol of N_2 is introduced. |
| EastErge 7.2 Concernent | I 1/14 databases Solution: 0/15 databases |
| r accolage 7.5 Compound. | 77 |

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Exercise 3. Changing the Amounts of Both Chlorine and Iron to the Reactor

| 存 Equilib - Menu: comments | | _ | | × | | | |
|--|--|--|-----------------------------|-------|---------|---------|--------|
| File Units Parameters Help | | | | | | | |
| | T(C) P(atm) Energy(J) Quantity(mol) Vol(litre) | 11 | 1 🖳 🕒 | * | | | |
| Reactants (5) | | | | | | | |
| Sn + (25C,s1,#1) | <pre></pre> | 3> N2 1,#3) | | | | | |
| Products | | | | | | | |
| Compound species | -Solution phases | Custom Solution 0 fixed activitie 0 ideal solution Pseudonyms | s Details is Edit | | | | |
| + pure solids + pure solids Specie: Cl ₂ (i | over the range from under-supple., $A > 1$). | y of Cl ₂ | (i.e., | A < | 1) to o | ver-sup | ply of |
| | | paraequilibrium | n & Grmin ∈e | edit | | | |
| - none - Estimate T(K): 1000 | For every mole of Sn recovered | , <mark>0.2</mark> mo | ol of F | e rea | acts. | | |
| Quantity(mol): | solutions: 0 | ital Phases (max | : 1500) | 33 | | | |
| Characteristics <a> 0.8 2 0.2 0.2 10 steps | T(C) P(atm) Delta H(J) € qui 500 1 C tra | librium rmal C nor nsitions only en C. | mal + transit alculate > | ions | | | |
| FactSage 7.3 w:\MSE30 | I2\Exercise\EquiTin_R, We are considering | the pro | cess a | t 50 | 0 °C. | | |

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Exercise 3. Changing the Amounts of Both Chlorine and Iron to the Reactor

| 存 Equilib - Menu: comments | | — | × |
|---|---|---|---------------------------------------|
| File Units Parameters Help | | | |
| | T(C) P(atm) Energy(J) Quantity(mol) Vol(litre) | 111 🔛 🖻 | · · · · · · · · · · · · · · · · · · · |
| Reactants (5) | + Fe + <2A> Cl2 + <0.825B> O2 + (25C,s1,#1) (25C,g,#2) (25C,g,#3) | <3.102B> N2 (25C,g,#3) | |
| Products Compound species + gas ● ideal ○ real 41 aqueous 0 + pure liquids 10 | -Solution phases | Custom Solutions O fixed activities Details O ideal solutions Pseudonyms apply Edit | s |
| specie Cl ₂ (i | over the range from under-su.e., $A > 1$). | upply of Cl ₂ (i.e., | A < 1) to over-supply of |
| | | 📃 🔲 paraequilibrium & Gmin | edit |
| - none - Estimate T(K): 1000 | For every mole of Sn recove | ered, 0.6 mol of F | Fe reacts. |
| Quantity(mol): 0 | solutions: 0 | Total Phases (max 1500) | 33 |
| Final Conditions <a> 0.8 2 0.2 0.6 10 steps Table | T(C) P(atm) ▼ Delta H(J) ▼ 500 1 | Equilibrium Image: marked strength of the strengt | sitions >> |
| FactSage 7.3 w:\MSE3 | D2\Exercise\EquiTin_R We are consider | ing the process a | at 500 °C. |

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Exercise 3. Changing the Amounts of Both Chlorine and Iron to the Reactor

After each calculation with different , plot the levels of oxygen and chlorine in the off-gas (e.g., mol fraction) against <A>.

Save the three graphs and use the Figure Module to superimpose them. Make sure you use different line types so that the conditions can be differentiated.

- (a) From the superimposed graph, can you see the correlation between the oxygen level in the off-gas and the chlorine supplied to the reactor?
- (b) Can you suggest proper operating conditions (i.e., <A> and values) based on the total Sn recovered to the gas phase?
- (c) Given B = 2, if we wish to increase the recovery of Sn to the gas phase, should we increase or decrease the excess rate of O_2 ?

Final Thought

You need to be aware that all the above calculations that have been performed using FactSage are equilibrium calculations. The real process may behave differently, because of kinetics. The oxidation of metals is one of the very important chemical reactions. Take the oxidation of iron for example. The species that may exist at equilibrium include metallic iron (bcc, fcc) and various types of iron oxides. The thermodynamic data for metallic iron are stored in FactPS, and the data for oxides can be found in both FactPS and FToxid. (You should use the View Data Module to check the Compounds and Solutions for the Fe-O system)

Reminder: when multiple thermodynamic databases are selected, special care must be taken so that the same compound is selected only once.

For iron oxides, iron can take the oxidation state of Fe^{2+} and Fe^{3+} . To aid your understanding, we can view Fe^{2+} and Fe^{3+} as two separate species. The relative amounts of Fe^{2+} and Fe^{3+} depend on the oxygen potential (i.e., oxygen partial pressure). Therefore, when calculating the equilibrium involving the metal oxides with different oxidation states, the oxygen partial pressure, P_{0_2} , must be specified. The input amount of the gas component will be automatically adjusted so that the desired P_{0_2} is met.

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Let us study the oxidation of iron by looking at the dependence of the oxidation state of iron on the oxygen partial pressure. We will adjust P_{O_2} and see what iron oxide is stable. We will fix the temperature at 1400 °C, the pressure at 1 atm.

Reactants Window

| 存 Equilib - Reactants | - 🗆 X |
|--|--|
| File Edit Table Units Data Search Data Evaluation Help T(C) P(atm) Energy(J) Quantity(mol) Vol(litre) Don't forget the Directory. Select the | e units. |
| Quantity(mol) Species Phase T(C) 1 Fe • 0 | P(total)** Stream# Data 1 2 |
| We will oxidize 1 mole of iron. For the quant automatically adjusted when we define P_{0_2} contains oxygen). | ntity of O_2 , we set the value to 0 since it will be Q_2 (we only need to tell FactSage that the system |
| We don't need to check "Initial Conditions" because we are not calculating the changes in the thermodynamic properties. | T Initial Conditions |
| Next >> FactSage 7.3 Compound: 1/14 databases Solution: 0/15 databases | 84 |

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Reactants Window: Database(s)

| 🕞 Equi | lib - Reactants | $ \Box$ \times | |
|---------|--|---|----------|
| File Ed | it Table Unit | ts Data Search Data Evaluation Help | |
| | Data Search | | |
| FactSa | - Databases - Cact FactPS Froxid FTsalt FTsalt FTsalt FThall FTOxCN FTfitz FThelg FTpulp FTIite - Information Compound: C: FTlite - FACT Solution: C:\Fa - FTlite - FACT Solution: C:\Fa | FactSes Selected because we need to consider O ₂ (g). FToxid contains models for some solid solutions of iron oxide, for example spinel and wustite. FTmisc contains the model for liquid Fe with limited solubility of oxygen. (Same database selection when calculating the Fe-O ₂ phase diagram.) Freder of Magaloy compounds (2019) FeedSage(FACTDATAFTIke60base.ord) Aladoy and Mg-aloy solutions (2019) Incled date compounds (2019) Incled date compounds (2019) Limits Unclude compounds (2019) Limits Incled date compounds (2019) Limits Incled date compounds (2019) Limits Incled date compounds (2019) Limits Unclude compounds (2019) Limits Incled date compounds (2019) Limits Unclude compounds (2019) Limits Unclude compounds (2019) Limits Incled date compounds (2019) Limits Unclude compounds (2010) Limits Limits Unclude compounds (2010) Limits Limits Unclude compounds (2010) Limits L | <u>۲</u> |
| | | | 85 |

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Menu Window: Set P₀₂

| 存 Equilib Menu last system | 🕼 Selection - Equilib - no results - 🛛 🚽 🗸 |
|--|--|
| File Units Parameters Help | File Edit Show Sort |
| | Selected: 5/5 GAS X denotes species excluded by default |
| Reactants (2) | + Code Spe We set P_{O_2} from 10^{-12} to $10^{-0.1}$ atm at $10^{0.1}$ atm intervals. + 1 0(g) FactPS gas + 3 03(g) 2 02(g) FactPS gas + 4 Fe(g) 2 02(g) |
| Compound species Compound species Gaueous Compound species Compound specie | Fe0(g) - clear - standard stable phase - standard stable phase - standard stable phase - dormant (metastable) phase F - formation target phase P - precipitate target phase C - cooling gas phase I deal Solution a Activity Help |
| Final Conditions | permit selection of X' species Help Suppress Duplicates Edit priority list : |
| (A) | Show Selected Select All Select/Clear Clear OK |
| 10 steps Table | 1 calculation C open Calculate >> |
| All gaseous spec | ies are selected, and |
| the ideal gas mo | del is used. |

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Menu Window: Select Pure Solids



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Menu Window: Select Solution Phases

| 存 Equilib Menu last system | − □ × Custom Solutions | × |
|--|---|---|
| File Units Parameters Help | Eixed Activ | ity: 1 Species |
| 🗅 😅 🖬 T(C) P(atm) Energy(J) Quantity(mol) Vol(litre) | 1: O2(g): | Log10(a) = -12 -0.1 0.1 (i.e. 120 values) |
| Reactants (2) | Ideal Solut | ions: 0 Phases |
| Fet 0.02 | | |
| | | ОК |
| Products | | • |
| Compound species Solution phases | Custom Solutions 1. fixed activities Details | |
| + Base-Friase Full Name + gas € ideal C real 5 + FTmisc-FeLQ Fe-lig | 0 ideal solutions | |
| aqueous 0 I FToxid-SLAGA A-Slag-liq all oxides + S | - Pseudonyms | |
| pure liquids 0 + FT oxid-SPINA A-Spinel | apply 🗖 🔄 Edit | |
| * + pure solids 5 + FToxid-MeO_A A-Monoxide | Volume data | |
| * - custom selection | solids and liquids = 0 | |
| species: 10 | include molar volume data and physical properties data | |
| | | |
| Select all the solution phases: t | wo liquid | |
| | | |
| solutions and two solid solutions | ns. <u>200</u> ⁵ | |
| | Total Phases (max 1500) 11 | |
| Final Conditions | auilibrium | |
| <a> T(C) P(atm) ▼ Product H(J) ▼ (| normal O normal + transitions | |
| 2500 1 | transitions only | |
| 10 steps Table 120 calculations C | open Calculate >> | |
| | | |
| FactSage 7.3 | | |

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Menu Window: Set Final Conditions

| Fquilib Menu last system | | – 🗆 X | |
|---|--|---|---|
| File Units Parameters Help | T(C) P(atm) Energy(J) Quantity(mol) Vol(litre) | III 🖳 🔚 💌 | |
| reactants [2] | Fe + 0 02 | | |
| Products Compound species + gas ● ideal C real 5 aqueous 0 pure liquids 0 * + pure solids 5 * - custom selection species: 10 | Solution phases * + Base-Phase Full Name + FTmisc-FeLQ Fe-liq I FToxid-SLAGA A-Slag-liq all oxides + S + FToxid-SPINA A-Spinel + FToxid-MeO_A A-Monoxide | Custom Solutions 1 fixed activities Details 0 ideal solutions Pseudonyms apply Edit Volume data • assume molar volumes of solids and liquids = 0 • include molar volume data and physical properties data | |
| - none - Estimate T(K): 1000 | Legend I - immiscible 1 + - selected 3 This option between diff | permits us to find a Ferent oxidation pro | Ill the transition temperatures oducts. |
| Quantity(mol): 0 Final Conditions (A) 10 steps Table | T(C) P(atm) Product H(J) (1400 1 120+ calculations) | Total Phases (max 1500) 11 Equilibrium Image: Contrast of the second | |
| FactSage 7.3 | idation of iron occurs at 1400 | °C. | 89 |

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Results: When $P_{0_2} = 10^{-4}$ atm



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Results: Plot the masses of oxidation products, i.e., gram~ P_{0_2} .



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Results: Plot the masses of oxidation products, i.e., gram $\sim P_{0_2}$.



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Recall we studied the **solution** properties by looking at an **isothermal mixing process** (Chapter 4.3). Now let us calculate some mixing properties using the Equilib Module.

Say we would like to mix varying amounts of liquid Pb and liquid Fe at 2500 °C and 1 atm. We assume the total amount of Pb and Fe is 1 mole.

The mixing process can be described as the following:

 $X_{\text{Pb}}\text{Pb}(l) + (1 - X_{\text{Pb}})\text{Fe}(l) \xrightarrow{2500 \text{ °C,1 atm}} 1 \text{ mole Solution}$

Reactants Window: Define Reactants

| 🗘 Equilib Reactants | | | | _ | | × |
|----------------------------|-------------------------|--------------------------------|--------------|-------------|---------------|-----|
| File Edit Table Units Data | Search Data Evaluation | Help | | | | |
| | T(C) P(atm) Ene | ergy(J) Quantity(g) Vol(litre) | | <u>111</u> | 9 | 1 |
| Don't | forget the Dir | ectory. | | | | |
| | | | | | | |
| Quantity(g) | Species | Phase T(C |) P(total)** | Stream | # Data | |
| 1 | РЬ | v | | 1 | | |
| + 1 | Fe | v | | | | |
| | | | | | _ | |
| | Sr | becies that are b | being mi | ixed. | | |
| | | | 0 | | _ | |
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| | | | | | | |
| | | | | Initial Cor | nditions | |
| | | | - | | | |
| | | Next >> | | | | |
| FactSage 7.3 Compound: 1/ | /14 databases Solution: | 1/15 databases | | | | /// |

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Reactants Window: Database(s)



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Reactants Window: Choose Units and Input the Quantity of Species

| Equilib - Reactants | - 🗆 × |
|--|---|
| File Edit Table Units Data Search Data Evaluation Help | |
| T(C) P(atm) Energy(J) Quantity(mol) | Vol(litre) |
| 1-2 | Choose the units. Use mol for quantity. |
| Quantity(mol) Species Phase (A> Pb | T(C) P(total)** Stream# Data |
| | Initial Conditions |
| Next >> | |
| FactSage 7.3 Compound: 1/14 databases Solution: 1/15 databases | |

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Reactants Window: Specify the Initial Conditions

| 存 Equilib Re | actants | | | | | | _ | × |
|-----------------|--------------|--|---|----------------------|-------------------------|--------------------------|--------------------|--------------------------|
| File Edit Tak | ole Units Da | ata Search Data Evaluatio | on Help | | | | | |
| □ 🗃 + | | T(C) P(atm) I | Energy(J) Quantity(mol) |) Vol(lii | tre) | • | | |
| 1-2 | | | | Ch | oose | the ur | nits. | |
| Qu (<a> | Jantity(mol) | Species Ph | Phase liquid | • | T(C) 2500 | P(total)** 1.0 | Stream# Dat | a |
| + <1-A> | | Fe | liquid | • | 2500 | 1.0 | 2 | |
| | L. | We are mixin B at | g liquid Pb oth liquid I : 2500 °C a: | an Pb a nd | d liq and l 1 atr | uid Fe. iquid F n. | Fe are ini | itially |
| | | ** P(total) is the hydros For a gaseous str partial pressures of | tatic pressure above th eam this is the sum of t the species in that stre | e phas he eam. | e. | | | |
| | | | | | | V | Initial Conditions | |
| | | | Next >> | | | | Che | eck "Initial Conditions" |
| FactSage 7.3 | Compound: | 1/14 databases Solutio | on: 1/15 databases | | | | | |

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Menu Window: Select Products and Define Final Conditions

| 存 Equilib 🛛 Menu last system | | – 🗆 X | | |
|--|---|---|----|--|
| File Units Parameters Help | | | | |
| | T(C) P(atm) Energy(J) Quantity(mol) Vol(litre) | 🚻 🗗 🔁 | | |
| Reactants (2) | <a> Pb + <1-A> Fe (2500C,liq,#1) (2500C,liq,#2) | | | |
| Products Compound species gas © ideal © real 0 aqueous 0 | Solution phases * Hease Full Name I FTlite-Liqu Liquid FTlite-A1 FCC-A1 | Custom Solutions 0 fixed activities Details 0 ideal solutions Pseudonyms Edit | | |
| Choose FTlite-Liqu only, and use the default [I]-option. From the Pb-Fe phase diagram (Documentation), it is seen that the immiscibility exists for liquid Pb and liquid Fe. | | | | |
| Target - none - Estimate T(K): 100 Quantity(mol): D pu | e would like to perform the c re Fe to pure Pb using the st | calculations from ep of 0.005. | | |
| Final Conditions <a> 0 1 0.005 10 steps Table FactSage 7.3 | T(C) P(atm) 		 Delta H(J) 2500 1 | Equilibrium • normal • transitions • transitions only transitions is isotherma | l. | |

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Results



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Menu Window: Select Products and Define Final Conditions

| 存 Equilib 🛛 Menu last system | | – 🗆 X | |
|---|--|---|----------------------------|
| File Units Parameters Help | | | |
| D 🚅 🖶 | T(C) P(atm) Energy(J) Quantity(mol) Vol(litre) | M 🗗 🕞 | |
| Reactants (2) | <a> Pb + <1-A> Fe (2500C,liq,#1) (2500C,liq,#2) | | |
| Products Compound species gas () ideal () real () aqueous () | -Solution phases | Custom Solutions 0 fixed activities 0 ideal solutions Pseudonyms E dit | |
| ^{pure soli} This time | , we do not consider the imr | niscibility. The single | e-phase setting is chosen. |
| species: 0 Target - none - Estimate T(K): 1000 Quantity(mol): 0 | Legend + · selected 1 species: 2 solutions: 1 | solids and ilgulds = 0 include molar volume data and physical properties data paraequilibrium & Gmin edit Virtual species: 1 <u>Total Species (max 5000)</u> 2 <u>Total Solutions (max 200)</u> 1 <u>Total Phases (max 1500)</u> 1 | |
| Final Conditions | | Equilibrium | |
| <a> 0 1 0.005 | ILU P(atm) Image: Delta H(J) 2500 1 201 calculations | rormal C normal + transitions transitions only open Calculate >> | |
| FactSage 7.3 | | | |

102

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Results: Make Plots $\Delta_{\min} g_{2500 \circ C} \sim X_{Pb}$



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103

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Results: Use the Figure Module to superimpose the two figures



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Results

Use the [I]-option for FTlite-Liqu, please plot other mixing properties

 $\Delta_{\min} h_{2500 \circ C} \sim X_{Pb}$ and $\Delta_{\min} s_{2500 \circ C} \sim X_{Pb}$.

Then, please go back to the Menu Window, and save the solution properties for FTlite-Liqu.

(It is also recommended that you use Fact-XML to plot all the solution properties)

Some general tips for the Equilib Module are summarized in a Q&A format

Q1: How to perform calculations when the mass of the reactant changes?

A1: You can use <A> or <aA + b> or <a + bA> where "a" and "b" are constants and <A> (alpha) is a variable to represent the quantities of the reactants.

Q2: How to calculate the adiabatic flame temperature?

A2: After inputting the initial temperature, you can leave the final temperature blank, and set 0 for the Enthalpy change .

Q3: I saw in the FToxid database, the slag is modeled as SLAGA, SLAGB, SLAG?, which one should I select?.

A3: On the Menu window, right click on FToxid-SLAGA, FToxid-SLAGB, FToxid-SLAG?, and then check the phase information. You should find the description which details the elements that are considered in the phase model, and then choose the model which contains the elements of interest.

Some general tips for the Equilib Module are summarized in a Q&A format

Q4: I want to perform some calculations about high-temperature treatment of solid wastes (slag, fly ash, mine tailings, municipal solid wastes...)?

A4: Sine the solid wastes are mostly high-order systems, trial-and-error calculations are required to find the optimal phase selection. If the molten oxide slag is expected, "FToxid-SLAG?" can be used for preliminary calculations; if you are interested in the chlorine behavior, you should select the FTsalt database.

Q5: How to control the oxygen partial pressure?

A5: You need to use the FactPS database. Right click on the gas (Compound species on the Menu Window), then right click on the "+" column of O_2 to set the activity which is numerally identical to partial pressure of O_2 in the ideal gas mixture. The oxygen input amount will be automatically calculated.

Some general tips for the Equilib Module are summarized in a Q&A format

Q6: How to calculate the equilibrium composition of slag by specifying the activity of the slag components?

A6: Right click on the FToxid-SLAGA, and use the [C]-option. This will permit us to specify the activity of the slag component.

Q7: How to determine the solidus temperature and liquidus temperature?

A7: Right click on the liquid phase (e.g., FTlite-Liqu), and use the [P]-option for the calculation of liquidus temperature and [F]-option for the calculation of solidus temperature. Also, you need to leave the temperature (Final Conditions) blank. However, for a complicated system, these two temperatures may not be obtained by this approach. In this case, it is suggested to activate the "normal + transitions" option, and generate the graph to find these two temperatures (We will discuss this in the advanced applications).
Some general tips for the Equilib Module are summarized in a Q&A format

Q8: What should I do if the solution model does not contain the species I want to calculate? For example, TiO_2 is not included in the FToxid-SLAG.

A8: If the amount of the species is low, we can consider using the dilute solution model. Instructions can be found in the help file (Select/Slide Show/Advanced Features).

Q9: Based on the information shown in the Documentation Module, the system I am investigating has not been optimized by any of the available FactSage databases? What should I do?

A9: Please consider building a private database for the system of interest using the assessment papers that have been published.

Some general tips for the Equilib Module are summarized in a Q&A format

Q10: I want to analyze a system containing metastable phases, for example, Fe-C system. What should I do?

A10: Do not select C(s) (Graphite), but select $Fe_3C(s)$ (Cementite), and then perform the calculation.

Q11: I am experiencing "Abort" issue (no solution) even though it is a simple problem?

A11: You can try to add a small amount of argon (e.g., 1E-6) to the list of reactants.

Question 1. Use the Equilib Module to solve the following questions.

(1) 1 mole of H_2O becomes a gas mixture at 2500 °C and 1 atm. Calculate the equilibrium partial pressure of H_2 in the gas mixture.

(2) For a gas mixture containing 2 mole of H_2O , 0.79 mole of N_2 , and 0.21 mole of O_2 , calculate at 25 °C and 1 atm the equilibrium partial pressure of H_2O .

(c) Heating of LVDS 3 (NaHCO₃) results in the formation of Na₂CO₃, CO₂, and H₂O, find the minimum temperature for this reaction.

(d) Find the Enthalpy for 1 mole of $H_2O(s)$, 1 mole of $H_2O(l)$, and 1 mole of $H_2O(g)$ when the temperature is 150 °C and the pressure is 1 atm.

(e) Find the composition and temperature of the system when 10 J of energy is supplied to 1 gram of water at 25 °C.

(f) Calculate the final temperature when 1 gram of ice (0 °C) and 2 gram of hot water (90 °C) are mixed. Assume no heat exchange with the surroundings.

Question 2. Mixing Properties

(1) Use FTlite database to calculate the Al-Mg phase diagram. $T(^{\circ}C) \sim X_{Mg}$

(2) From the diagram, you should see that at 800 °C, the system exists as liquid over the entire composition range, i.e., X_{Mg} varies from 0 to 1. Calculate and plot for the liquid phase $\Delta_{mix}g_{800 \ ^{\circ}C} \sim X_{Mg}$ and $\Delta_{mix}h_{800 \ ^{\circ}C} \sim X_{Mg}$.

(3) From the diagram, you should see that at 500 °C, the system may exists as two coexisting phases or single phase over the entire composition range. Calculate and plot the molar Gibbs energy of the system when X_{Mg} varies from 0 to 1.