

Steel composites for energy generation systems

C. Capdevila¹, J. Chao¹, M. Serrano², G. Pimentel¹,
E. Urones-Garrote³, C.M. Parish⁴ and M.K. Miller⁴

¹Centro Nacional de Investigaciones Metalúrgicas (CENIM-CSIC), Spain

²Centro Investigaciones Medioambientales y tecnológicas (CIEMAT), Spain

³Centro Nacional de Microscopía Electrónica (CNME), Spain

⁴Oak Ridge National Laboratory (ORNL), USA

Acknowledgements:

APM 2013 Conference Chair

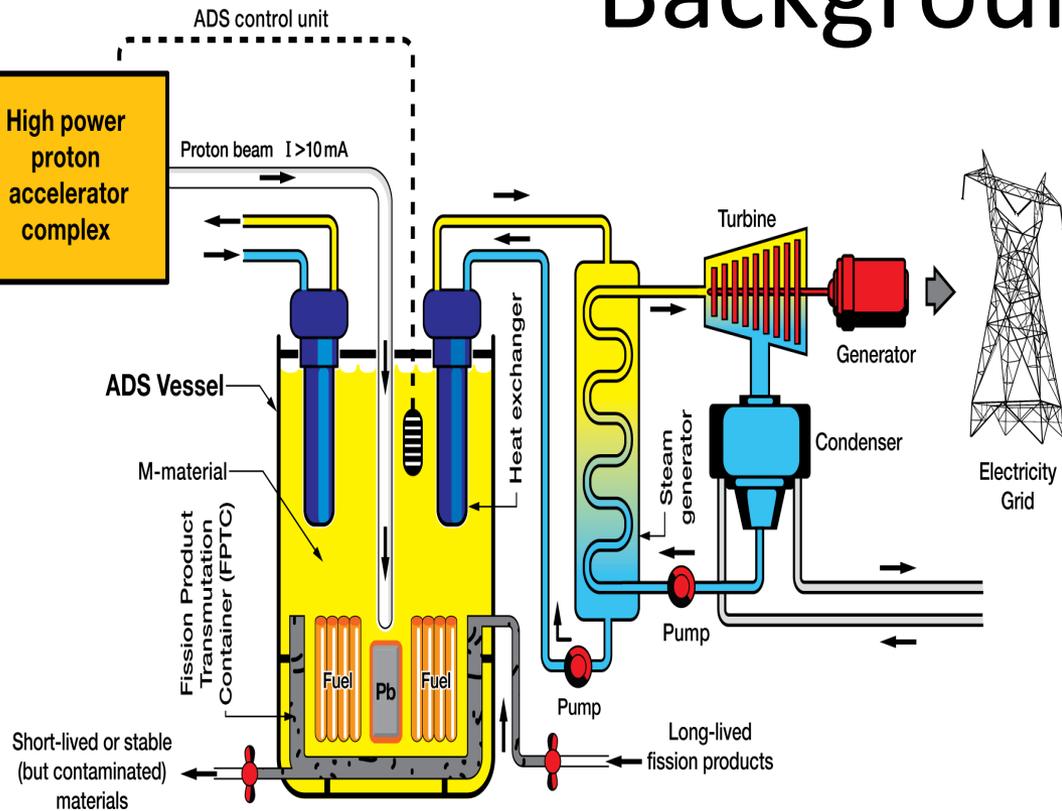
MINECO (ENE2009-13766-C04) and ORNL's Shared Research Equipment (ShaRE) User Facility, which is sponsored by the Office of Basic Energy Sciences, U.S. Department of Energy.



Background

- The need to reduce CO₂ emissions coupled with the need to increase the quantity of electricity supplied are driving to the development of new power generation systems.
- Significant gains in efficiency for power generation systems can be made by increasing the steam temperatures and pressures. This lead to an improvement of the high-temperature properties of current heat resistant alloys.
- The low creep resistance at high temperatures of Fe-base alloys could be mainly improved by different methods:
 - ❑ One method consists on a combination of composition adjustments, guided by computational thermodynamics, and thermo-mechanical control process (TMCP) optimization.
 - ❑ Second method is to strength the steel by oxide dispersion, and this line led to work on ferritic oxide dispersion-strengthened (ODS) alloys. The advantages of ODS alloys at high temperatures are clear: high strength and high creep resistance.
 - ❑ Third method consists on compositional tuning to induce the formation of nanoclusters and nanophases. An example is illustrated here.

Background



(S.R. Hashemi-Nezhad, University of Sydney, Australia)

- Fe-Cr-Al-Ti ODS alloys have promising properties where corrosion and creep resistance is paramount, i.e. beam windows in subcritical accelerator driven systems (ADS) nuclear reactors.
- Phase separation of α (Fe-rich) - α' (Cr-rich) during service affect mechanical properties.

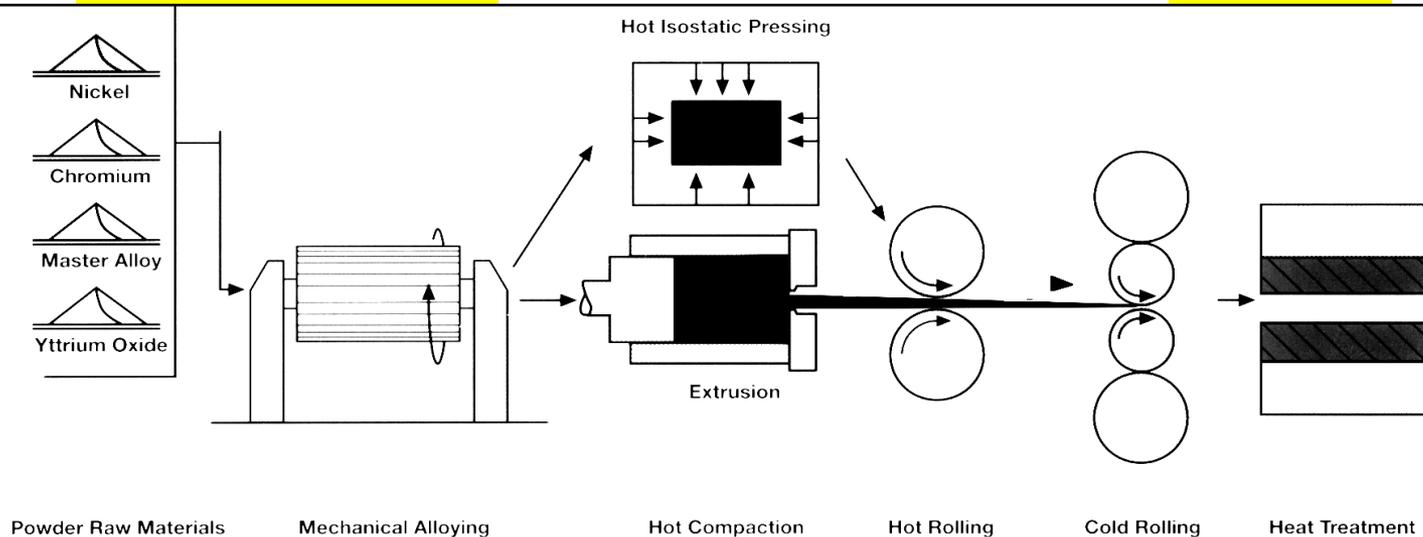
- Topics included in this presentation and its effect on phase separation:
 - Activation energy of α - α' phase separation
 - Novel nanophase formation of β' (Fe-Ti-Al precipitate)
 - Effect of elastic stress on α - α' + β' precipitation

Material

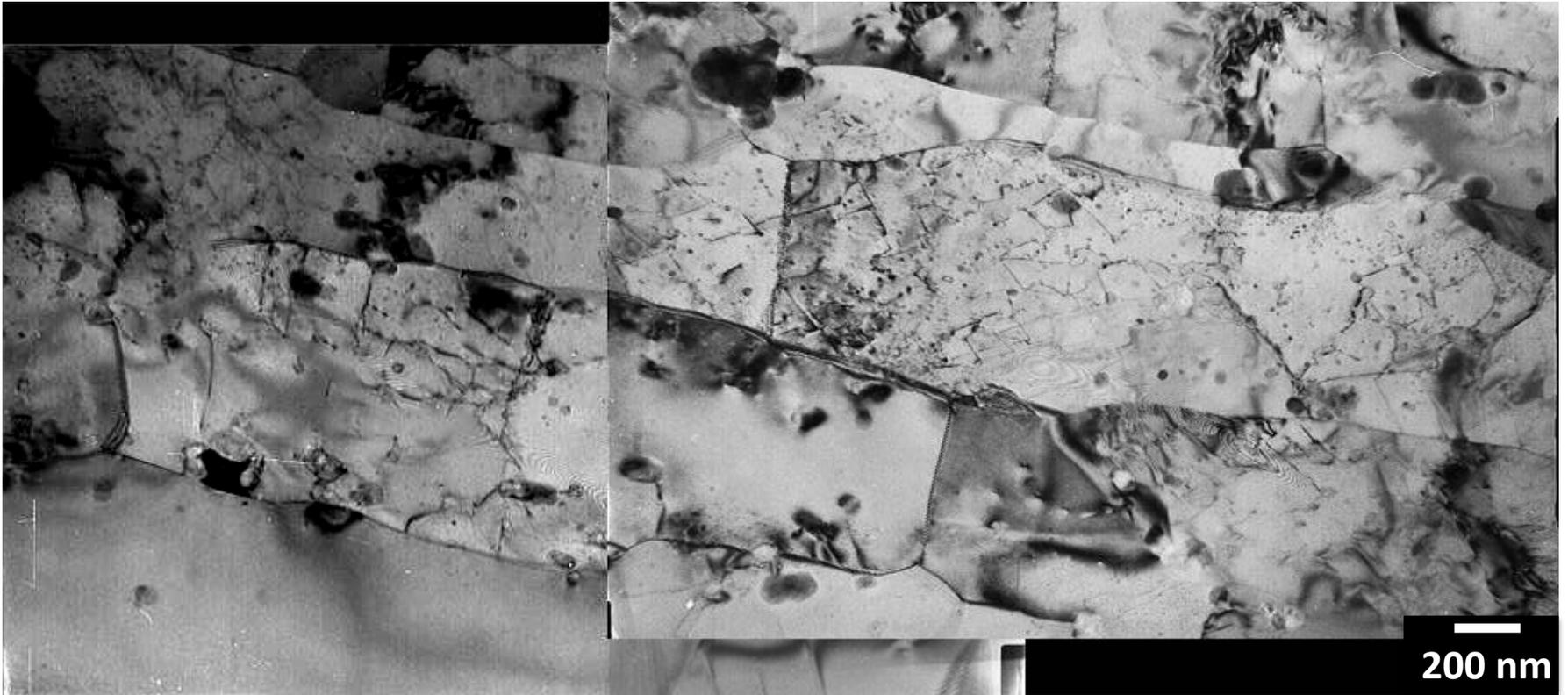
PM 2000tm is a commercial Fe-base ODS alloy manufactured by PLANSEE in Lechbruck, Germany

Chemical composition of PM 2000

	Cr	Al	C	O	N	Ti	Y
wt. %	18.6	5.5	0.04	0.09	0.006	0.54	0.39
at. %	18.5	10.5	0.17	0.28	0.022	0.58	0.23



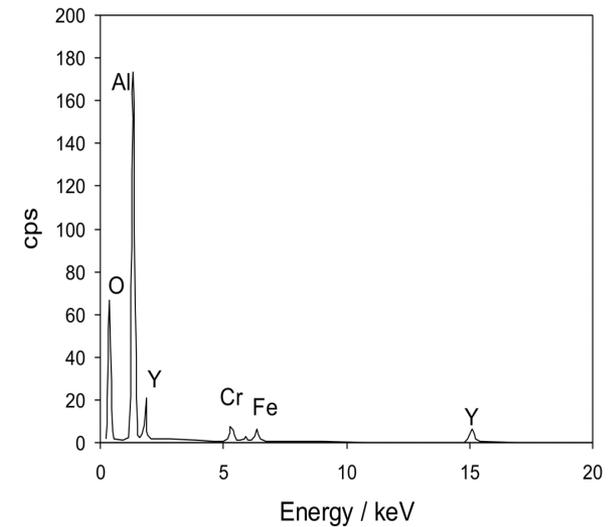
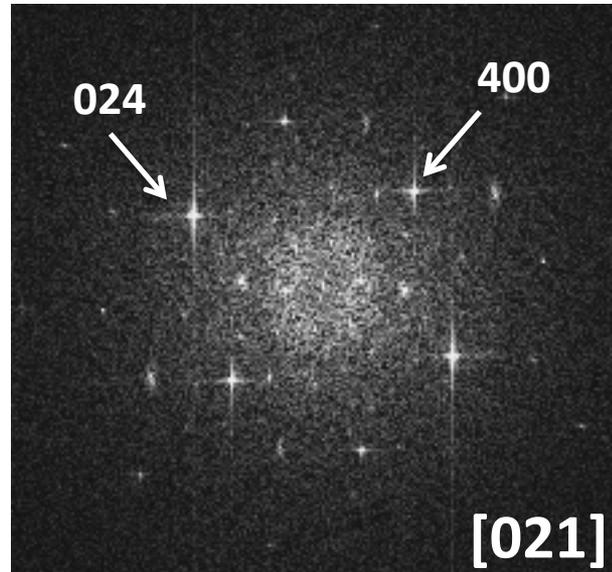
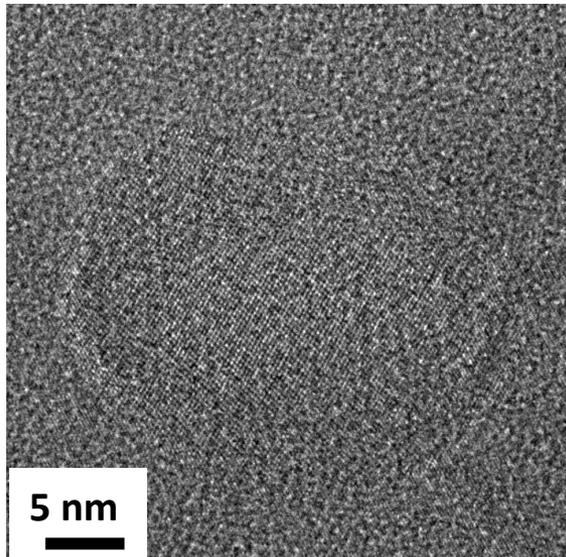
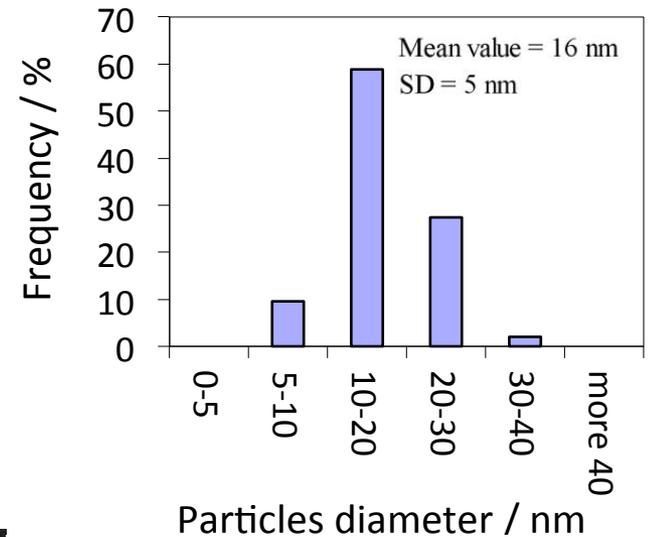
Microstructure



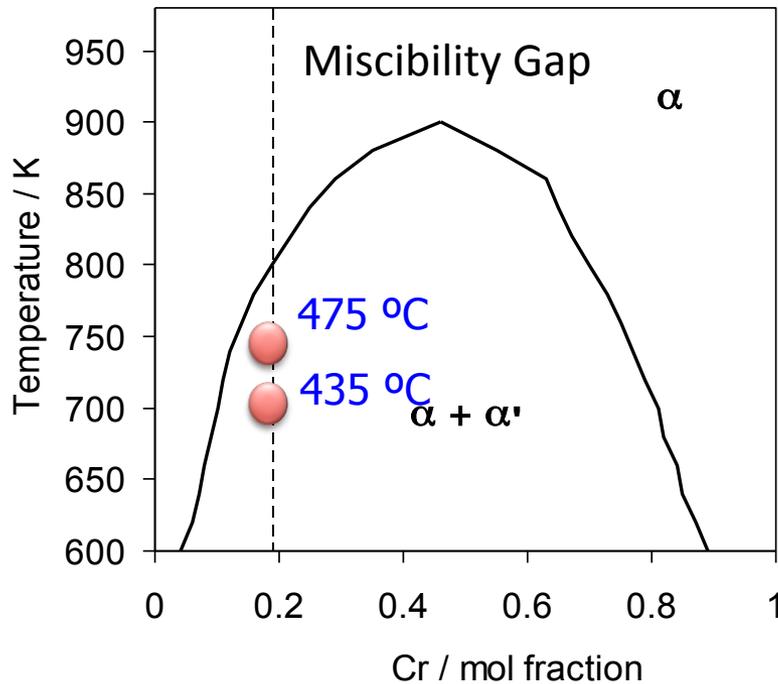
Anisotropic microstructure: Strongly textured ($\langle 110 \rangle$ || RD) elongated grains with high-dislocation density and homogenous distribution of particles

Microstructure

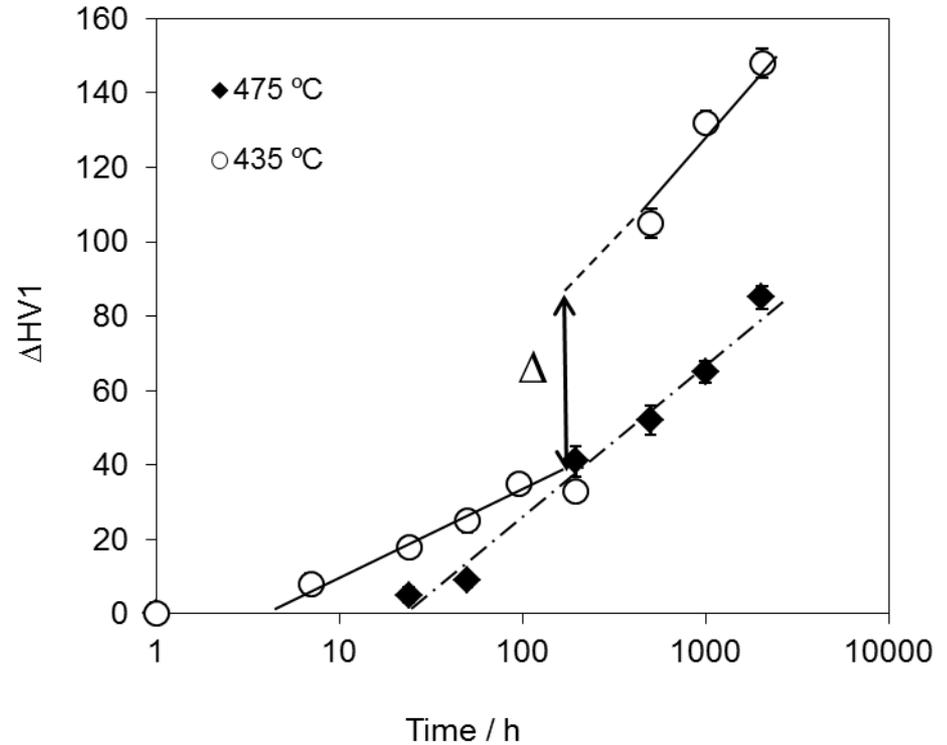
- The structure and composition of initial yttria particles is modified during mechanical alloying
- Particles in as-received condition:
 - Composition $Y_3Al_5O_{12}$ and garnet structure
 - Sizes: 3-40 nm



Hardening



- [Al]=11 at.%
- - - PM2000
- Ageing Temperature

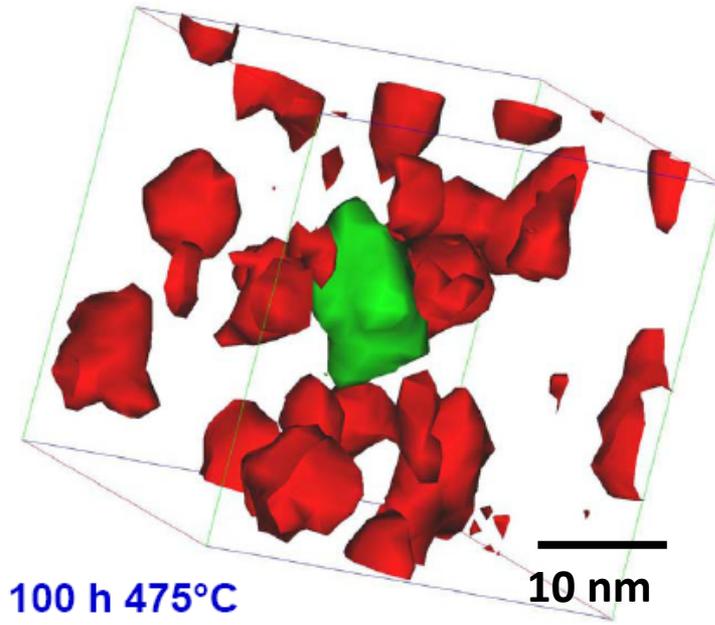


Annealing at temperatures below 500 °C induce hardening. Surprising increase at 435 °C is observed.

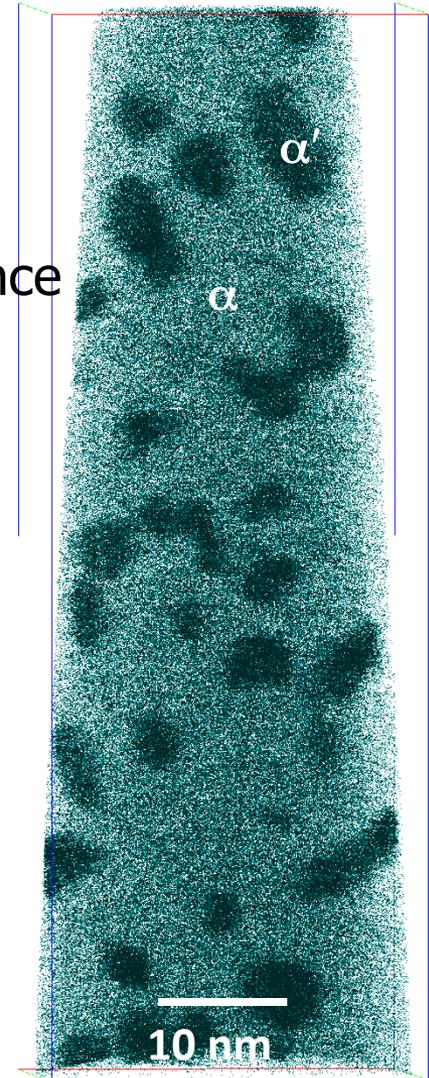
APT Results

Red 30% Cr isoconcentration surface revealing the distribution and spherical morphology of Cr-rich α' phase.

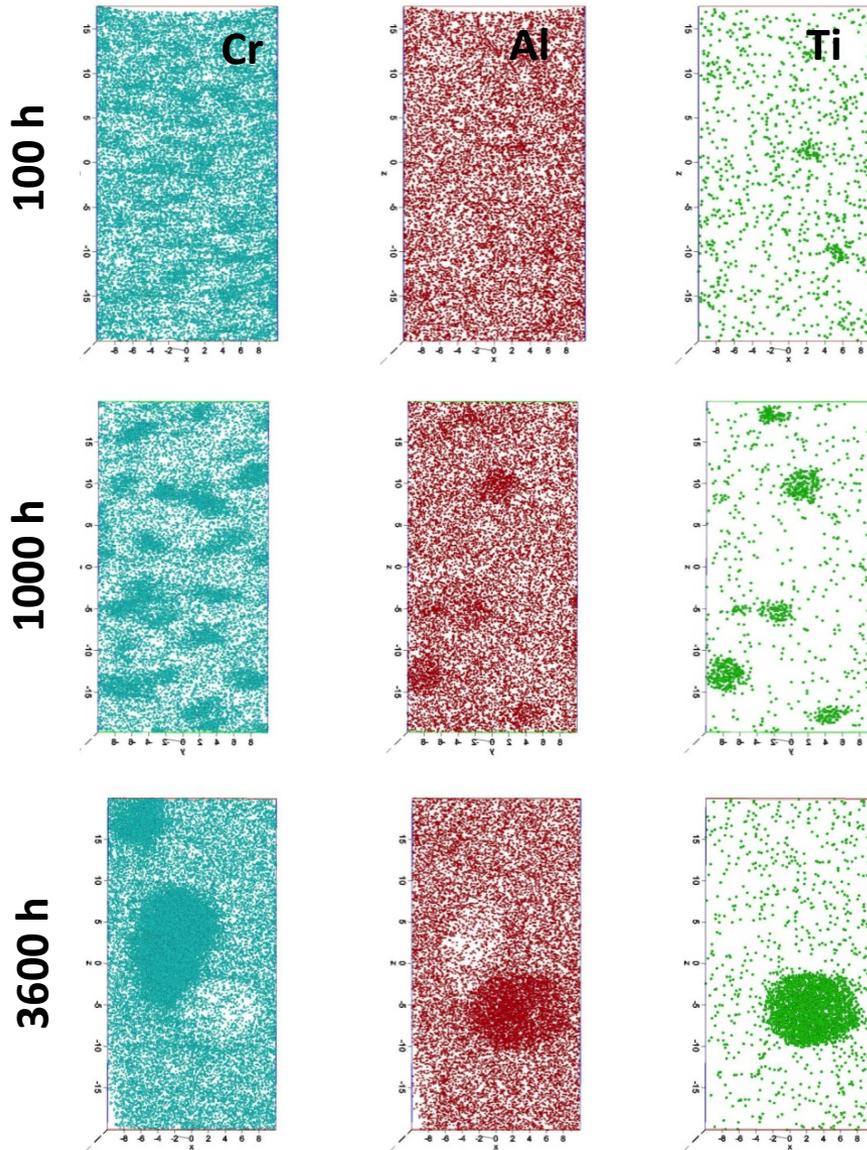
Green 5% Ti isoconcentration surface revealing the existence of 3.2 nm in diameter nanoclusters of Fe(Ti,Al) (β' phase)



Cr atom map
2040 h 475 °C



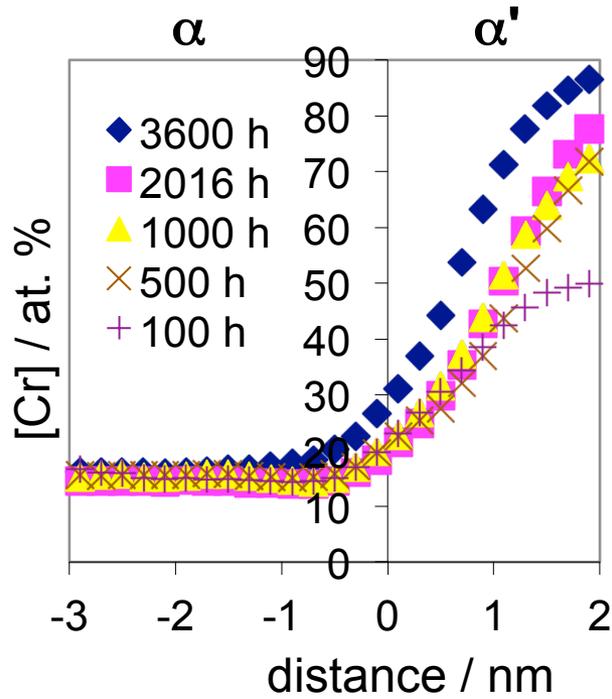
Nanoparticles at 435 °C



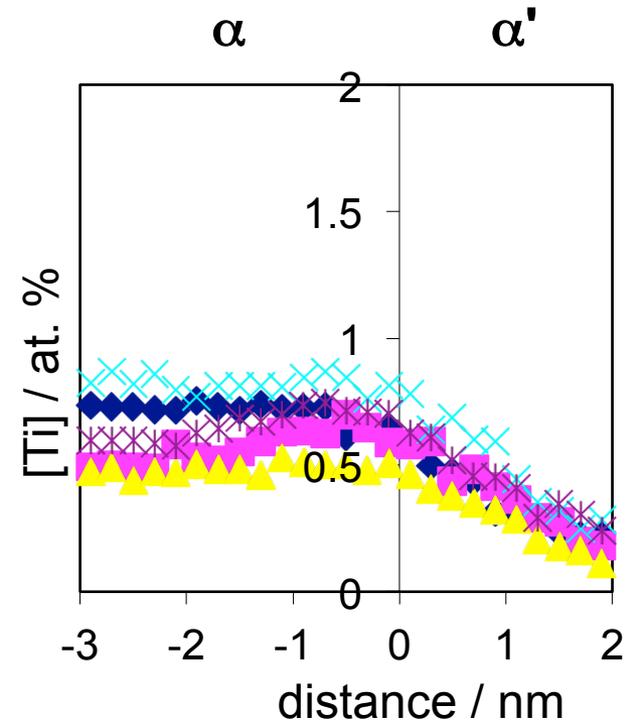
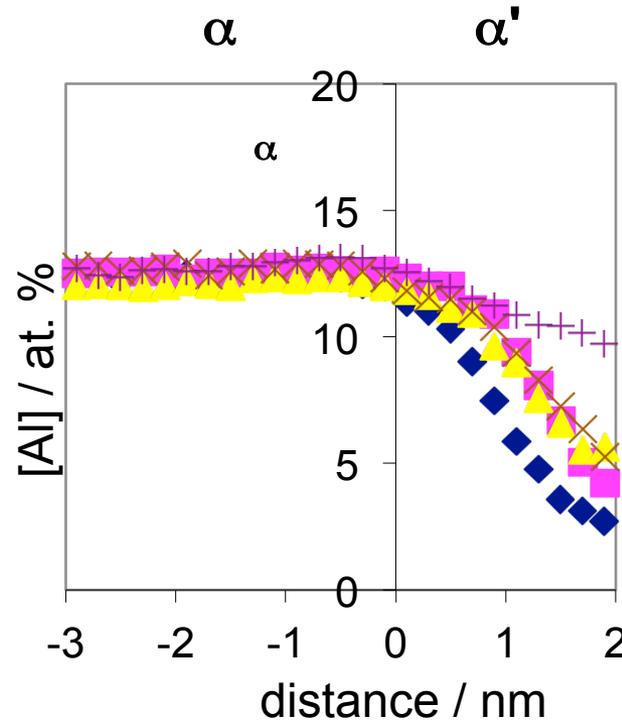
- ❑ 4-nm-thick atom maps for selected times (volume of 4×20×40 nm³)
- ❑ The Cr-enriched α' regions were found to be depleted in Al
- ❑ The phase separation is of a finer scale and is less well developed at lower ageing temperatures
- ❑ The atom maps also reveal the presence of a Ti- and Al-enriched phase (β'). This phase is present at a significantly lower number density compared to the Cr-enriched α' phase, but its number density increases at lower ageing temperatures

α' -phase composition

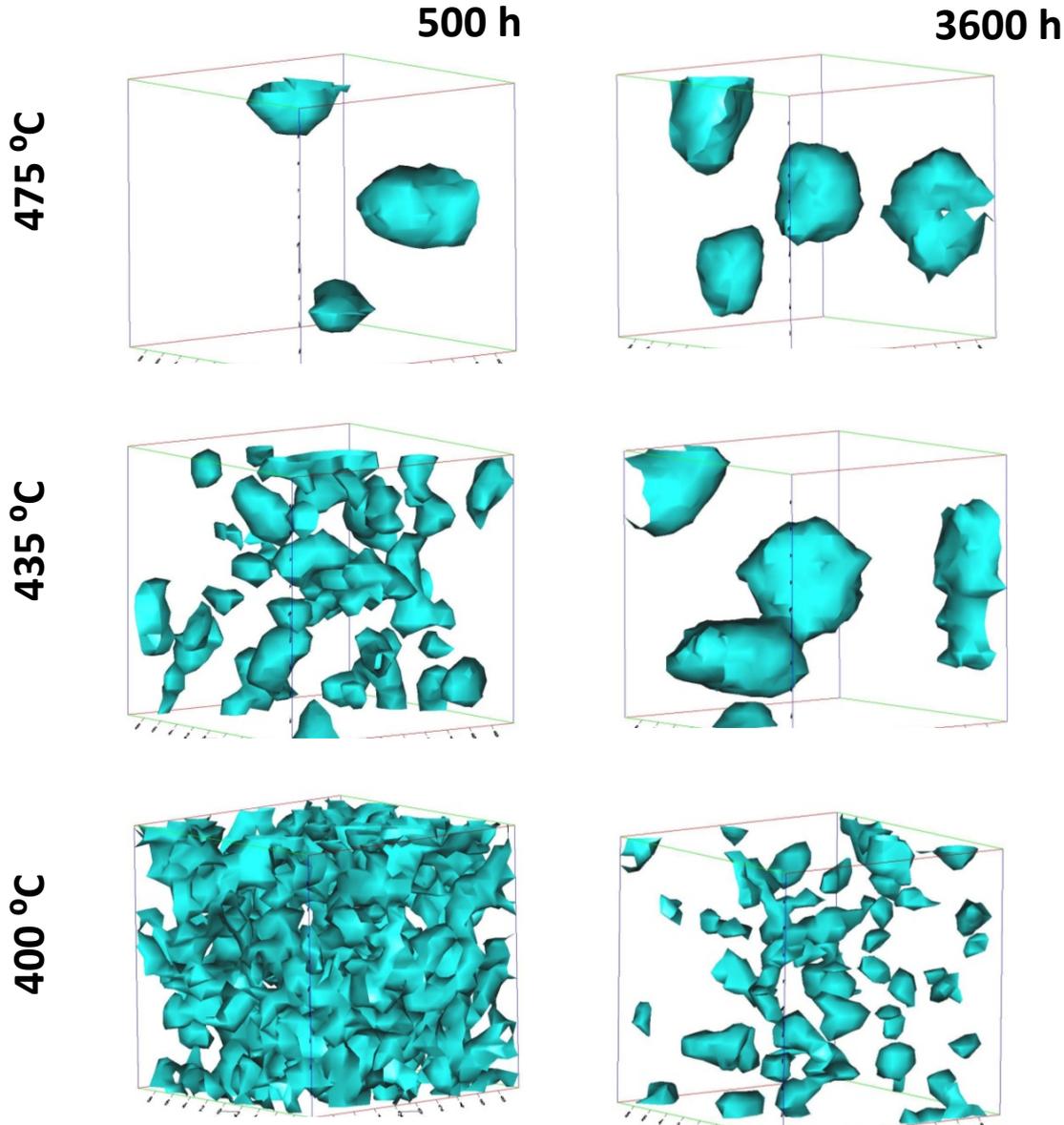
Proximity histograms analysis



475 °C



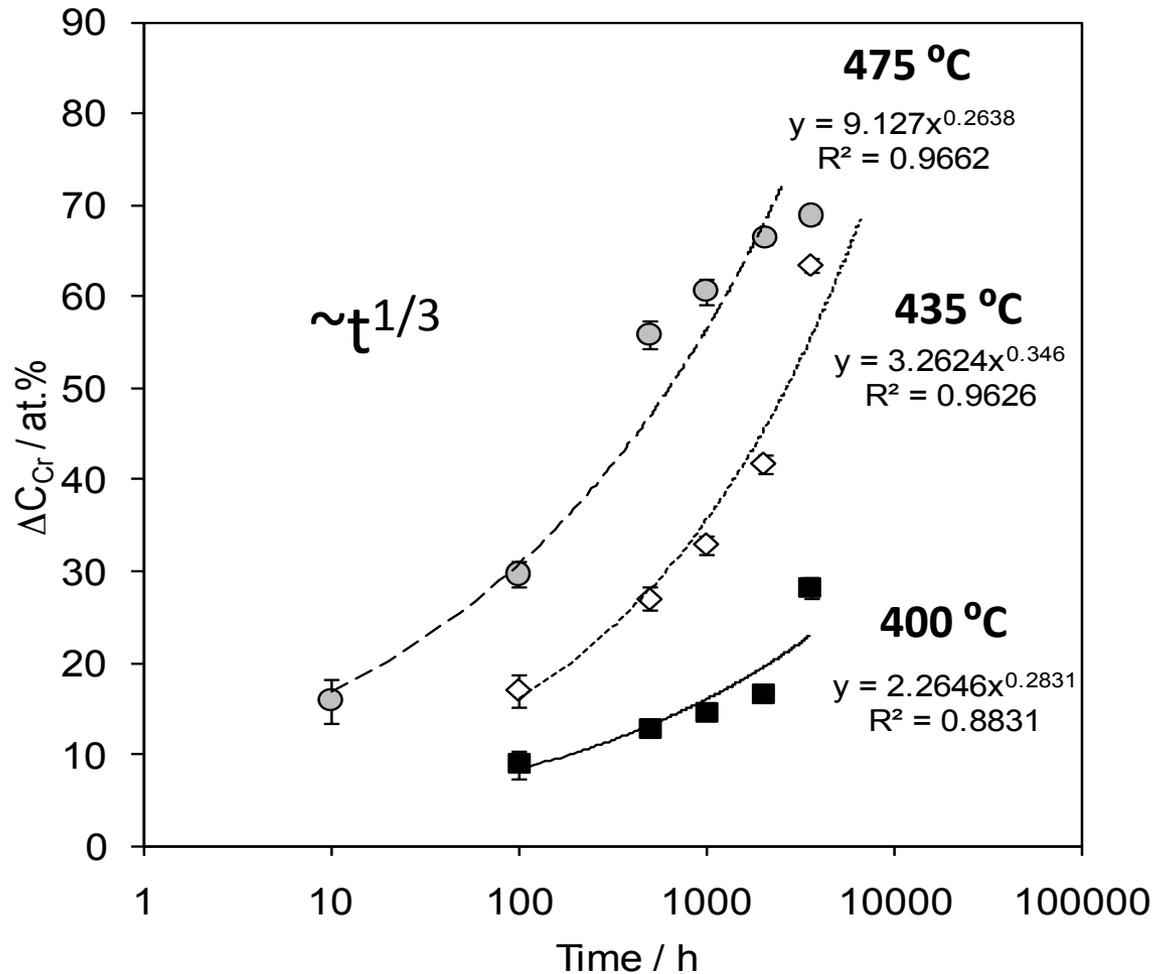
α' -phase morphology



□ The spheroidal α' particles observed at 475°C are clearly isolated and do not form a percolated microstructure

□ At the lower ageing temperatures the morphology of the Cr-enriched α' phase after 3600 h is of a finer scale and forms an interconnected network

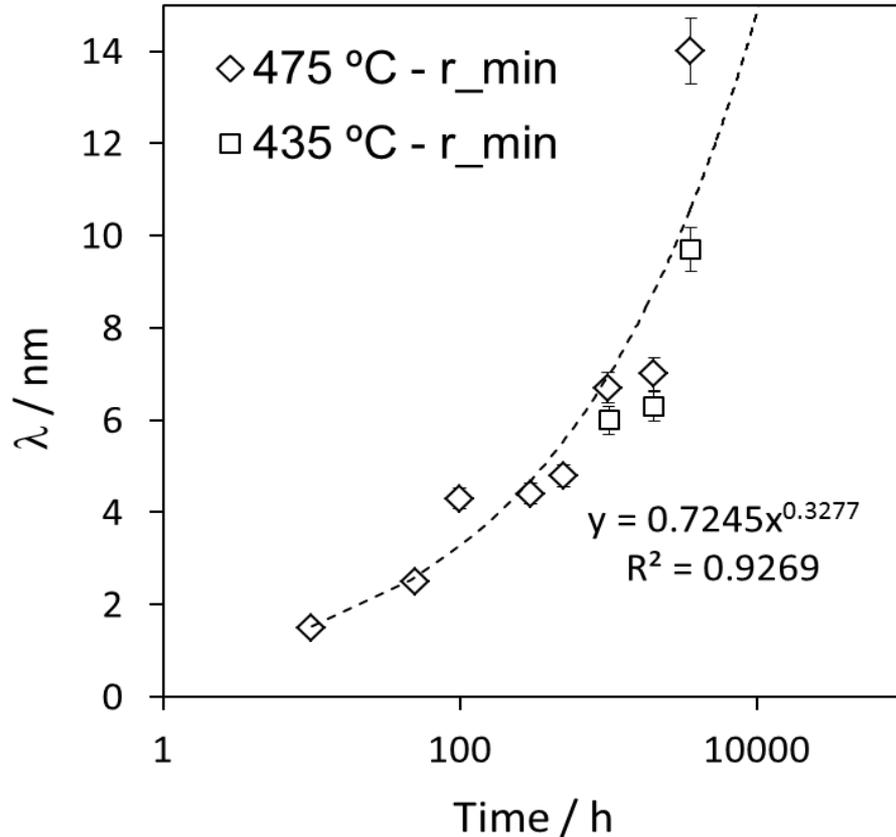
α' -phase kinetics



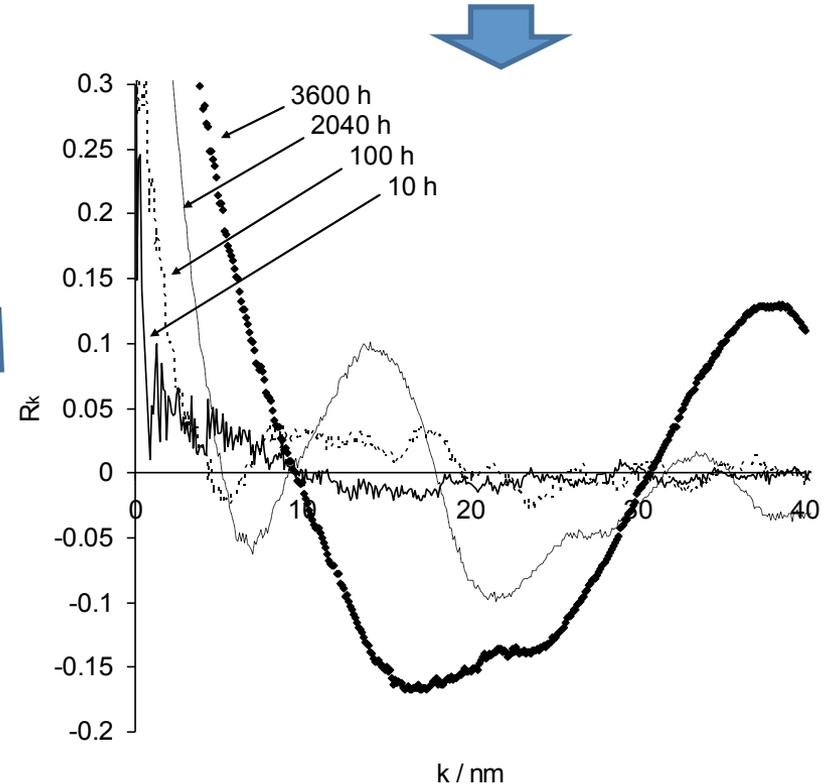
The kinetics of $\alpha - \alpha'$ phase separation process were determined from the analysis of proximity histogram

α' -phase kinetics

α' - size



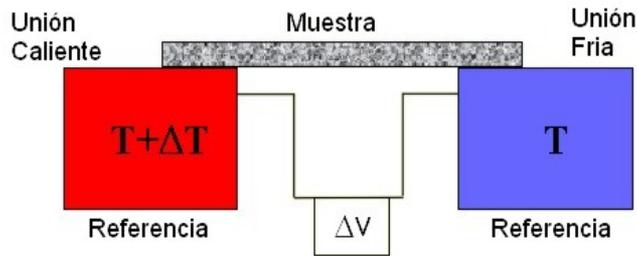
The size of the α' particles (λ) is determined by the first minima (r_{\min}) of the autocorrelation function



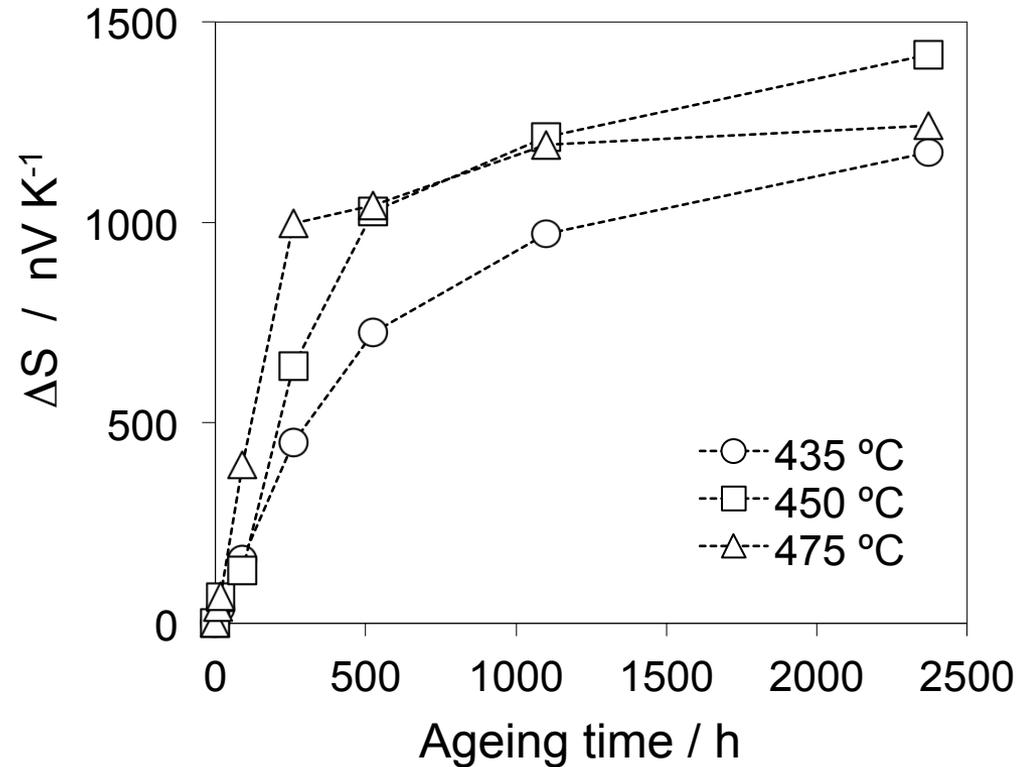
The size of the α' increases with a time exponent of ~ 0.3 which is consistent with the mean precipitate size $R(t)$ varying as $\sim t^{1/3}$ predicted by the LSW theory.

Activation energy for α' -phase

Thermoelectrical Power (TEP) measurements have been used to track microstructure evolution



$$\Delta S = \frac{\Delta V}{\Delta T} \text{ in nV/K}$$



Since volume fraction of β' is significantly lower than α' , the influence of β' on TEP is negligible.

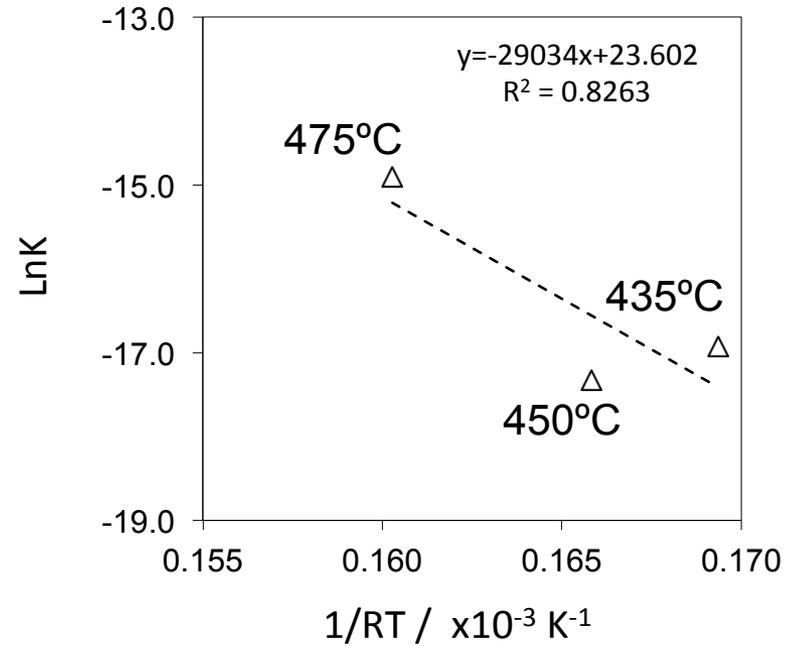
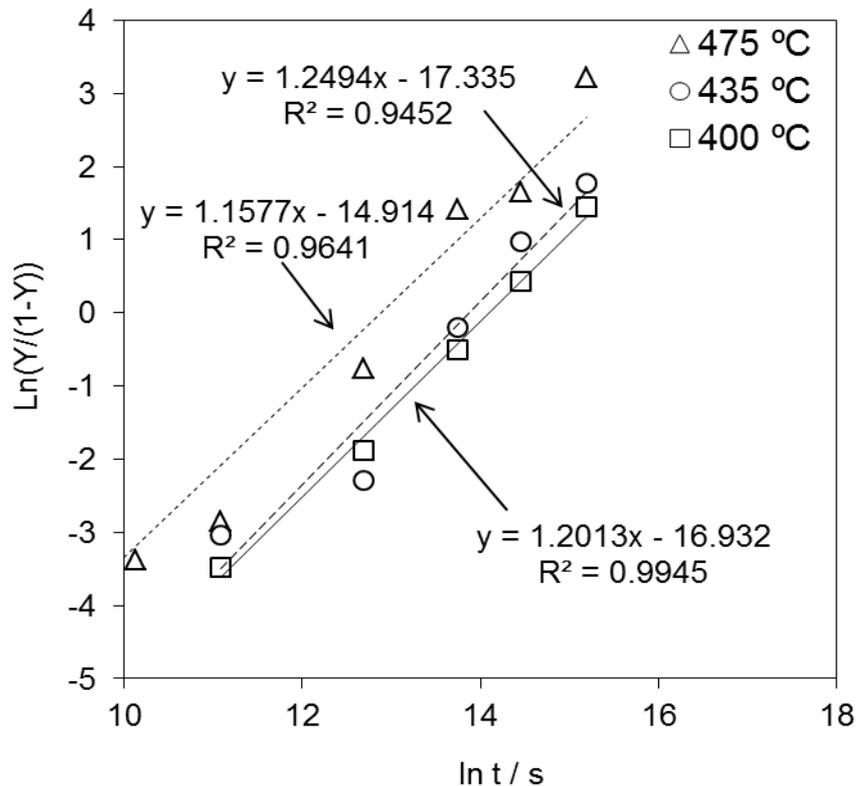
Activation energy for α' -phase

Fitting TEP (ΔS) to Austin-Rickett equation:

$$\frac{f(t)}{1-f(t)} = K(T)t^n$$

$$f(t) = \frac{(\Delta S - \Delta S_i)}{(\Delta S_f - \Delta S_i)} \quad ,, \quad f(t) \equiv Y$$

$$K(T) = k_o \exp\left\{-\frac{Q}{RT}\right\}$$

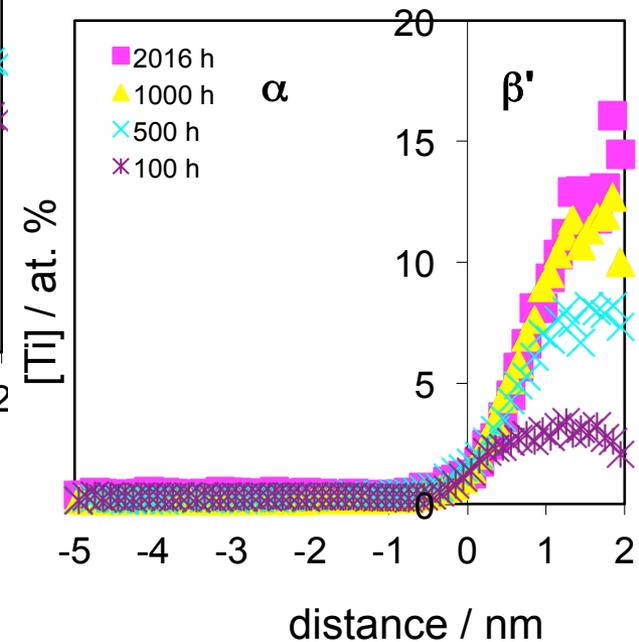
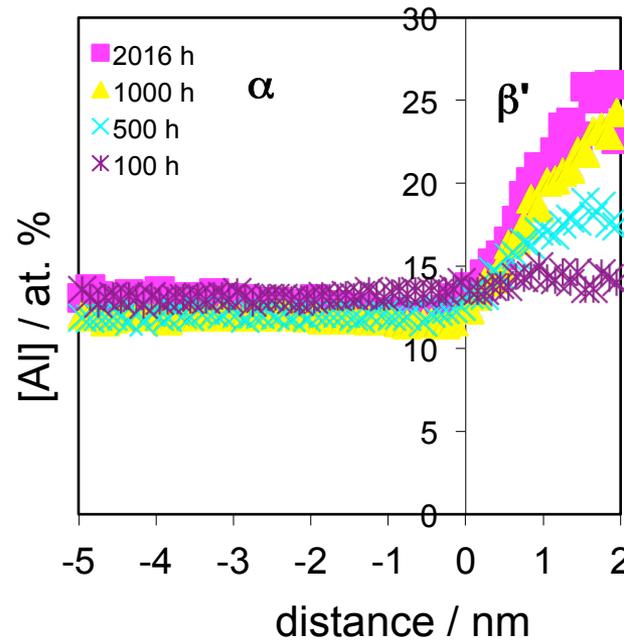
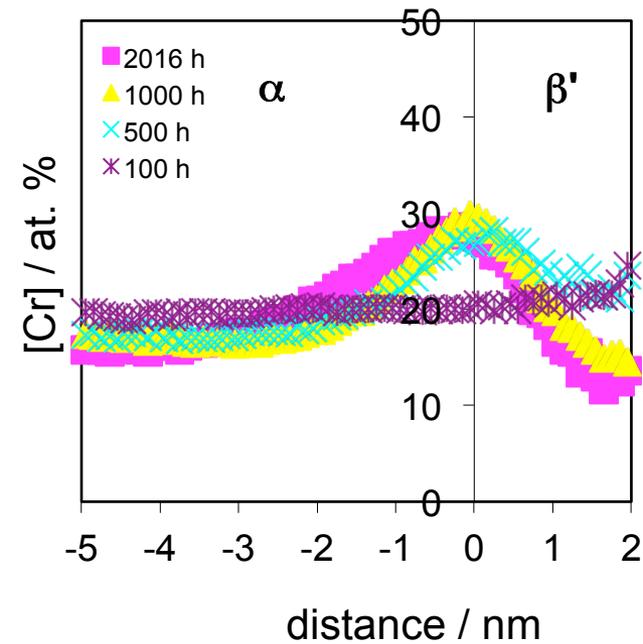


$Q = 242 \text{ kJ mol}^{-1}$,, $n=1.2$

Activation energy for Cr self-diffusion in Fe $\rightarrow 248 \text{ kJ mol}^{-1}$

Novel β' -phase: Composition

Proximity histograms analysis



435 °C

Nature of β' -phase

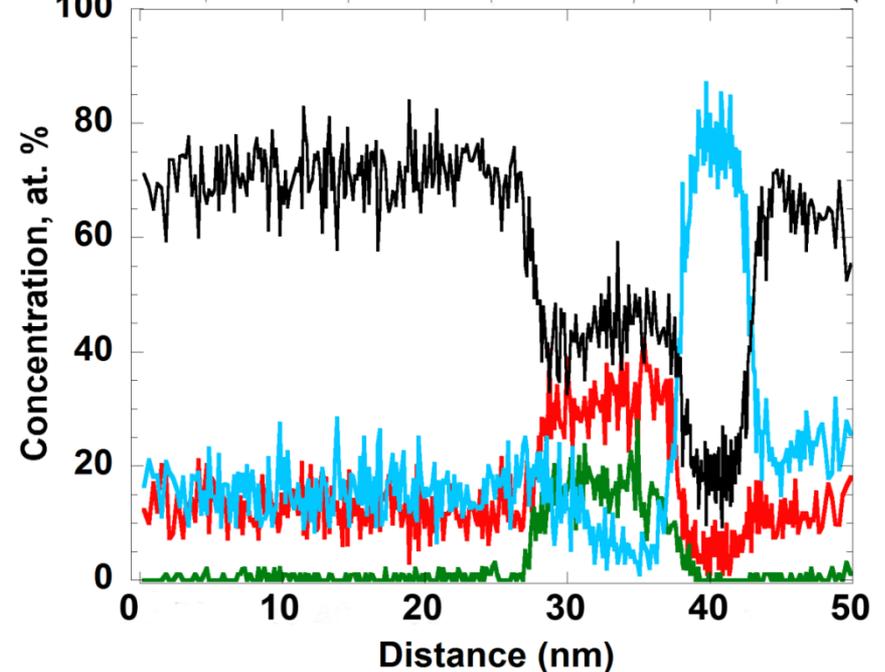
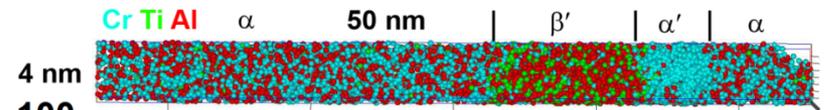
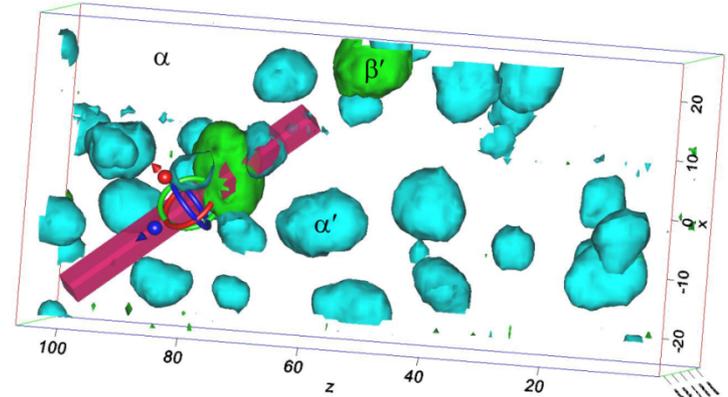
Composition of β' phase:

Fe = 49 at.%

Al = 25 at.%

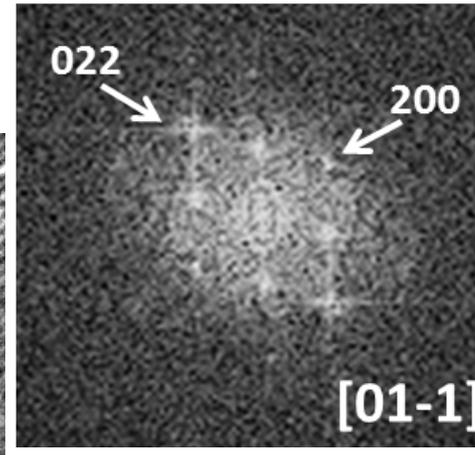
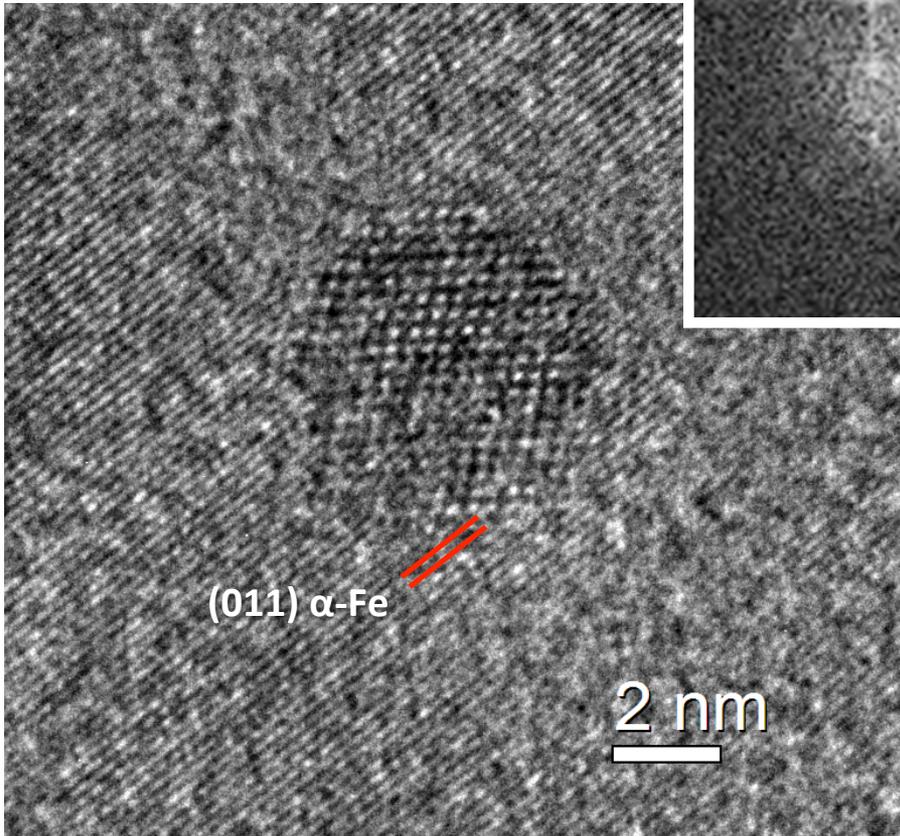
Ti = 15 at.%

Cr = 11 at.%



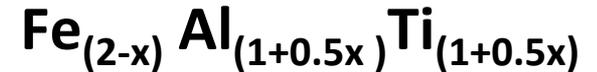
Nature of β' -phase

HRTEM Results



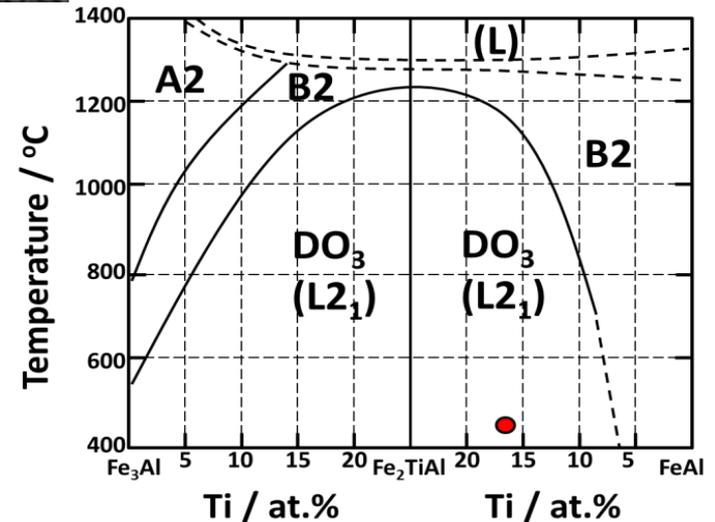
(FFT)

Solid-solution type:



Cubic space group Fm3m

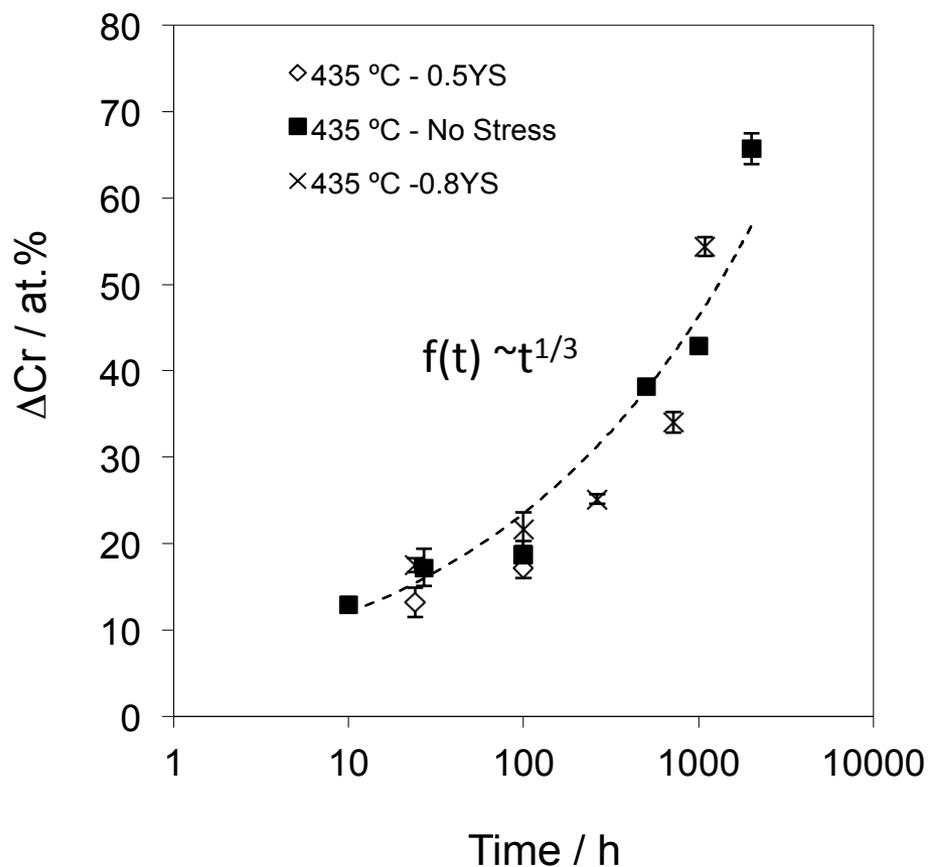
$a=0.5879 \text{ nm}$



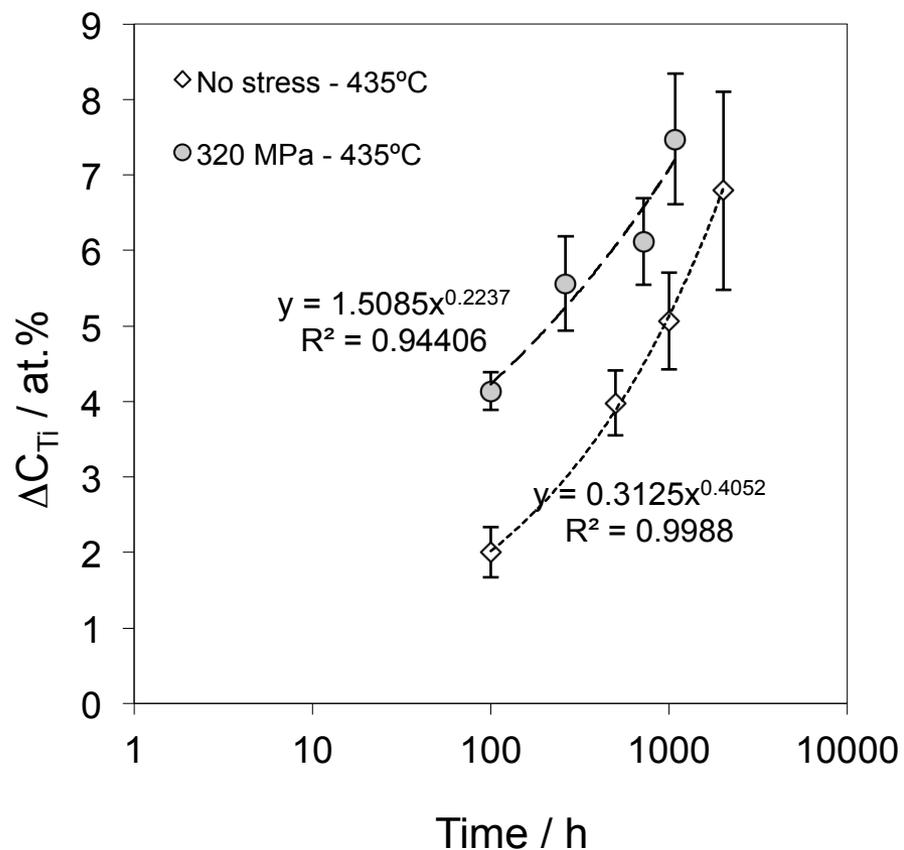
Coherency with matrix: (011) of Fe (0.203 nm) coincide with the planes (022) of the particle (0.208 nm)

Effect of elastic stress

α - α' phase separation



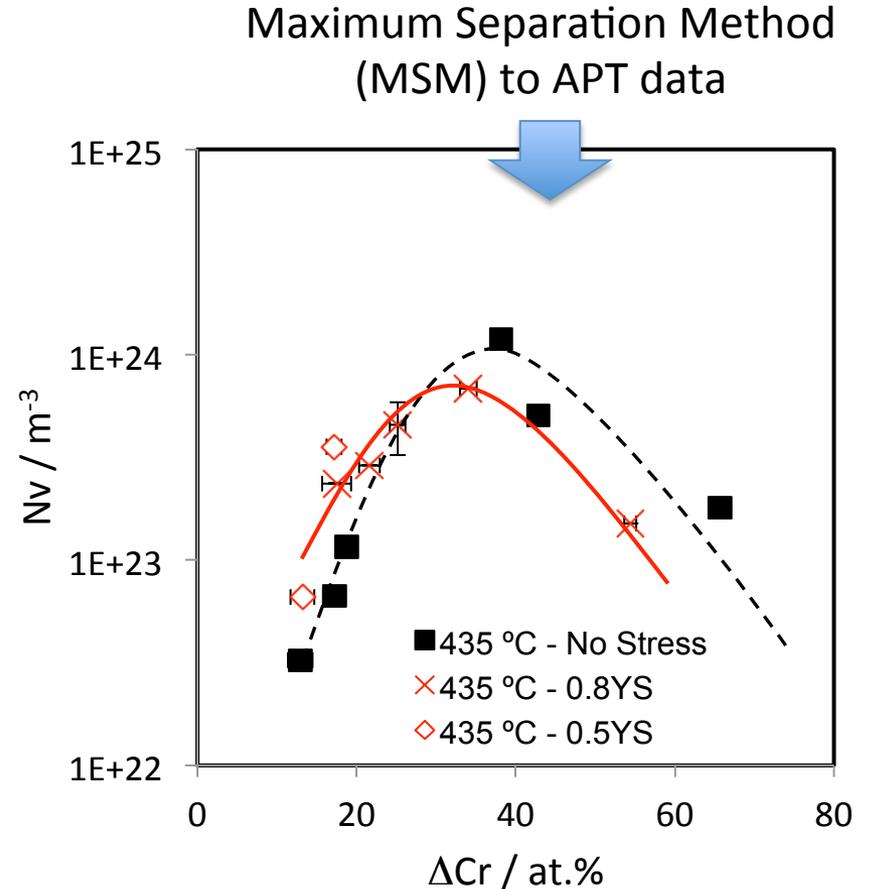
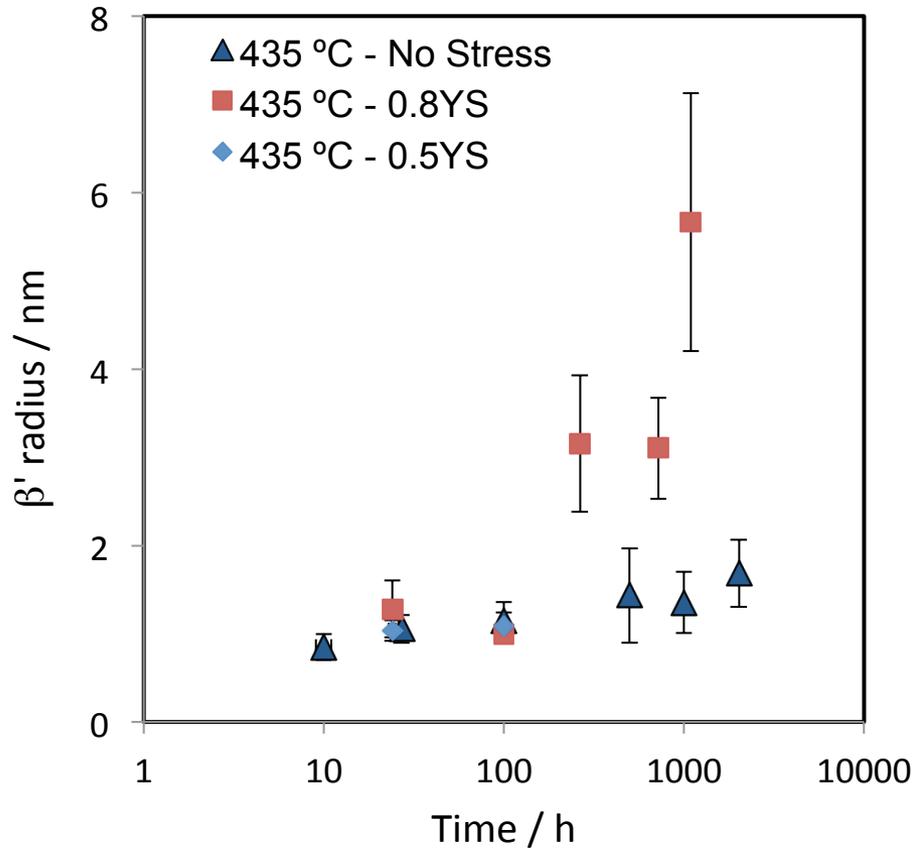
β' precipitation



α' -phase precipitation is insensitive and β' -phase is very sensitive to elastic stresses

Effect of elastic stress

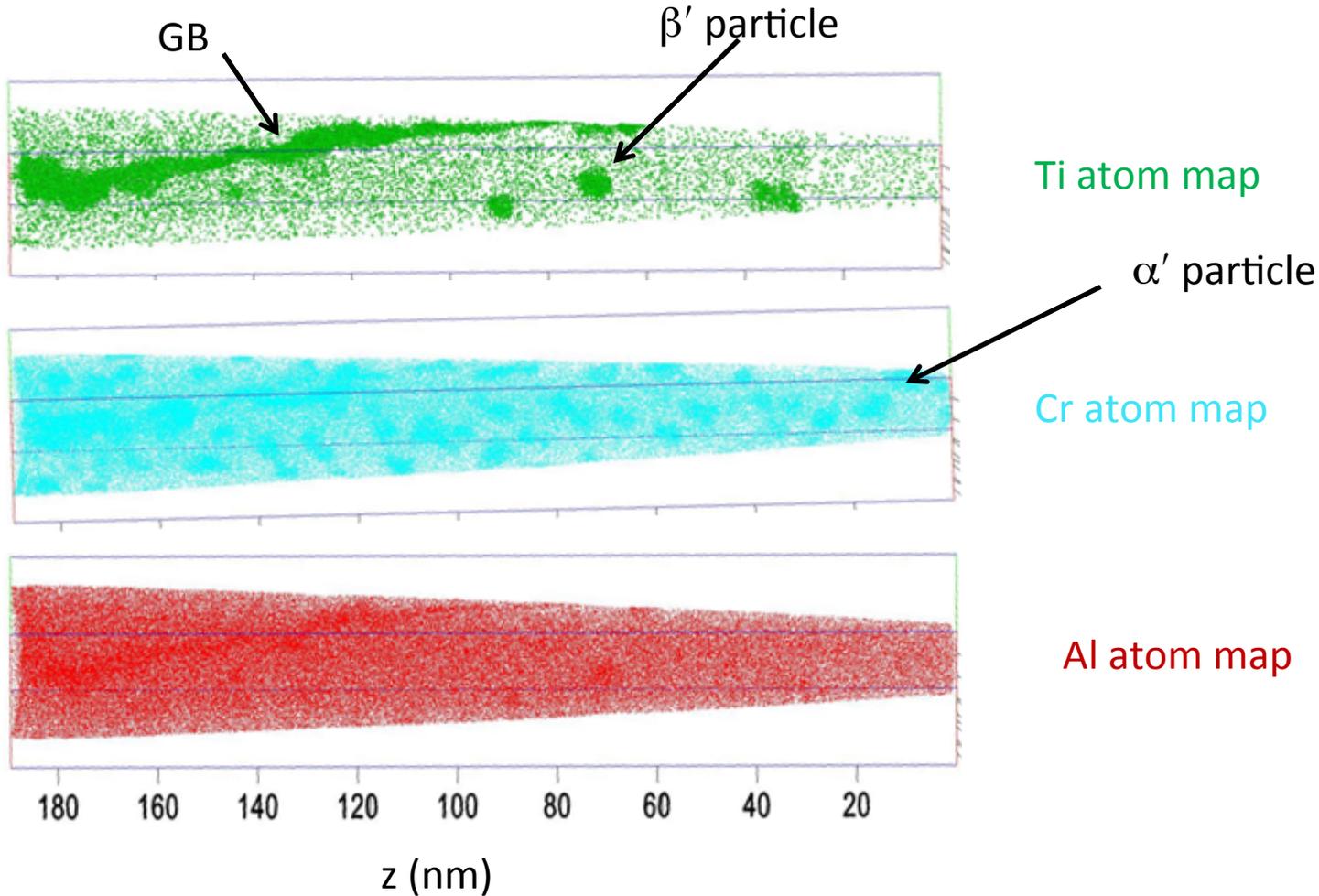
β' precipitation



Elastic stresses induce coarsen β' particles but no significant change in number density

Effect of elastic stress

Grain boundary segregation



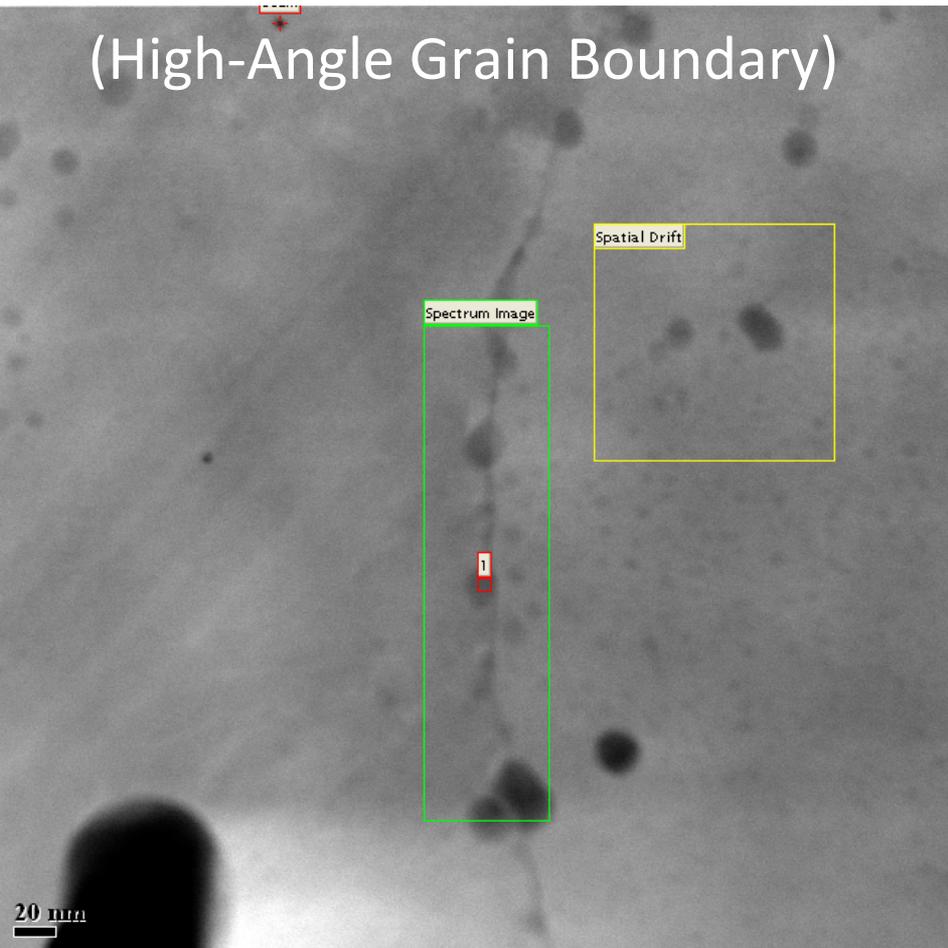
$\sigma = 0.8Y_S$

Elastic stresses induce GB segregation of Cr, Al and mainly Ti

Effect of elastic stress

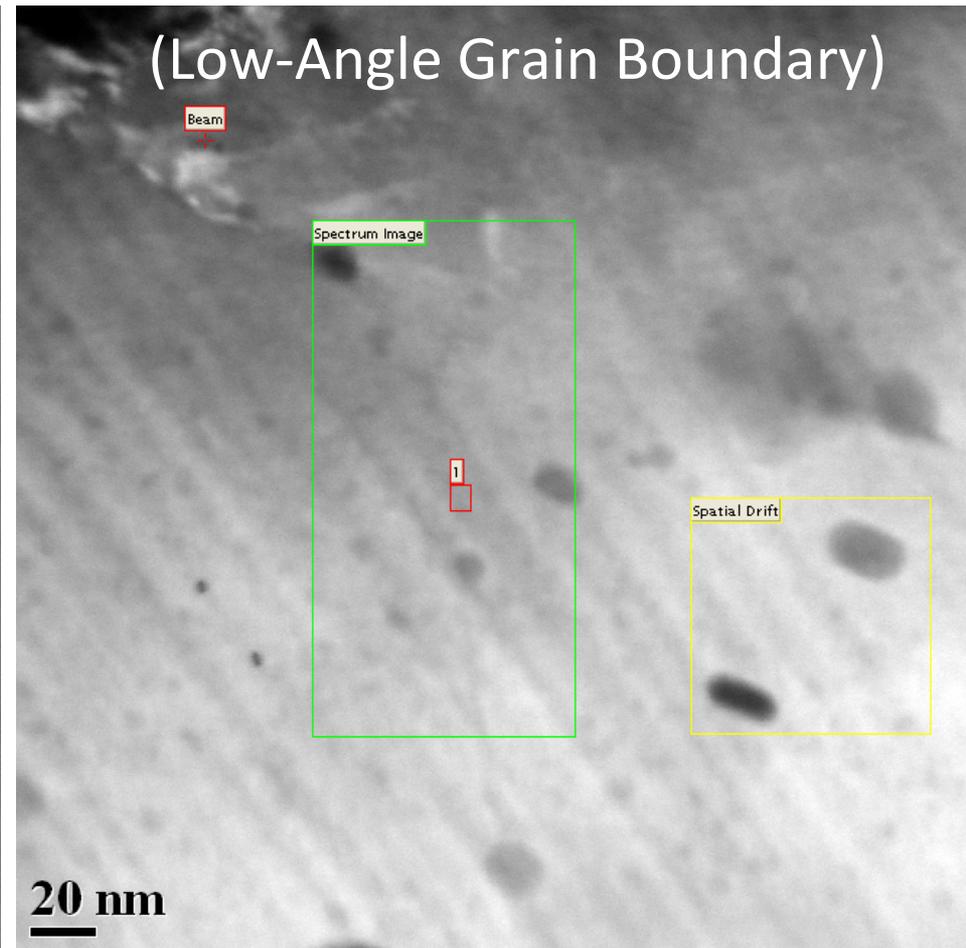
HAGB

(High-Angle Grain Boundary)



LAGB

(Low-Angle Grain Boundary)

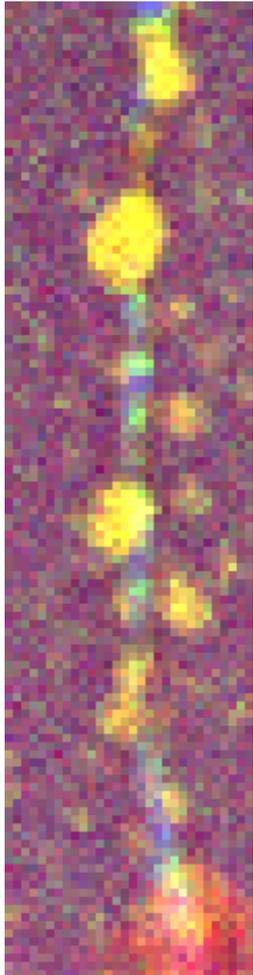


STEM energy-dispersive X-ray spectroscopy (EDS) mapping

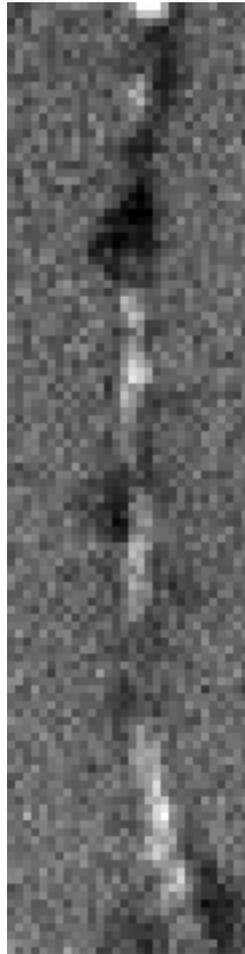
435 °C / 2000 h / 320 MPa

Effect of elastic stress

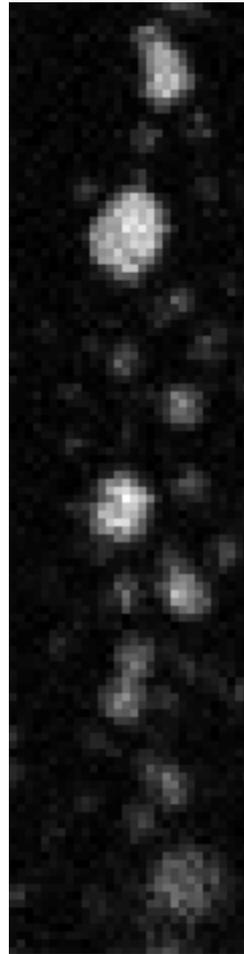
Total



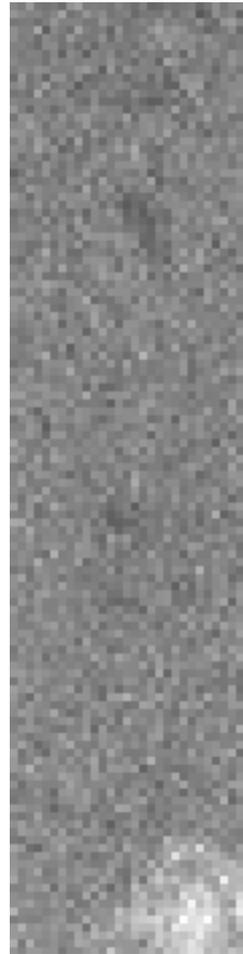
Cr



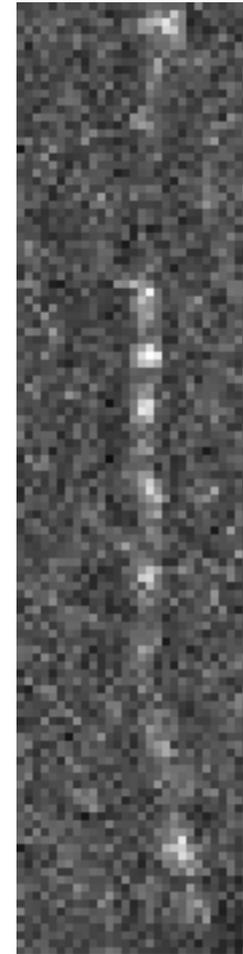
Y



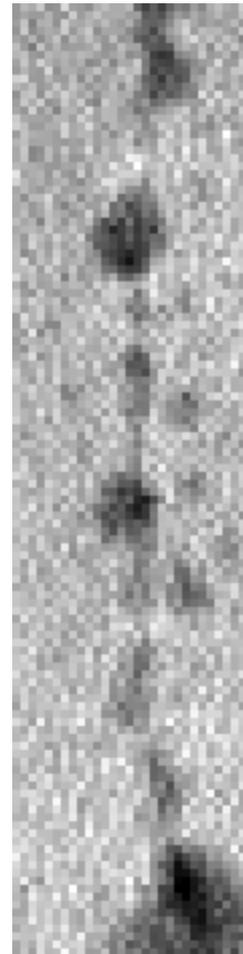
Al



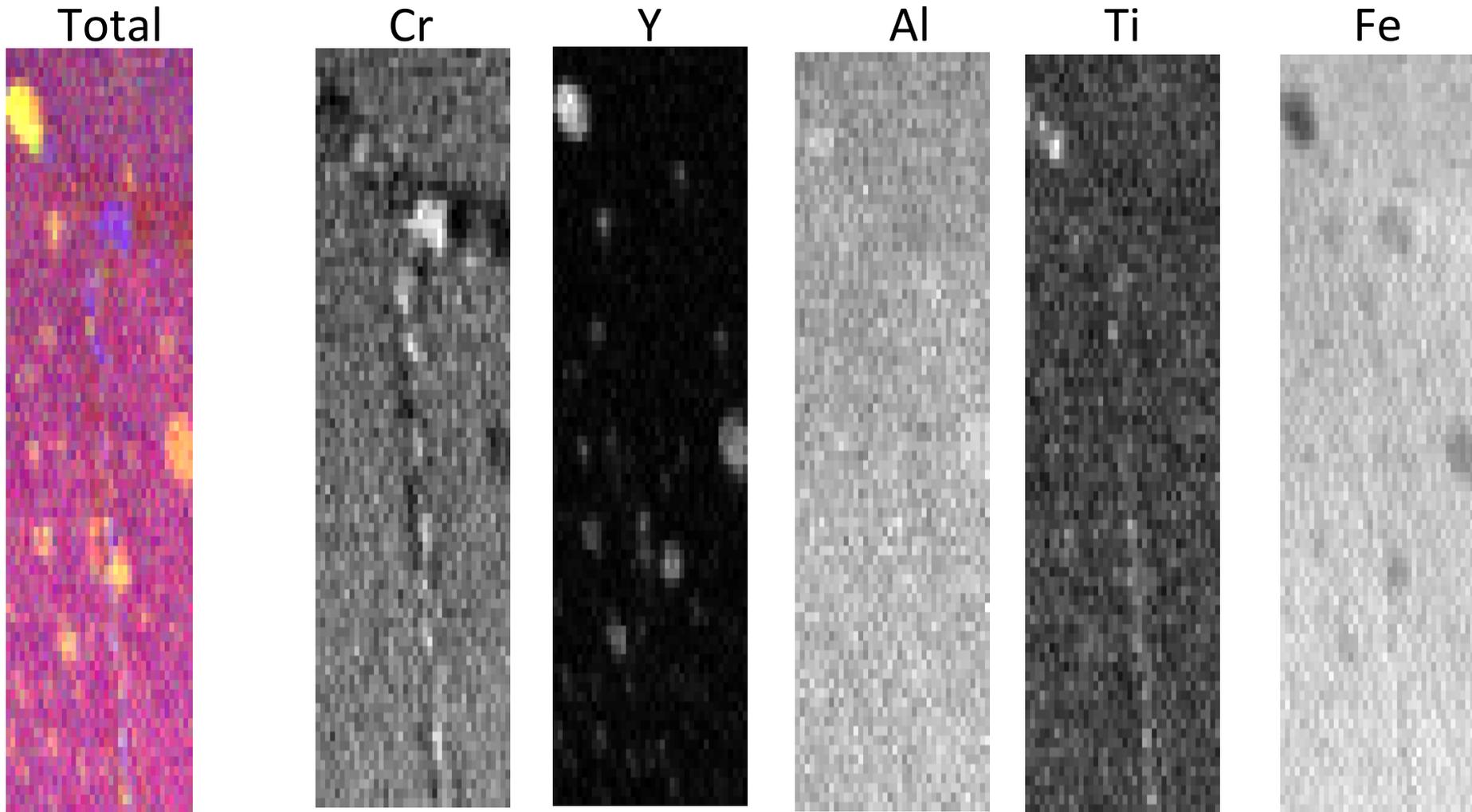
Ti



Fe



Effect of elastic stress



Conclusions

Hardening of FeCrAlTi alloy by both dispersion of nanometer in size oxides and precipitation of nanophases is studied. The following conclusions arise:

1. Proximity histograms analysis revealed that the faster phase separation kinetics without stress applied is 475 °C. The activation energy for $\alpha - \alpha'$ phase separation is 242 kJ mol⁻¹, which is similar than Cr-self diffusion in Fe.
2. Al is rejected from the α' to the matrix during the phase separation. A simultaneous precipitation of Fe-Ti-Al intermetallics: β' phase Fe₂(AlTi_{0.6}Cr_{0.4}) is found.
3. The maximum separation method estimated the size and number density of β' particles. The β' particles are more abundant and finer at 435 °C than that at 475 °C, which lead to an extra hardening.
4. Elastic stress does not affect $\alpha - \alpha'$ phase separation kinetics, but significant coarsening in β' phase is observed.
5. It was observed Ti and Al segregation at the grain boundary (HAGB and LAGB) during elastic stressed ageing treatments.